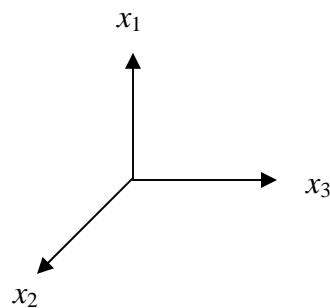


12.520 Lecture Notes 14

Simple Example: Uniaxial Strain

Uniaxial strain is excellent approximation, but not exact.

Sediment loading erosion:



Assume $e_{22} = e_{33} = 0$, $e_{11} \neq 0$

$$\begin{aligned}\tau_{11} &= (\lambda + 2\mu)e_{11} \\ \tau_{22} = \tau_{33} &= \lambda e_{11} = \frac{\lambda}{\lambda + 2\mu} \tau_{11} = \frac{\nu}{1 - \nu} \tau_{11} \\ \tau_{11} &= \frac{(1 - \nu)Ee_{11}}{(1 + \nu)(1 - 2\nu)}\end{aligned}$$

$$\tau = -\rho gd \begin{bmatrix} 1 & 0 & 0 \\ 0 & \frac{1}{3} & 0 \\ 0 & 0 & \frac{1}{3} \end{bmatrix} = \underline{\underline{\tau}}^{\text{uniaxial}}$$

For $\gamma = 0.25$, $\tau_{11} = -\rho gh$; -0.27 kbar/km (crustal rock)

$$\tau_{22} = \tau_{33} = \frac{\tau_{11}}{3}; -0.1 \text{ kbar/km} \Rightarrow \text{deviatoric stress}$$

$$\begin{bmatrix} -0.27 & 0 & 0 \\ 0 & -0.09 & 0 \\ 0 & 0 & -0.09 \end{bmatrix} = \begin{bmatrix} -0.15 & 0 & 0 \\ 0 & -0.15 & 0 \\ 0 & 0 & -0.15 \end{bmatrix} + \begin{bmatrix} -0.12 & 0 & 0 \\ 0 & -0.06 & 0 \\ 0 & 0 & -0.06 \end{bmatrix}$$

Unloading:

Assume initially lithostatic

$$\tau_{11} = \tau_{22} = \tau_{33} = -\rho gd$$

$$\Rightarrow \begin{bmatrix} 0 & 0 & 0 \\ 0 & -\frac{2}{3}\rho gd & 0 \\ 0 & 0 & -\frac{2}{3}\rho gd \end{bmatrix} = \begin{bmatrix} \frac{4}{9} & 0 & 0 \\ 0 & -\frac{2}{9} & 0 \\ 0 & 0 & -\frac{2}{9} \end{bmatrix} \rho gd + \begin{bmatrix} -\frac{4}{9} & 0 & 0 \\ 0 & -\frac{4}{9} & 0 \\ 0 & 0 & -\frac{4}{9} \end{bmatrix} \rho gd$$

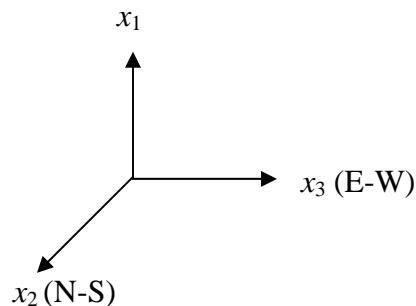
\Rightarrow thrust faults

popups

give direction of compressional stress

Assume $\sigma_2 < \sigma_3$ tectonic stress

Type of faulting: (compression negative)



$\sigma_2 < \sigma_3 < \sigma_1 \Rightarrow$ thrusting on E-W plane

$\sigma_2 < \sigma_1 < \sigma_3 \Rightarrow$ strike-slip

$\sigma_1 < \sigma_2 < \sigma_3 \Rightarrow$ normal faulting on N-S plane

Stress increment from burial

$$\tau = -\begin{bmatrix} 1 & 0 & 0 \\ 0 & \frac{1}{3} & 0 \\ 0 & 0 & \frac{1}{3} \end{bmatrix} \rho gd = -\begin{bmatrix} \frac{5}{9} & 0 & 0 \\ 0 & \frac{5}{9} & 0 \\ 0 & 0 & \frac{5}{9} \end{bmatrix} \rho gd + \begin{bmatrix} -\frac{4}{9} & 0 & 0 \\ 0 & \frac{2}{9} & 0 \\ 0 & 0 & \frac{2}{9} \end{bmatrix} \rho gd$$

Near surface in Ventura Basin, thrusting occurs. Stress tensor could look something like:

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & -\tau & 0 \\ 0 & 0 & -\alpha\tau \end{bmatrix}$$

$\tau \equiv$ "tectonic" stress

$$0 \leq \alpha \leq 1$$

$$p = -\frac{1+\alpha}{3}\tau$$

Assume tectonic stress independent of depth.

For simplicity, assume

$$\alpha = \frac{1}{2} \Rightarrow p = -\frac{\tau}{2}$$

Total deviatoric stress is

$$\begin{bmatrix} -\frac{4}{9} & 0 & 0 \\ 0 & \frac{2}{9} & 0 \\ 0 & 0 & \frac{2}{9} \end{bmatrix} \rho g d - \begin{bmatrix} -\frac{1}{2} & 0 & 0 \\ 0 & \frac{1}{2} & 0 \\ 0 & 0 & 0 \end{bmatrix} \tau$$

Normal faulting occurs if

$$\begin{aligned} -\frac{4}{9} \rho g d + \frac{\tau}{2} &< \frac{2}{9} \rho g d - \frac{\tau}{2} < \frac{2}{9} \rho g d \\ -\frac{2}{3} \rho g d &< -\tau \end{aligned}$$