

Massachusetts Institute of Technology
Department of Electrical Engineering and Computer Science
 6.691 Seminar in Advanced Electric Power Systems

Problem Set 2 Solutions

March 8, 2006

This problem set involves the example power system which was presented in class on February 20, reproduced in Figure 1.

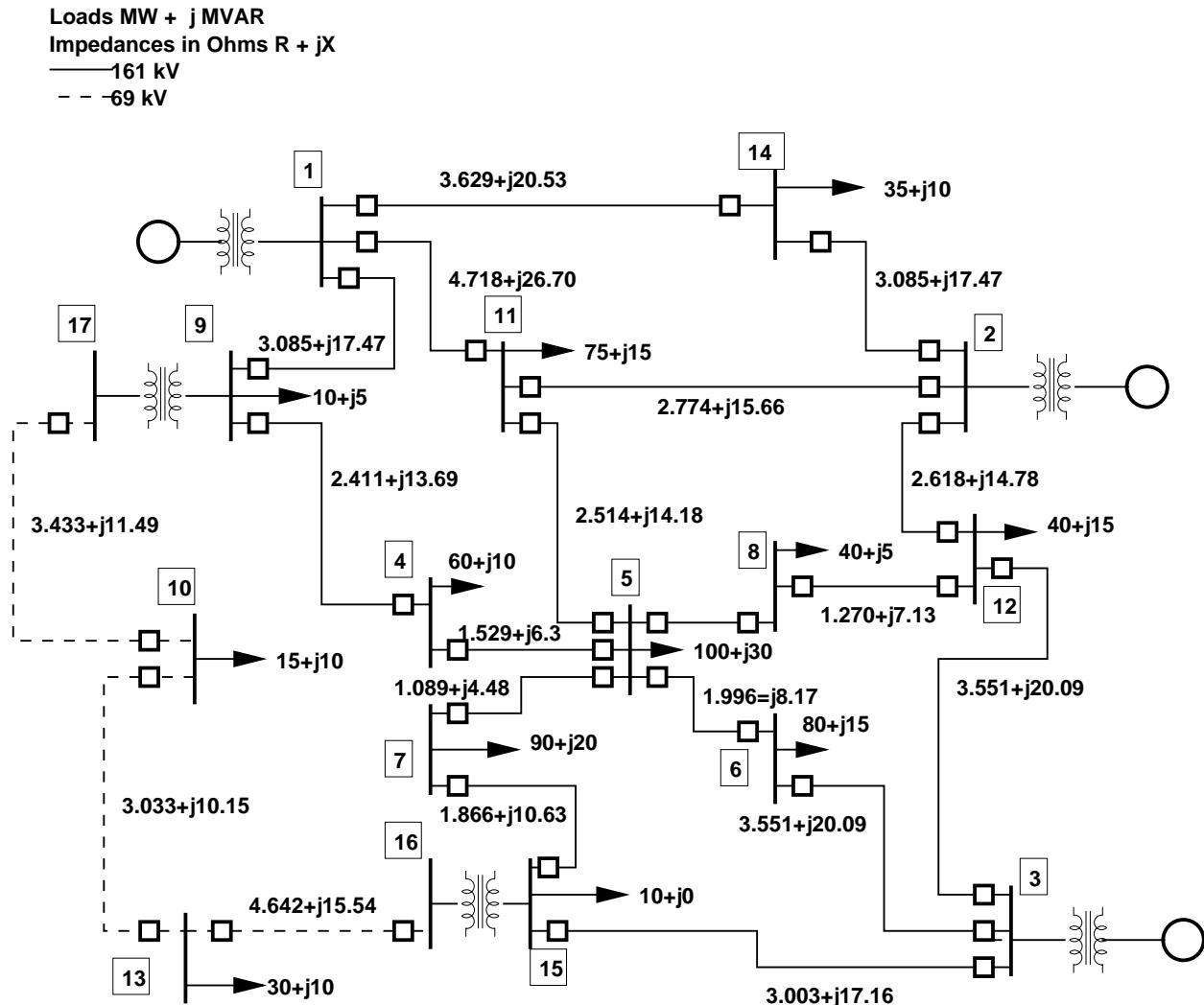


Figure 1: Example Power System

The first part of the problem consists of translating the impedances and power levels into per-unit. This is not difficult: it is necessary to divide the impedances by the base value. Here is a schedule of that calculation.

6.961 Problem Set 2 Setup

Line Impedances

Line	Buses	Ohms				Per-Unit		
1	1 14	3.629	+	j	20.530	0.0140	+	j 0.0792
2	1 11	4.718	+	j	26.700	0.0182	+	j 0.1030
3	14 2	3.085	+	j	17.470	0.0119	+	j 0.0674
4	11 2	2.774	+	j	15.660	0.0107	+	j 0.0604
5	1 9	3.085	+	j	17.470	0.0119	+	j 0.0674
6	9 4	2.411	+	j	13.690	0.0093	+	j 0.0528
7	11 5	2.514	+	j	14.180	0.0097	+	j 0.0547
8	2 12	2.618	+	j	14.780	0.0101	+	j 0.0570
9	5 8	1.996	+	j8.170		0.0077	+	j 0.0315
10	5 4	1.529	+	j6.300		0.0059	+	j 0.0243
11	5 7	1.089	+	j4.460		0.0042	+	j 0.0172
12	5 6	1.970	+	j8.090		0.0076	+	j 0.0312
13	12 3	3.551	+	j	20.090	0.0137	+	j 0.0775
14	6 3	3.551	+	j	20.090	0.0137	+	j 0.0775
15	7 15	1.886	+	j	10.630	0.0073	+	j 0.0410
16	3 15	3.003	+	j	17.160	0.0116	+	j 0.0662
17	17 10	3.433	+	j	11.490	0.0721	+	j 0.2413
18	10 13	3.033	+	j	10.150	0.0637	+	j 0.2132
19	13 16	4.462	+	j	15.540	0.0937	+	j 0.3264
20	8 12	1.270	+	j7.130		0.0049	+	j 0.0275
21	9 17					0.0000	+	j 0.0533
22	15 16					0.0000	+	j 0.0533

Note that we have included two 'lines' (21 and 22) that represent the per-unit impedance of the two transformers. Per the instructions, a re-drawn network diagram (one-line) is shown in Figure 2, with per-unit impedances, real and reactive power.

The scripts that do the work in this problem set will be appended to the end of this solution set.

The load flow problem can be done in a variety of ways, as described in class. Both Gauss-Seidel and Newton-Raphson methods are detailed in the scripts appended. The results below were generated from the decoupled Newton-Raphson script (the last one appended) The voltages at the various buses are:

Bus Voltages are:

Bus	Per-Unit	Angle (Radians)	(Degrees)
1	1.0000	0.0000	0.00
2	1.0020	0.0072	0.41
3	0.9896	-0.0160	-0.91
4	0.9545	-0.0918	-5.26
5	0.9548	-0.0909	-5.21
6	0.9574	-0.0876	-5.02
7	0.9516	-0.0972	-5.57
8	0.9640	-0.0732	-4.19

Loads MW + j MVAR
 Impedances in Ohms R + jX
 — 161 kV
 - - - 69 kV

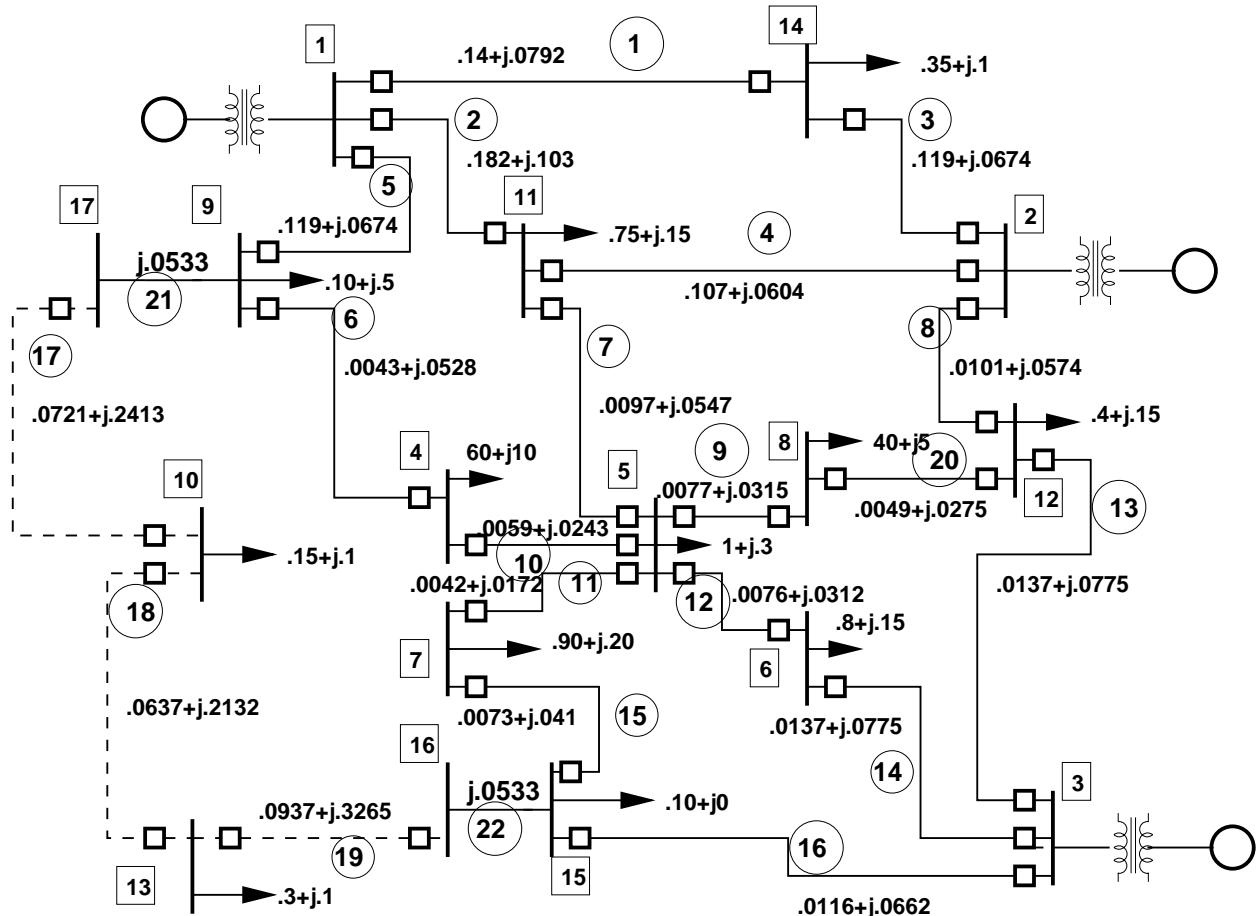


Figure 2: Per-Unit Example Power System

9	0.9657	-0.0603	-3.46
10	0.9073	-0.1325	-7.59
11	0.9745	-0.0505	-2.90
12	0.9749	-0.0463	-2.65
13	0.8981	-0.1556	-8.91
14	0.9951	-0.0083	-0.47
15	0.9609	-0.0734	-4.21
16	0.9547	-0.0859	-4.92
17	0.9582	-0.0746	-4.28

And the associated line flows are (note they are translated back into amperes):

Line Current Flows
 Line Amperes

1	42.8
2	192.1
3	88.6
4	370.1
5	358.8
6	215.6
7	281.7
8	367.8
9	213.7
10	12.9
11	136.1
12	46.4
13	151.4
14	349.7
15	211.4
16	335.7
17	246.3
18	85.6
19	211.5
20	362.8
21	105.5
22	90.6

1 Appendix 1: Starting Script (per-unit values)

```
% 6.691 Spring 2006 Solutions to Problem Set 2

% first, here are the line impedances
Z_l = [3.629+j*20.53 4.718+j*26.7 3.085+j*17.47 2.774+j*15.66 3.085+j*17.47...
        2.411+j*13.69 2.514+j*14.18 2.618+j*14.78...
        1.996+j*8.17 1.529+j*6.30 1.089+j*4.46 1.97+j*8.09 3.551+j*20.09...
        3.551+j*20.09 1.886+j*10.63 3.003+j*17.16 3.433+j*11.49 3.033+j*10.15...
        4.462+j*15.54 1.270+j*7.13];
Pb = 100e6; % we are going to use this base power
Vb1 = 161e3; % and these base voltages
Vb2 = 69e3;
Zb1 = Vb1^2/Pb;
Zb2 = Vb2^2/Pb;
% and here are the connections for each line
C_l = [1 14;
        1 11;
        14 2;
        11 2;
        1 9;
        9 4;
        11 5;
        2 12;
        5 8;
        5 4;
        5 7;
        5 6;
        12 3;
        6 3;
        7 15;
        3 15;
        17 10;
        10 13;
        13 16;
        8 12;
        9 17;
        15 16];

% here we calculate per-unit impedances: lines 1-16 and 20 are on base 1
% and lines 17 to 19 are on base 2
z_l(1:16) = Z_l(1:16) ./ Zb1;
z_l(20) = Z_l(20) / Zb1;
z_l(17:19) = Z_l(17:19) ./ Zb2;
```

```

% the last two lines are transformers
z_line = [z_l j*.08/1.5 j*.08/1.5];

fprintf('6.961 Problem Set 2 Setup\n')
fprintf('Line Impedances \n')
fprintf('Line Buses          Ohms          Per-Unit\n')
for i = 1:length(Z_l)
fprintf('%3.0f %3.0f %3.0f %10.3f + j %10.3f %10.4f + j %10.4f\n',...
    i, C_l(i, 1), C_l(i, 2), real(Z_l(i)), imag(Z_l(i)),...
    real(z_l(i)), imag(z_l(i)))
end
for i = 21:22
fprintf('%3.0f %3.0f %3.0f %10.4f + j %10.4f\n',...
    i, C_l(i, 1), C_l(i, 2), real(z_line(i)), imag(z_line(i)))
end

```

2 Gauss-Seidel Solution Script

```
% Solution to Problem Set 2
% Gauss-Seidel solution

tol=.0001;

% first, here are the line impedances
Z_l = [3.629+j*20.53 4.718+j*26.7 3.085+j*17.47 2.774+j*15.66 3.085+j*17.47...
        2.411+j*13.69 2.514+j*14.18 2.618+j*14.78...
        1.996+j*8.17 1.529+j*6.30 1.089+j*4.46 1.97+j*8.09 3.551+j*20.09...
        3.551+j*20.09 1.886+j*10.63 3.003+j*17.16 3.433+j*11.49 3.033+j*10.15...
        4.462+j*15.54 1.270+j*7.13];

% and here are the connections for each line
C_l = [1 14;
        1 11;
        14 2;
        11 2;
        1 9;
        9 4;
        11 5;
        2 12;
        5 8;
        5 4;
        5 7;
        5 6;
        12 3;
        6 3;
        7 15;
        3 15;
        17 10;
        10 13;
        13 16;
        8 12;
        9 17;
        15 16];

Pb = 100e6;      % we are going to use this base power
Vb1 = 161e3;    % and these base voltages
Vb2 = 69e3;

Zb1 = Vb1^2/Pb;
Zb2 = Vb2^2/Pb;
Ib1 = Pb/(sqrt(3)*Vb1);
Ib2 = Pb/(sqrt(3)*Vb2);
```

```

z_l = zeros(size(Z_l));
% unfortunately we have to cobble together the impedance vector
z_l(1:16) = Z_l(1:16) ./ Zb1;
z_l(20) = Z_l(20) / Zb1;
z_l(17:19) = Z_l(17:19) ./ Zb2;

% the last two lines are transformers
z_line = [z_l j*.08/1.5 j*.08/1.5];

fprintf('Line Impedances \n')
fprintf('Buses          Ohms           Per-Unit\n')
for i = 1:length(Z_l)
fprintf('%3.0f %3.0f %10.3f + j %10.3f %10.4f + j %10.4f\n',...
    C_l(i, 1), C_l(i, 2), real(Z_l(i)), imag(Z_l(i)),...
    real(z_l(i)), imag(z_l(i)))
end

Nl = length(z_line);      % number of lines
Nb = 17;                  % number of buses
% Now construct the node-incidence matrix:
NI = zeros(Nb, Nl);      % to start: now we fill it in
for i = 1:Nl
    NI(C_l(i, 1), i) = 1;
    NI(C_l(i, 2), i) = -1;
end

y_line = zeros(Nl);
% now the line admittance matrix is:
for i = 1:Nl
y_line(i, i) = 1 / z_line(i);
end

% and the bus admittance matrix is:
y_bus = NI * y_line * NI';

% Here are the bus power flows:

S_bus = [2.2+j*.7;
          2.2+j*.7;
          2.2+j*.7;
          -.6-j*.1;
          -1-j*.3;
          -.8-j*.15;
          -.9-j*.2;

```

```

-.4-j*.05;
-.1-j*.05;
-.15-j*.1;
-.75-j*.15;
-.4-j*.15;
-.3+j*.1;
-.35-j*.1;
-.1;
0; 0];

P_r = real(S_bus);
Q_r = imag(S_bus);

% now here is an initial guess about voltages:
V = ones(Nb, 1);
%Vn = ones(Nb, 1);
% now we go into a loop: check error below

n_iter = 0;
not_done = 1;
while (not_done == 1)

    for i = 2:Nb % bus 1 is the swing bus: don't modify it!
        psum = 0;
        for k = 1:Nb
            if k ~= i,
                psum = psum+y_bus(i, k) * V(k);
            end
        end
        V(i) = ((P_r(i) - j*Q_r(i))/conj(V(i)) - psum)/y_bus(i, i);
    end
%     V = Vn;
% ok, having run through the correction one cycle, check errors

P = zeros(Nb, 1);
Q = zeros(Nb, 1);
for i = 1:Nb,
    PQ = 0;
    for k = 1:Nb,
        PQ = PQ + V(i) * conj(V(k) * y_bus(i, k));
    end
    P(i) = real(PQ);
    Q(i) = imag(PQ);
end

```

```

% now find real and reactive power
PE = P-P_r;
QE = Q-Q_r;
E = [PE(2:Nb);QE(2:Nb)]; % note that bus 1 is the 'swing bus'
SE = sum(E.^2);           % this is absolute, per-unit error
if SE < tol
    not_done = 0;
end

n_iter = n_iter + 1;

fprintf('Iteration %8.0f Error = %g\n',n_iter, SE);
%pause
end

fprintf('That took %10.0f iterations\n', n_iter)

% now generate per-unit line flows

v_bus = V;
v_line = NI' * v_bus;
i_line = y_line * v_line;

I_line = zeros(size(i_line));
I_line(1:16) = Ib1 .* i_line(1:16);
I_line(17:19) = Ib2 .* i_line(17:19);
I_line(20:22) = Ib1 .* i_line(20:22);

% now generate a report:

fprintf('Bus Voltages are:\n')
fprintf('Bus      Per-Unit      Angle (degrees)\n');
for i = 1:Nb
    fprintf('%3.0f      %3.4f      %6.2f\n',i, abs(V(i)), (180/pi)*angle(V(i)));
end

fprintf('Line Current Flows\n')
fprintf('Line      Amperes\n')
for i = 1:22
    fprintf('%3.0f      %3.1f\n',i, abs(I_line(i)));
end

```

3 Newton-Raphson Solution Script

```
% Solution to Problem Set 2
% Newton-Raphson Solution...

tol=.000001;

% first, here are the line impedances
Z_1 = [3.629+j*20.53 4.718+j*26.7 3.085+j*17.47 2.774+j*15.66 3.085+j*17.47...
        2.411+j*13.69 2.514+j*14.18 2.618+j*14.78...
        1.996+j*8.17 1.529+j*6.30 1.089+j*4.46 1.97+j*8.09 3.551+j*20.09...
        3.551+j*20.09 1.886+j*10.63 3.003+j*17.16 3.433+j*11.49 3.033+j*10.15...
        4.462+j*15.54 1.270+j*7.13];
% and here are the connections for each line
C_1 = [1 14;
        1 11;
        14 2;
        11 2;
        1 9;
        9 4;
        11 5;
        2 12;
        5 8;
        5 4;
        5 7;
        5 6;
        12 3;
        6 3;
        7 15;
        3 15;
        17 10;
        10 13;
        13 16;
        8 12;
        9 17;
        15 16];

Pb = 100e6;      % we are going to use this base power
Vb1 = 161e3;    % and these base voltages
Vb2 = 69e3;

Zb1 = Vb1^2/Pb;
Zb2 = Vb2^2/Pb;
Ib1 = Pb/(sqrt(3)*Vb1);
Ib2 = Pb/(sqrt(3)*Vb2);
```

```

z_l = zeros(size(Z_l));
% unfortunately we have to cobble together the impedance vector
z_l(1:16) = Z_l(1:16) ./ Zb1;
z_l(20) = Z_l(20) / Zb1;
z_l(17:19) = Z_l(17:19) ./ Zb2;

% the last two lines are transformers
z_line = [z_l j*.08/1.5 j*.08/1.5];

% now we can assemble line capacity (in per-unit)
Icap = zeros(size(Z_l));
Icap(1:9) = 907 / Ib1;
Icap(10) = 726/Ib1;
Icap(11) = 907/Ib1;
Icap(12:14) = 726/Ib1;
Icap(15:16) = 907/Ib1;
Icap(17)=907/Ib2;
Icap(18:19) = 659/Ib2;
Icap(20) = 659/Ib1;
Icap(21:22) = 1.5;

Nl = length(z_line); % number of lines
Nb = 17; % number of buses
% Now construct the node-incidence matrix:
NI = zeros(Nb, Nl); % to start: now we fill it in
for i = 1:Nl
    NI(C_l(i, 1), i) = 1;
    NI(C_l(i, 2), i) = -1;
end

y_line = zeros(Nl);
% now the line admittance matrix is:
for i = 1:Nl
    y_line(i, i) = 1 / z_line(i);
end

% and the bus admittance matrix is:
y_bus = NI * y_line * NI';

% Here are the bus power flows:

S_bus = [2.2+j*.7; % actually, bus 1 is swing bus
         2.2+j*.7; % bus2
         2.2+j*.7]; % bus3

```

```

-.6-j*.1;           % bus 4: note this one is loaded
-1-j*.3;           % bus 5
-.8-j*.15;          % bus 6
-.9-j*.2;           % bus 7
-.4-j*.05;          % bus 8
-.1-j*.05;          % bus 9
-.15-j*.1;          % bus 10
-.75-j*.15;         % bus 11
-.4-j*.15;          % bus 12
-.3-j*.1;           % bus 13
-.35-j*.1;          % bus 14
-.1;                % bus 15
0; 0];              % buses 16 and 17 are unloaded

G = real(y_bus);
B = imag(y_bus);

P_r = real(S_bus);
Q_r = imag(S_bus);

% now here is an initial guess about voltages:
V = ones(Nb, 1);
th = zeros(Nb, 1);

% now we go into a loop
n_iter = 0;
not_done = 1;
while (not_done == 1)
P = zeros(Nb, 1);
Q = zeros(Nb, 1);
for i = 1:Nb,
    for k = 1:Nb,
        P(i) = P(i) + V(i)*V(k)*(G(i, k)*cos(th(i)-th(k))+B(i,k)*sin(th(i)-th(k)));
        Q(i) = Q(i) + V(i)*V(k)*(G(i, k)*sin(th(i)-th(k))-B(i,k)*cos(th(i)-th(k)));
    end
end

X = [th(2:Nb); V(2:Nb)];                      % to be found
J11 = zeros(Nb-1);                             % components of the Jacobian
J12 = zeros(Nb-1);
J21 = zeros(Nb-1);
J22 = zeros(Nb-1);

for i = 2:Nb
    for k = 2:Nb

```

```

ii= i-1;
kk = k-1;
if k ~= i
    J11(ii, kk) = V(i)*V(k)*(G(i,k)*sin(th(i)-th(k))-B(i,k)*cos(th(i)-th(k)));
    J12(ii, kk) = V(i)*(G(i,k)*cos(th(i)-th(k))+ B(i,k)*sin(th(i)-th(k)));
    J21(ii, kk) = -V(i)*V(k)*(G(i,k)*cos(th(i)-th(k))+B(i,k)*sin(th(i)-th(k)));
    J22(ii, kk) = V(i)*(G(i,k)*sin(th(i)-th(k))-B(i,k)*cos(th(i)-th(k)));
else
    J11(ii, ii) = -V(i)^2*B(i,i)-Q(i);
    J12(ii, ii) = P(i)/V(i)+V(i)*G(i,i);
    J21(ii, ii) = P(i)-V(i)^2*G(i,i);
    J22(ii, ii) = Q(i)/V(i)-V(i)*B(i,i);
% pause
end % end of if k~= i
end % end of index k loop
end % end of index i loop: Jacobian is constructed

J = [J11 J12;J21 J22];

% now find real and reactive power
PE = P-P_r;
QE = Q-Q_r;
E = [PE(2:Nb);QE(2:Nb)];
SE = sum(E .^2);           % this is absolute, per-unit error
if SE < tol
    not_done = 0;
end

X = X - inv(J)*E;
th =[0;X(1:Nb-1)];          % angle in radians
V = [1; X(Nb:2*Nb-2)];      % voltage in per-unit
A = (180/pi) .* th;         % angle in degrees

n_iter = n_iter + 1;

fprintf('Error = %g\n', SE);
%pause
end

fprintf('That took %10.0f iterations\n', n_iter)

% now generate per-unit line flows

v_bus = V .* exp(j .* th);
v_line = NI' * v_bus;

```

```

i_line = y_line * v_line;

I_line = zeros(size(i_line));
I_line(1:16) = Ib1 .* i_line(1:16);
I_line(17:19) = Ib2 .* i_line(17:19);
I_line(20:22) = Ib1 .* i_line(20:22);

% now generate a report:

fprintf('Bus Voltages are:\n')
fprintf('Bus Per-Unit\n');
for i = 1:Nb
    fprintf('%3.0f %8.4f %8.4f\n', i, V(i), A(i));
end

fprintf('Line Current Flows\n')
fprintf('Line per-unit Rel to capacity\n')
for i = 1:22
    fprintf('%3.0f %5.3f %5.3f\n', i, abs(i_line(i)), abs(i_line(i))/Icap(i));
end

```

4 Decoupled Newton-Raphson Solution Script

```
% Solution to Problem Set 2
% Newton-Raphson Solution..Decoupled.

tol=.000001;

% first, here are the line impedances
Z_1 = [3.629+j*20.53 4.718+j*26.7 3.085+j*17.47 2.774+j*15.66 3.085+j*17.47...
        2.411+j*13.69 2.514+j*14.18 2.618+j*14.78...
        1.996+j*8.17 1.529+j*6.30 1.089+j*4.46 1.97+j*8.09 3.551+j*20.09...
        3.551+j*20.09 1.886+j*10.63 3.003+j*17.16 3.433+j*11.49 3.033+j*10.15...
        4.462+j*15.54 1.270+j*7.13];
% and here are the connections for each line
C_1 = [1 14;
         1 11;
         14 2;
         11 2;
         1 9;
         9 4;
         11 5;
         2 12;
         5 8;
         5 4;
         5 7;
         5 6;
         12 3;
         6 3;
         7 15;
         3 15;
         17 10;
         10 13;
         13 16;
         8 12;
         9 17;
         15 16];

Pb = 100e6;      % we are going to use this base power
Vb1 = 161e3;    % and these base voltages
Vb2 = 69e3;

Zb1 = Vb1^2/Pb;
Zb2 = Vb2^2/Pb;
Ib1 = Pb/(sqrt(3)*Vb1);
Ib2 = Pb/(sqrt(3)*Vb2);
```

```

z_l = zeros(size(Z_l));
% unfortunately we have to cobble together the impedance vector
z_l(1:16) = Z_l(1:16) ./ Zb1;
z_l(20) = Z_l(20) / Zb1;
z_l(17:19) = Z_l(17:19) ./ Zb2;

% the last two lines are transformers
z_line = [z_l j*.08/1.5 j*.08/1.5];

fprintf('Line Impedances \n')
fprintf('Buses          Ohms           Per-Unit\n')
for i = 1:length(Z_l)
fprintf('%3.0f %3.0f %10.3f + j %10.3f %10.4f + j %10.4f\n',...
    C_l(i, 1), C_l(i, 2), real(Z_l(i)), imag(Z_l(i)),...
    real(z_l(i)), imag(z_l(i)))
end

Nl = length(z_line);      % number of lines
Nb = 17;                  % number of buses
% Now construct the node-incidence matrix:
NI = zeros(Nb, Nl);      % to start: now we fill it in
for i = 1:Nl
    if C_l(i, 1) ~=0,
        NI(C_l(i, 1), i) = 1;
        NI(C_l(i, 2), i) = -1;
    end
end

y_line = zeros(Nl);
% now the line admittance matrix is:
for i = 1:Nl
y_line(i, i) = 1 / z_line(i);
end

% and the bus admittance matrix is:
y_bus = NI * y_line * NI';

% Here are the bus power flows:

S_bus = [2.2+j*.7;      % but note we are going to ignore this one
         2.2+j*.7;
         2.2+j*.7;
         -.6-j*.1;
         -1-j*.3;

```

```

-.8-j*.15;
-.9-j*.2;
-.4-j*.05;
-.1-j*.05;
-.15-j*.1;
-.75-j*.15;
-.4-j*.15;
-.3-j*.1;
-.35-j*.1;
-.1;
0; 0];

G = real(y_bus);
B = imag(y_bus);

P_r = real(S_bus);
Q_r = imag(S_bus);

% now here is an initial guess about voltages:
V = ones(Nb, 1);
th = zeros(Nb, 1);

% now we go into a loop
n_iter = 0;
not_done = 1;
while (not_done == 1)
P = zeros(Nb, 1);
Q = zeros(Nb, 1);
for i = 1:Nb,
    for k = 1:Nb,
        P(i) = P(i) + V(i)*V(k)*(G(i, k)*cos(th(i)-th(k))+B(i,k)*sin(th(i)-th(k)));
        Q(i) = Q(i) + V(i)*V(k)*(G(i, k)*sin(th(i)-th(k))-B(i,k)*cos(th(i)-th(k)));
    end
end

X = [th(2:Nb); V(2:Nb)]; % to be found
J11 = zeros(Nb-1); % components of the Jacobian
J12 = zeros(Nb-1);
J21 = zeros(Nb-1);
J22 = zeros(Nb-1);

for i = 2:Nb
    for k = 2:Nb
        ii= i-1;
        kk = k-1;

```

```

if k ~= i
J11(ii, kk) = V(i)*V(k)*(G(i,k)*sin(th(i)-th(k))-B(i,k)*cos(th(i)-th(k)));
J12(ii, kk) = V(i)*(G(i,k)*cos(th(i)-th(k))+ B(i,k)*sin(th(i)-th(k)));
J21(ii, kk) = -V(i)*V(k)*(G(i,k)*cos(th(i)-th(k))+B(i,k)*sin(th(i)-th(k)));
J22(ii, kk) = V(i)*(G(i,k)*sin(th(i)-th(k))-B(i,k)*cos(th(i)-th(k)));
else
J11(ii, ii) = -V(i)^2*B(i,i)-Q(i);
J12(ii, ii) = P(i)/V(i)+V(i)*G(i,i);
J21(ii, ii) = P(i)-V(i)^2*G(i,i);
J22(ii, ii) = Q(i)/V(i)-V(i)*B(i,i);
% pause
end % end of if k~=i
end % end of index k loop
end % end of index i loop: Jacobian is constructed

J = [J11 zeros(Nb-1);zeros(Nb-1) J22];

% now find real and reactive power
PE = P-P_r;
QE = Q-Q_r;
E = [PE(2:Nb);QE(2:Nb)];
SE = sum(E .^2); % this is absolute, per-unit error
if SE < tol
not_done = 0;
end

X = X - inv(J)*E;
th =[0;X(1:Nb-1)];
V = [1; X(Nb:2*Nb-2)];

n_iter = n_iter + 1;

fprintf('Error = %g\n', SE);
%pause
end

fprintf('That took %10.0f iterations\n', n_iter)

% now generate per-unit line flows

v_bus = V .* exp(j .* th);
v_line = NI' * v_bus;
i_line = y_line * v_line;

I_line = zeros(size(i_line));

```

```

I_line(1:16) = Ib1 .* i_line(1:16);
I_line(17:19) = Ib2 .* i_line(17:19);
I_line(20:22) = Ib1 .* i_line(20:22);

% now generate a report:

fprintf('Bus Voltages are:\n')
fprintf('Bus Per-Unit Angle (Radians) (Degrees)\n');
for i = 1:Nb
    fprintf('%3.0f %3.4f %8.4f %6.2f\n', i, V(i), th(i), (180/pi)*th(i));
end

fprintf('Line Current Flows\n')
fprintf('Line Amperes\n')
for i = 1:22
    fprintf('%3.0f %3.1f\n', i, abs(I_line(i)));
end

```