Massachusetts Institute of Technology

Department of Electrical Engineering and Computer Science

6.691 Seminar in Advanced Electric Power Systems

Problem Set 1 Solutions

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Problem 2.7 This one can be done almost by inspection. The capacitor delivers reactive power $Q_c = -5$, the inductor absorbs reactive power: $Q_L = 10$. The resistor absorbs real power: $P_R = .1$. So the total complex power delivered by the source is

$$S_s = P_R + jQ_c + jQ_L = .1 + j5$$

Problem 2.11 The delta-connected capacitors may be replaced by a wye connected capacitor with value $X_c = 1/3$. The delta connected voltage source can be replaced with a wye connected source with value $V = \frac{1}{\sqrt{3}}e^{-j\frac{\pi}{6}}$. then we can work a single phase problem. Voltage at the node a' is found through superposition. Note that the voltage divider relationship in both directions is between a reactance of value .1 and a parallel combination of the other reactance of value .1 and the capacitance with reactance of $-\frac{1}{3}$. The parallel impedance is inductive and has value:

$$j.1||(-j\frac{1}{3}) = \frac{j}{7}$$

$$\frac{j.1||\frac{-j}{3}}{\frac{j.1}{1}|\frac{-j}{3}+.1} = \frac{10}{17}$$

The voltage at the node indicated is then:

$$v_a = \frac{10}{17} \left(1 + \frac{1}{\sqrt{3}} e^{-j\frac{\pi}{6}} \right)$$

Since the problem is balanced, the other two phase voltages are the same but rotated by 120°

$$v_b = v_a e^{-j\frac{2\pi}{3}}$$
$$v_c = v_a e^{j\frac{2\pi}{3}}$$

Line-line voltage is simply:

$$v_a - v_b = v_a \sqrt{3}e^{j\frac{\pi}{6}}$$

Problems 4.1, 4.2 and 4.15 This can be worked right out of the textbook, using the formulae on Page 96 and 98. This is all worked out in the following MATLAB script:

% Problem 4.1 and 4.2

% basic info for problem 4.1

z = .17 + j * .79;

y = j * 5.4e-6;

```
gamma1 = sqrt(y*z);
Zc1 = sqrt(z/y);
alpha1 = real(gamma1);
beta1 = imag(gamma1);
% and now for problem 4.2
z=.02+j * .54;
y = j*7.8e-6;
gamma = sqrt(y*z);
Zc2 = sqrt(z/y);
alpha2 = real(gamma);
beta2 = imag(gamma);
% Idiot Check Time:
C = 186000;
                   % remember we are dealine in miles
beta_f = 377/C;
fprintf('Problems 4.1 and 4.2\n')
fprintf(' 138 kV LineDecay Rate = %g Propagation Constant = %g Char Impedance = %g\n',
fprintf(' 765 kV LineDecay Rate = %g Propagation Constant = %g Char Impedance = %g\n',
fprintf(' Free Space
                                             Propagation Constant = %g\n', beta_f)
% now on to problem 4.15
1 = 400;
                     % miles!
P1 = 100e6;
                     % receiving end real power
Ql = Pl*sqrt(1-.95^2);
T11 = cosh(gamma*1); % these are the parameters of the T-model
T22 = T11;
T12 = Zc2*sinh(gamma*l);
T21 = sinh(gamma*1)/Zc2;
Ir = P1/(3*Vr) - j*Q1/(3*Vr);
                             % and line current
Vs = Vr * T11 + Ir * T12;
Is = Vr * T21 + Ir * T22;
delta = angle(Vs);
Ps = 3*real(Vs * conj(Is));
Qs = 3*imag(Vs * conj(Is));
eff = P1/Ps;
fprintf('Receiving End Voltage = %g Current = %g\n', Vr, abs(Ir))
fprintf('Sending End Voltage = %g Current = %g\n', abs(Vs), abs(Is))
fprintf('Sending End Real Power = %g Reactive Power = %g\n', Ps, Qs)
fprintf('Power Angle = %g Efficiency = %g\n', delta, eff)
% another idiot check: what is Surge Impedance Loading?
VI_si = 3*Vr^2/Zc2;
fprintf('Surge Impedance Loading P = %g Q = %g\n', real(VI_si), imag(VI_si))
```

And the screen printout that results is:

```
Problems 4.1 and 4.2
```

```
138 kV Line

Decay Rate = 0.000220969 Propagation Constant = 0.00207722 Char Impedance = 384.67

765 kV Line

Decay Rate = 3.79993e-05 Propagation Constant = 0.00205267 Char Impedance = 263.16

Free Space Propagation Constant = 0.00202688

Receiving End Voltage = 433013 Current = 80.6455

Sending End Voltage = 300852 Current = 1189.7

Sending End Real Power = 1.12271e+08 Reactive Power = -1.06789e+09

Power Angle = 0.0648288 Efficiency = 0.890702

Surge Impedance Loading P = 2.13673e+09 Q = 3.95555e+07
```

Note we have done a couple of things beyond the problem statement: the propagation coefficient of the transmission line is nearly the same as free space, so the two lines have propagation coefficients that are similar, but their decay coefficients are, as one would expect, quite a bit different. Note also this line is very lightly loaded, which is why the sending end current and voltage are markedly different from the receiving end conditions. Were we to drive the line with power closer to the surge impedance loading the two end conditions would be much closer together.

Problem 4.27 Well, we kind of wimped out here and let MATLAB do all the work. Here is the script that does it all:

```
% Problem 4.27
% data
Rl = .01;
                              % line impedance
X1 = .1;
P1 = .5;
                               % real power on load side
Q1 = .5;
% despairing of closed form solution, set up Newton's method
delt = .1;
                              % starting guess
not_done = 1;
while not_done == 1,
    P = real((exp(-j*delt)-1)/(Rl - j*Xl));
                                                    \% real power at load bus for this delta
    J = real(-j*exp(-j*delt)/(Rl - j*Xl));
                                                    % one element jacobian
    if abs(P-P1) < .0000001,
                                                      % test
        not_done = 0;
    end
    delt = delt - (P-P1)/J;
                                                    % correction
Qb = imag((exp(-j*delt)-1)/(Rl - j*Xl));
                                                    % this is total reactive power at load
Qg = Qb + Q1;
                                                    % add reactive load
\% now get the sending end conditions
Ss = (1-exp(j*delt))/(Rl - j*Xl);
                                                   % sending end line power
Sg = Ss + .5 + j*.5;
                                                    % required at generator
```

% Now we do the idiot check

```
Il = abs(Ss);
                                             % this is line current
Pd = Rl * Il ^2;
                                             % line power dissipation
Pe = real(Sg) - .5 - Pl - Pd;
                                             % should be zero
Qd = X1 * I1^2;
                                            % reactive power in line
Qe = imag(Sg) - .5 - Qd - Qb;
                                             % should be zero
fprintf('Problem 4.27\n')
fprintf('Injected Reactive Power at Load Bus = \frac{m}{q} n', Qg)
fprintf('Load Angle = %g\n', delt)
fprintf('Generator Power = %g + j*%g\n', real(Sg), imag(Sg))
fprintf('Line Dissipation = %g, Reactive Power = %g\n', Pd, Qd)
fprintf('Check for errors = %g, %g\n', Pe, Qe)
```

Formal output from that script is: Note that we have done an 'idiot check' to see if both real and reactive powers balance (and they do, to the extent that $10^{-17} \approx 0$).

```
>>Problem 4.27  
Injected Reactive Power at Load Bus = 0.437176  
Load Angle = 0.0506499  
Generator Power = 1.00254 + j*0.46257  
Line Dissipation = 0.00253947, Reactive Power = 0.0253947  
Check for errors = -3.42608e-17, -1.249e-16
```