

# **2.019 Design of Ocean Systems**

## **Lecture 13**

### **Mooring Dynamics (II)**

**March 28, 2011**

# Static Analysis: Catenary Cable

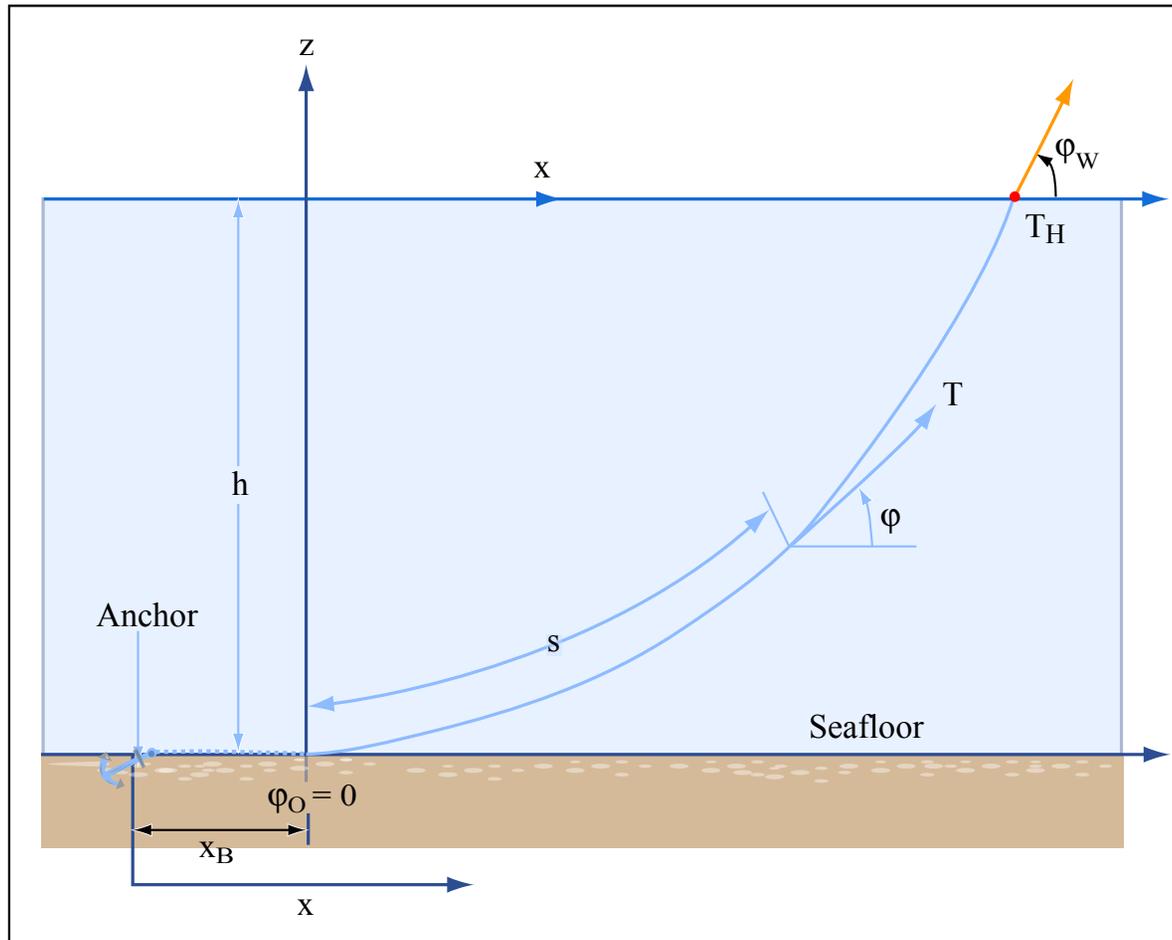


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**Cable configuration:**

$$s = \frac{T_H}{\omega} \sinh\left(\frac{\omega}{T_H} x\right)$$

$$z + h = \frac{T_H}{\omega} \left[ \cosh\left(\frac{\omega}{T_H} x\right) - 1 \right]$$

**Tension along the cable:**

$$T = T_H + \omega h + (\omega + \rho g A) z$$

$$T_z = \omega s$$

## Catenary Solution — Key Results (without Elasticity)

- Minimum line length required (or suspended length for a given fairlead tension) for gravity anchor:

$$l_{\min} = h \left( \frac{2T_{\max}}{wh} - 1 \right)^{\frac{1}{2}}$$

- Horizontal force for a given fairlead tension:

$$T_H = T - wh$$

- Horizontal scope (length in plan view from fairlead to touchdown point):

$$x = \frac{T_H}{w} \sinh^{-1} \left( \frac{wl_{\min}}{T_H} \right)$$

- Vertical force at the fairlead:

$$T_z = wl_{\min}$$

# Simple Examples

- Given  $T_{\max} = T_{\text{br}} = 1510 \text{ KN}$ ,  $w = 828 \text{ N/m}$ ,  $h = 25\text{m}$ , then

$$l_{\min} = h \left( \frac{2T_{\max}}{wh} - 1 \right)^{\frac{1}{2}} = 25 * \sqrt{\frac{2*1510*10^3}{828*25} - 1} = 300.93\text{m}$$

$$T_H = T - wh = 1510 * 10^3 - 828 * 25 = 1489\text{KN}$$

$$T_z = wl_{\min} = 828 * 301 = 249\text{KN}$$

$$x = \frac{T_H}{w} \sinh^{-1} \left( \frac{wl_{\min}}{T_H} \right) = \frac{1489*10^3}{828} \sinh^{-1} \frac{828*301}{1489*10^3} = 300\text{m}$$

- Given  $x = 270\text{m}$ ,  $w = 828 \text{ N/m}$ ,  $h = 25\text{m}$ , then

$$h = \frac{T_H}{w} \left[ \cosh \frac{wx}{T_H} - 1 \right] \longrightarrow T_H = 1200\text{kN}$$

$$T = T_H + wh = 1221\text{kN}$$

$$l_{\min} = h \left( \frac{2T}{wh} - 1 \right)^{\frac{1}{2}} = 271\text{m}$$

$$T_z = wl_{\min} = 828 * 271 = 224\text{KN}$$

# Cable Load-Excursion Relation

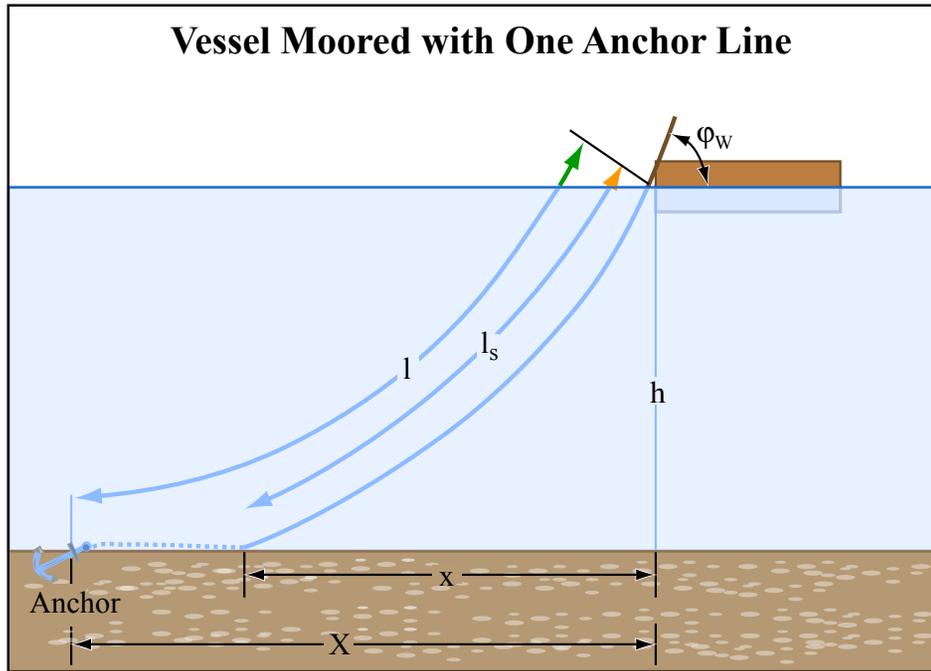


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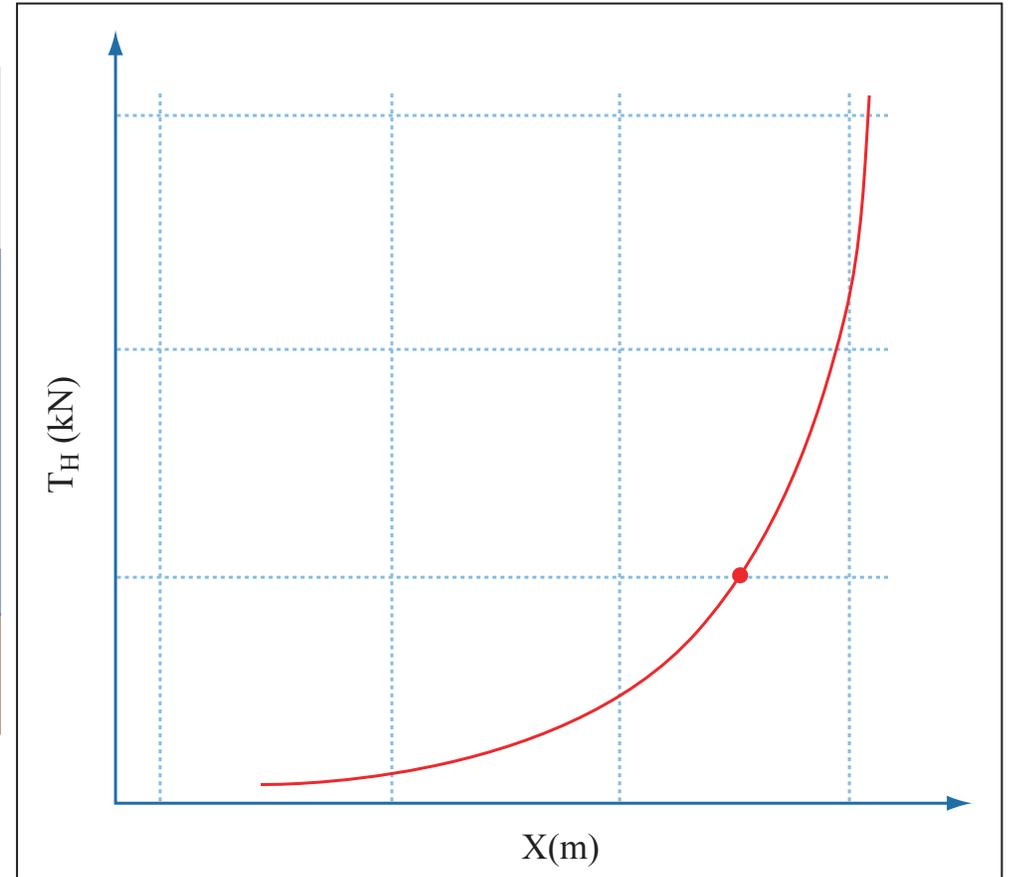


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$$X = l - l_s + x$$

$$X = l - h \left( 1 + 2 \frac{T_H}{wh} \right)^{\frac{1}{2}} + \frac{T_H}{w} \cosh^{-1} \left( 1 + \frac{wh}{T_H} \right)$$

Restoring Coefficient:

$$C_{11} = \frac{dT_H}{dX} = w \left[ \frac{-2}{\left( 1 + 2 \frac{T_H}{wh} \right)^{1/2}} + \cosh^{-1} \left( 1 + \frac{wh}{T_H} \right) \right]^{-1}$$

# Simple Example

Given: A ship experiences a total mean drift force (in surge) of 50kN, wave frequency oscillation of amplitude  $\zeta_1 = 3$  m and frequency  $2\pi/10$  rad/s, what is the total tension in the cable?

Steady tension:  $T_{0H} = 50kN$

Mean position:  $X_0 = 92.5m$

Restoring coefficient:  $C_{11}(T_{0H}) \approx 10kN/m$

$$T_H = T_{0H} + T_H(\omega) = T_{0H} + [-C_{11}\zeta_1 \cos(\omega t + \alpha)] = 50 - 30 \cos(\omega t + \alpha)$$

$$|T_H| = 80kN$$

Plus effect due to slowly varying motion

$$T' = T'_H + wh$$

# Catenary Solution — Key Results (with Elasticity)

- Horizontal force for a given fairlead tension  $T$ :

$$T_H = AE \sqrt{\left(\frac{T}{AE} + 1\right)^2 - \frac{2wh}{AE}} - AE$$

- Minimum line length required (or suspended length for a given fairlead tension) for gravity anchor:

$$l_{\min} = \frac{1}{w} \sqrt{T^2 - T_H^2}$$

- Vertical force at the fairlead:

$$T_z = wl_{\min}$$

- Horizontal scope (length in plan view from fairlead to touchdown point):

$$x = \frac{T_H}{w} \sinh^{-1} \frac{wl_{\min}}{T_H} + \frac{T_H l_{\min}}{AE}$$

$AE$ : stiffness of the cable

# Analysis of Spread Mooring System

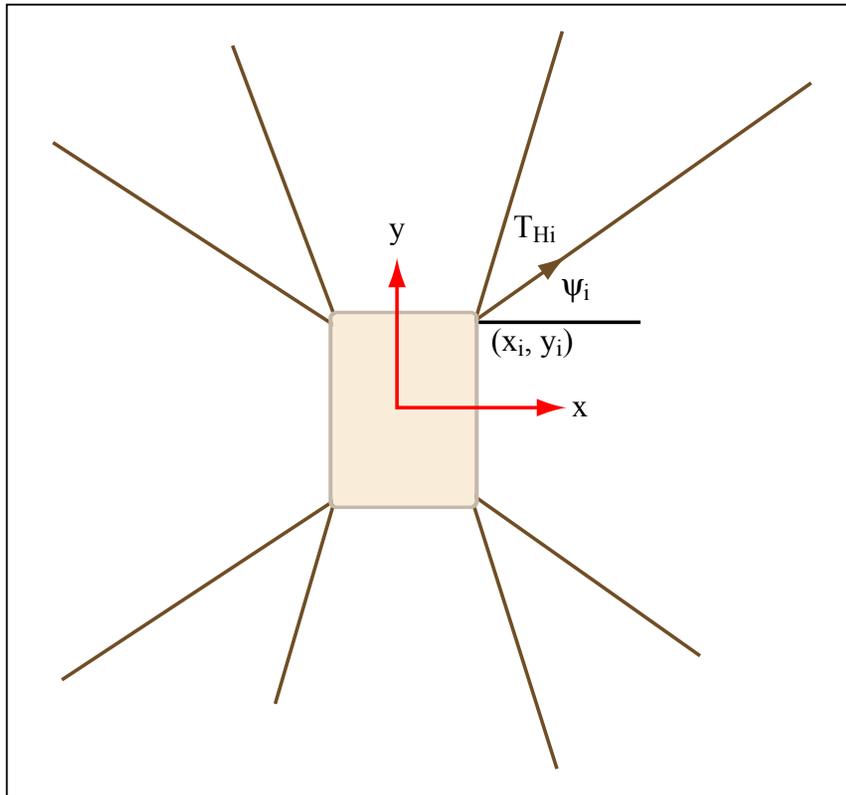


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**Total mooring line force/moment:**

$$F_1^M = \sum_{i=1}^n T_{Hi} \cos \psi_i$$

$$F_2^M = \sum_{i=1}^n T_{Hi} \sin \psi_i$$

$$F_6^M = \sum_{i=1}^n T_{Hi} [x_i \sin \psi_i - y_i \cos \psi_i]$$

**Total mooring line restoring coefficients:**

$$C_{11} = \sum_{i=1}^n k_i \cos^2 \psi_i$$

$$C_{22} = \sum_{i=1}^n k_i \sin^2 \psi_i$$

$$C_{66} = \sum_{i=1}^n k_i (x_i \sin \psi_i - y_i \cos \psi_i)^2$$

$$C_{26} = C_{62} = \sum_{i=1}^n k_i (x_i \sin \psi_i - y_i \cos \psi_i) \sin \psi_i$$

- Mean position of the body is determined by balancing force/moment between those due to environments and mooring lines
- Iterative solver is usually applied

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