

## TR\_1D\_model1\_SS\TR\_1D\_model1\_SS.m

```

% TR_1D_model1_SS\TR_1D_model1_SS.m
%
% function imain_flag = TR_1D_model1_SS();
%
% This program calculates the steady state concentration
% and temperature profiles in a 1-D tubular reactor for
% an arbitrary number of species and an arbitrary reaction
% network. The reaction network is specified by the
% stoichiometric coefficients and the exponential powers to
% which the concentrations of each species are raised in
% the rate laws. The effective diffusivities for each
% species and the density and heat capacity of the medium
% are assumed to be constant. The heats of reaction are
% likewise assumed constant, and the temperature dependence
% of each rate constant is specified by the value of the
% rate constant at a reference temperature and a constant
% activation energy. The heat transfer coefficient for the
% cooling jacket is assumed constant. Dankwert's boundary
% conditions are applied at the inlet and outlet. A constant
% superficial velocity, obtained from knowledge of the reactor
% dimensions and volumetric flow rate, is used to quantify the
% convective contribution to the fluxes of each species'
% concentration and the enthalpy.
%
%
% PROGRAM INPUT/OUTPUT DATA
% =====
%
% problem_dimension_data (struct ProbDim)
% -----
% .num_species IN INT
%           the number of species
% .num_rxn    IN INT
%           the number of reactions
%
% reactor_data (struct Reactor)
% -----
% .len       IN    REAL
%           the length of the tubular reactor
% .dia       IN    REAL
%           the diameter of the tubular reactor
% .Qflow     IN    REAL

```

```

%           the volumetric flow rate through the
%           reactor. Along with the dimensions
%           of the reactor, it defines the superficial
%           velocity used in the convective terms of
%           the species and enthalpy balances.
% .Temp_cool  IN REAL
%           the temperature of the reactor coolant
%           jacket
% .U_HT       IN REAL
%           the overall heat transfer coefficient of
%           the reactor
% .conc_in    IN REAL(ProbDim.num_species)
%           the concentrations of each species in
%           the reactor inlet
% .Temp_in    IN REAL
%           the temperature of the reactor inlet
% .volume     PROG REAL
%           the volume of the reactor
% .cross_area PROG REAL
%           the cross sectional area of the reactor
% .surf_area  PROG REAL
%           the surface area of the reactor available
%           for heat transfer to the cooling jacket
% .velocity   PROG REAL
%           the superficial velocity in the reactor
%           that is included in the convective
%           flux terms
%
% physical_data (struct Physical)
% -----
% .diffusivity IN REAL(num_species)
%           the constant diffusivities of each species
% .density     IN REAL
%           the constant density of the medium
% .Cp         IN REAL
%           the constant heat capacity of the medium
% .thermal_conduct IN REAL
%           the constant thermal conductivity of
%           the medium
% .thermal_diff PROG REAL
%           the constant thermal diffusivity of
%           the medium
%
% rxn_data (struct Rxn)
% -----
% .stoich_coeff IN

```

```

%          REAL(ProbDim.num_rxn,ProbDim.num_species)
%          the stoichiometric coefficients
%          possibly fractional) of each
%          species in each reaction.
% .ratelaw_exp IN
%          REAL(ProbDim.num_rxn,ProbDim.num_species)
%          the exponential power (possibly fractional)
%          to which the concentration of each species
%          is raised each reaction's rate law.
% .is_rxn_elementary IN INT(ProbDim.num_rxn)
%          if a reaction is elementary, then the
%          rate law exponents are zero for the
%          product species and the negative of the
%          stoichiometric coefficient for the
%          reactant species. In this case, we need
%          not enter the corresponding components of
%          ratelaw_exp since these are determined by
%          the corresponding values in stoich_coeff.
%          We specify that reaction number irxn is
%          elementary by setting
%          is_rxn_elementary(irxn) = 1.
%          Otherwise (default = 0), we assume that
%          the reaction is not elementary and require
%          the user to input the values of
%          ratelaw_exp for reaction # irxn.
% .k_ref IN REAL(ProbDim.num_rxn)
%          the rate constants of each reaction at a
%          specified reference temperature
% .T_ref IN REAL(ProbDim.num_rxn)
%          This is the value of the reference
%          temperature used to specify the
%          temperature dependence of each
%          rate constant.
% .E_activ IN REAL(ProbDim.num_rxn)
%          the constant activation energies of
%          each reaction divided by the value
%          of the ideal gas constant
% .delta_H IN REAL(num_rxn)
%          the constant heats of reaction
%
%
% PROGRAM IMPLEMENTATION NOTES
% =====
%
% Section 1. Method of discretizing PDE's :
% -----

```

```

%
% To discretize the partial differential equations
% that describe the balances on the species
% concentrations and the enthalpy, use the method of
% finite differences. To avoid spurious oscillations
% when convection dominates and the local Peclet
% number is greater than two, use upwind differencing.
% Implement the finite difference procedure so that
% the grid point spacing may be non-uniform.
%
% grid_data (struct Grid)
% -----
% .num_pts    PIN INT
%             the number of grid points in
%             the axial direction
% .z          POUT    REAL(Grid.num_pts)
%             the values of the z-coordinate
%             at the grid points
%
% state_data (struct State)
% -----
% .conc       POUT
%             REAL(Grid.num_pts,ProbDim.num_species)
%             the values of the species'
%             concentrations at grid points
% .Temp       POUT    REAL(Grid.num_pts)
%             the values of the temperature
%             at each grid point
%
%
% Section 2. Method of solving for the steady state profiles :
% -----
%
% To solve for the steady-state profiles, we will use a robust
% two-step procedure. We will initially assume that the inlet
% conditions hold uniformly throughout the reactor. As this is
% likely to be far from the true solution, we will first perform
% a number of implicit Euler time integration steps to get
% within the vicinity of the stable steady state solution. The
% time integration will proceed until a maximum number of time
% steps have been performed or until the norm of the time
% derivative vector falls below a specified value. If the time
% derivative has become sufficiently small, we will switch to
% Newton's method with a weak-line search to aid global
% convergence.
%

```

```

% If one wishes to use only Newton's method to solve for the
% steady state profile (for example to find an unstable steady
% state), then Solver.max_iter_time is set to 0. Otherwise,
% if the maximum number of time integration steps has been
% performed and the time derivative is still too large, the
% program exits without performing any Newton's method iterations.
%
% A restart utility will be added so that if convergence is not
% achieved, executing the program again will start from the
% previously saved results. Upon a restart, new time step and
% convergence tolerances are input.
%
% At each time or Newton's method iteration, the values of the
% concentration and temperatures at each grid point will be
% constrained to be non-negative.
%
%
% iflag_restart PIN INT
%         This integer flag indicates whether the
%         simulation is a restart of a previous simulation,
%         in which only new convergence parameters need be
%         input, or is an initial simulation in which all
%         system parameters must be input. If iflag_restart
%         is non-zero, then it is a restart, if 0 then it is
%         an initial simulation.
%
% imain_flag POUT INT
%         This integer flag signifies whether the solution
%         method has converged. A positive value signifies
%         that convergence to the steady state value has
%         been attained. A negative value indicates some error.
%
% solver_data (struct Solver)
% -----
% .max_iter_time PIN INT
%         the maximum number of implicit Euler time steps.
%         If =0, then no time simulation is performed and the
%         solver goes immediately to Newton's method
% .dt PIN REAL
%         the time step to be used in the implicit
%         Euler simulation
% .atol_time PIN REAL
%         the norm of the function (time derivative) vector
%         at which the time integration procedure is deemed
%         to have been sufficiently converged
% .max_iter_Newton PIN INT

```

```
%           the maximum number of Newton's method iterations
% .atol_Newton PIN      REAL
%           the norm of the function (time derivative) vector
%           at which convergence to the steady state solution is
%           deemed to have been achieved
% .iflag_Adepend  PROGINT
%           if this integer flag is non-zero, then the A matrix
%           is assumed to be state-dependent and so must be
%           recalculated at every iteration
% .iflag_nonneg   PROG INT
%           if this integer flag is non-zero, then the elements
%           of the state vector are enforced to be non-negative
%           at every iteration
% .iflag_verbose  PROG INT
%           if this integer flag is non-zero, then the solver
%           routine is instructed to print to the screen the
%           progress of the solution process; otherwise, it
%           runs silent
%
% Interaction with Section 1. Method of discretizing PDE's :
%
% Each time that the program runs, the solver will overwrite the
% value of the concentration and temperature profiles. It could
% be that too large of a time step is used or that Newton's method
% has a problem converging, so that the quality of the solution
% is poorer than it was before the solver was called. The next
% restart should therefore start from the old, better solution
% and not necessarily the most recent. To guard against this,
% if the output solution estimate appears farther from steady
% state than the input estimate, a warning message will be
% returned and two separate output files will be created. The
% results of the solver will be written to the standard output
% file, but a second file will be written that retains the initial
% results. If these previous results are to be used in a
% subsequent restart, the user copies this file to the name of
% the standard output file before running again. User discretion
% is required in this case, because the dynamics of some systems
% have an induction period. In this case, the magnitude of the
% time derivative vector will naturally increase in the course
% of approaching the stable steady state.
%
% Kenneth Beers
% Massachusetts Institute of Technology
% Department of Chemical Engineering
% 7/2/2001
```

```

%
% Version as of 7/25/2001

function imain_flag = TR_1D_model1_SS();

func_name = 'TR_1D_model1_SS';

imain_flag = 0;

% This integer flag controls what to do if an assertion fails.
% See assertion routines for meaning.
i_error = 2;

% PDL> Ask if it is a restart, read answer to iflag_restart

disp('Starting TR_1D_model1_SS');
iflag_restart = input('Is this a restart? (0=no, 1=yes) : ');
check_real=1; check_sign=2; check_int=1;
assert_scalar(i_error,iflag_restart,'iflag_restart',...
    func_name,check_real,check_sign,check_int);

% PDL> IF it is not a restart, THEN

if(iflag_restart == 0)

% PROCEDURE: read_program_input
% PDL> Read in the program input data (intent IN)
% PDL> Among PIN data, read grid_data:num_pts
% ENDPROCEDURE

disp('Reading program input ...');

[ProbDim,Reactor,Physical,Rxn,Grid,iflag_func] = ...
    read_program_input;
if(iflag_func <= 0)
    imain_flag = -1;
    if(i_error > 1)
        save dump_error.mat;
    end
    error([func_name, ': ', ...
        'Error (', int2str(iflag_func), ') ', ...

```

```

        'returned from read_problem_input']);
end

% PROCEDURE: set_grid_1D
% PDL> Specify the locations of the grid points in z_grid.
% For the moment, simply use a uniform grid, although
% write the rest of the program to be compatible with
% the use of a non-uniform grid
% ENDPROCEDURE

disp('Setting grid ...');
[Grid.z,iflag_func] = set\_grid\_1D(Grid.num_pts,Reactor.len);
if(iflag_func <= 0)
    imain_flag = -2;
    if(i_error > 1)
        save dump_error.mat;
    end
    error(['func_name, ': ', ...
        'Error (', int2str(iflag_func), ') ', ...
        'returned from set_grid_1D']);
end

% PDL> Initialize the concentration and temperature profiles
% by setting them to be uniformly equal to the inlet
% conditions.

State.conc = zeros(Grid.num_pts,ProbDim.num_species);
for ispecies = 1:ProbDim.num_species
    State.conc(:,ispecies) = Reactor.conc_in(ispecies);
end

State.Temp = linspace(...
    Reactor.Temp_in,Reactor.Temp_in,Grid.num_pts);

% PDL> ELSE IF NOT a restart THEN

else

% PDL> Read in the file TR_1D_model1_SS.mat

disp('Reading file TR_1D_model1_SS.mat');
load TR_1D_model1_SS.mat;

```

```
% PDL> ENDIF
```

```
end
```

```
% PROCEDURE: read_solver_input  
% PDL> Input the values of the PIN variables that control  
% the solver operation  
% ENDPROCEDURE
```

```
[Solver,iflag_func] = read\_solver\_input;  
if(iflag_func <= 0)  
    imain_flag = -3;  
    if(i_error > 1)  
        save dump_error.mat;  
    end  
    error(['func_name, ': ', ...  
        'Error (', int2str(iflag_func), ') ', ...  
        'returned from read_solver_input']);  
end
```

```
%PDL> Save the initial concentration and temperature  
% profiles in back-up variables for possible later  
% use in a restart in case the solver behaves badly.
```

```
State_init = State;
```

```
% PROCEDURE: TR_1D_model1_SS_solver  
% PDL> Call the solver to update the estimate  
% of the solution vector  
% ENDPROCEDURE
```

```
[State,iflag_converge,f,f_init] = ...  
TR\_1D\_model1\_SS\_solver(State_init, ...  
    Solver,ProbDim,Reactor,Physical,Rxn,Grid);
```

```
% PDL> Write the results of the simulation to  
% the file TR_1D_model1_SS.mat
```

```
save TR_1D_model1_SS.mat;
```

```

% PDL> CASE : Select course of action based on
% value of iflag_converge returned from
% steady state solver

switch iflag_converge;

% PDL> IF iflag_converge IS 0,
% signifying no convergence

case {0}

% PDL> Set integer flag of main program,
% imain_flag to 0

imain_flag = 0;

% PDL> If the norm of the function (time derivative)
% vector is greater after the solver operation
% than it was before, set the return value of
% imain_flag to indicate this. Then, write the
% old profiles to the file
% TR_1D_model1_SS_backup.mat and set
% imain_flag as indicator

norm_f_init = max(abs(f_init));
norm_f = max(abs(f));

if(norm_f > norm_f_init)
    disp(' ');
    disp(['Final estimate had larger error ',...
        'than initial estimate']);
    imain_flag = -4;
    State = State_init;
    clear State_init;
    save TR_1D_model1_SS_backup.mat;
end

% PDL> IF iflag_converge IS 1, signifying convergence
% PDL> Print convergence message and set
% imain_flag to 1

```

```
case {1}

    imain_flag = 1;
    disp(' ');
    disp('Solver converged');

%     PDL> IF iflag_converge IS negative, signfying error
%         PDL> Print error message and set imain_flag to -1

otherwise

    imain_flag = -5;
    disp(['Error encountered with iflag_converge = ', ...
          int2str(iflag_converge)]);

% PDL> ENDCASE

end

% PDL> Make plots of the solver output results

plot\_results(ProbDim.num_species,Grid,State);

return;
```