



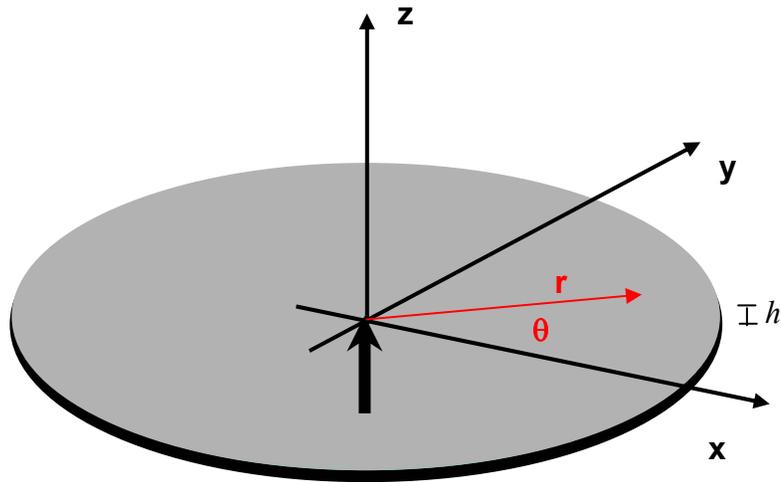
13.811

Advanced Structural Dynamics and Acoustics

Acoustics
Lecture 6



Point-Driven Plate Radiation



Cylindrical Coordinates

$$D \left(\frac{d^2}{dr^2} + \frac{d}{r dr} \right)^2 w_\omega - \rho_s h \omega^2 w_\omega = F_\omega \frac{\delta(r)}{2\pi r} - p \mathbf{x}(r)$$

Light Fluid Loading

$$D k_r^4 w_\omega(k_r) - \rho_s h \omega^2 w_\omega(k_r) \simeq F_\omega$$

$$w_\omega(k_r) = \frac{F(\omega)}{2\pi D (k_r^4 - k_f^4)}$$

Flexural Wavenumber

$$k_f = \left(\frac{m_s \omega^2}{D} \right)^{1/4} = \left(\frac{\rho_s h \omega^2}{D} \right)^{1/4}$$

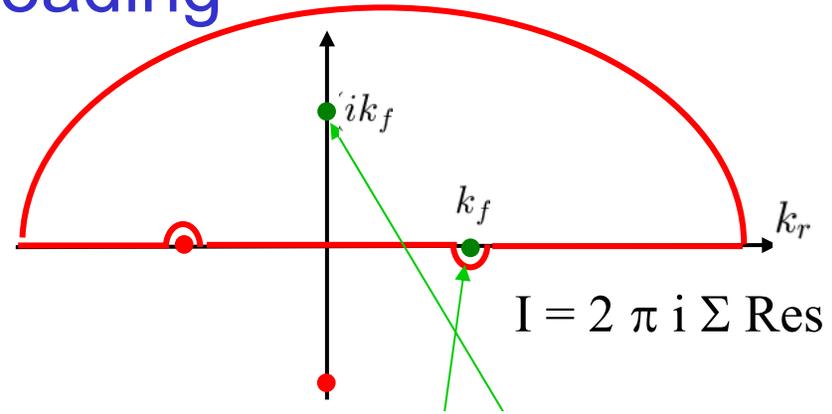
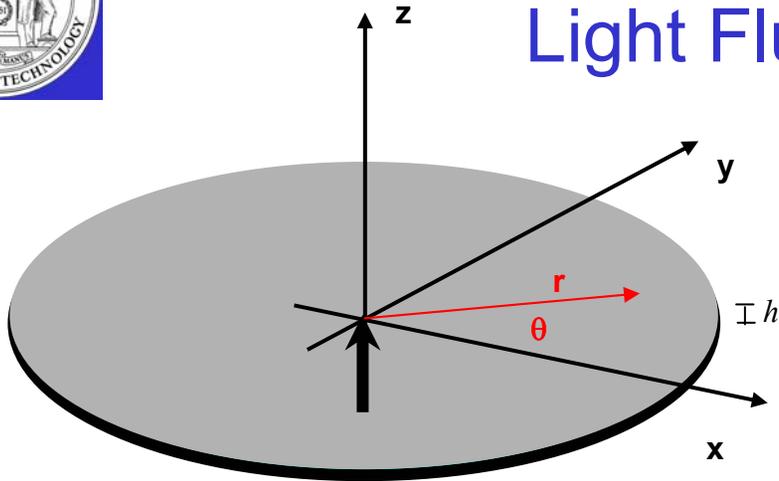
$$k_f = \frac{\omega}{\alpha}$$

Particle Velocity

$$\dot{w}_\omega(k_r) = \frac{-i\omega F_\omega}{2\pi D (k_r^4 - k_f^4)}$$



Point-driven Plate Light Fluid Loading



Inverse Hankel Transform

$$\begin{aligned}
 w(r) &= \frac{F_\omega}{2\pi D} \int_0^\infty \frac{J_0(k_r r)}{k_r^4 - k_f^4} k_r dk_r \\
 &= \frac{F_\omega}{2\pi D} \int_{-\infty}^\infty \frac{H_0^{(1)}(k_r r)}{k_r^4 - k_f^4} k_r dk_r
 \end{aligned}$$

$$\begin{aligned}
 J_0(x) &= \frac{1}{2} \left(H_0^{(1)}(x) + H_0^{(2)}(x) \right) \\
 &= \frac{1}{2} \left(H_0^{(1)}(x) - H_0^{(1)}(-x) \right)
 \end{aligned}$$

Complex Contour Integration

$$\begin{aligned}
 \dot{w}_\omega(r) &= \frac{F_\omega}{8\alpha^2 m_s} \left[H_0^{(1)}(k_f r) - H_0^{(1)}(i k_f r) \right] \\
 &= \frac{F_\omega}{8\alpha^2 m_s} \left[H_0^{(1)}(k_f r) - \frac{2i}{\pi} K_0(k_f r) \right]
 \end{aligned}$$

$$H_0^{(1)}(k_r r) \rightarrow \sqrt{\frac{2}{\pi k_r r}} e^{i(k_r r - \pi/4)}$$

Drive-point Impedance

$$Z_p = F_\omega / \dot{w}(0) = 8\alpha^2 m_s$$

Flexural Wave Speed

$$k_f = \omega / c_f$$

$$c_f = \omega / k_f = \alpha \sqrt{\omega}$$



Point Driven Plate

$$D(\theta, \phi) = -\frac{i\rho\omega}{2\pi} \dot{w}_\omega(k \sin\theta)$$

Radiated Pressure

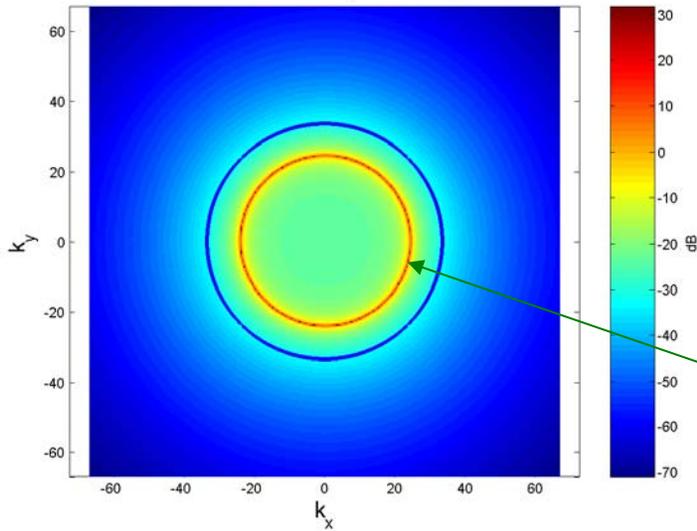
$$p(R, \theta, \phi) = -\frac{i\rho\omega}{2\pi} \frac{e^{ikR}}{R} \dot{w}_\omega(k_r) = -\frac{i\rho\omega}{2\pi} \frac{e^{ikR}}{R} \dot{w}_\omega(k \sin\theta)$$

$$\sin \theta_0 = k_f / k$$

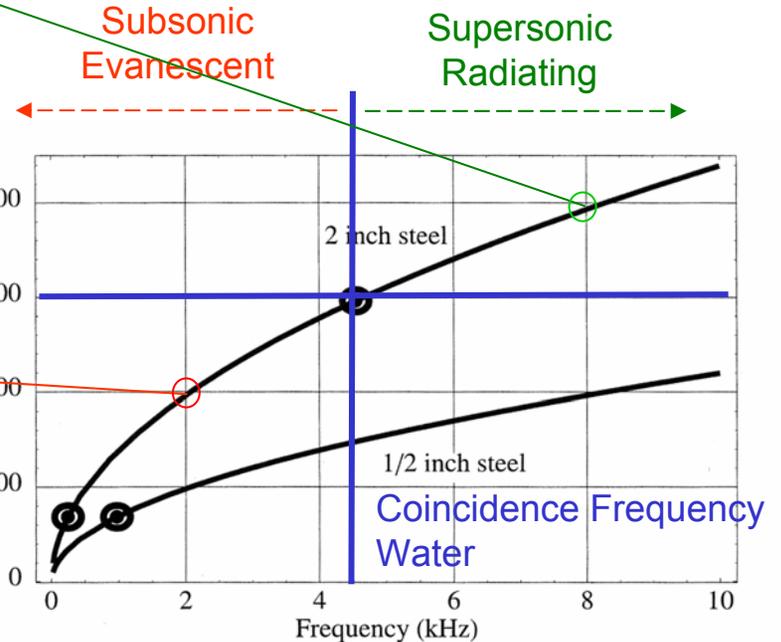
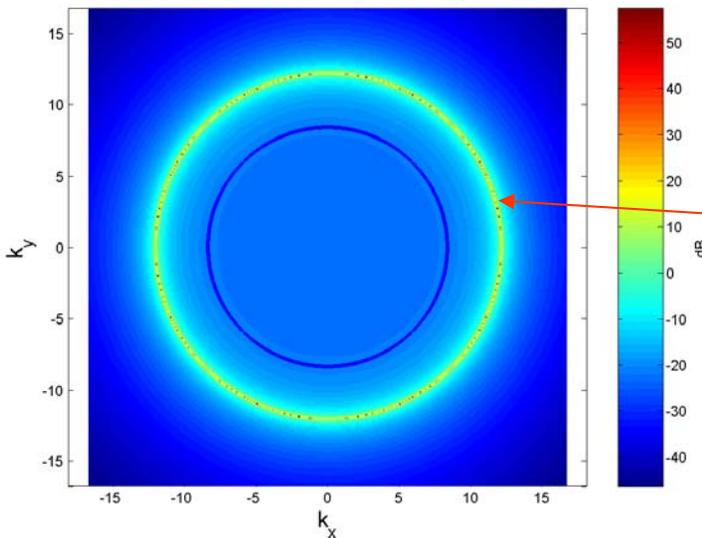
Flexural Wave Speed

$$c_f = \omega / k_f = \alpha \sqrt{\omega}$$

Point Driven LFL-Plate, h = 0.05, f = 8000



Point Driven LFL-Plate, h = 0.05, f = 2000





Point-Driven Plate Radiation Exact Formulation

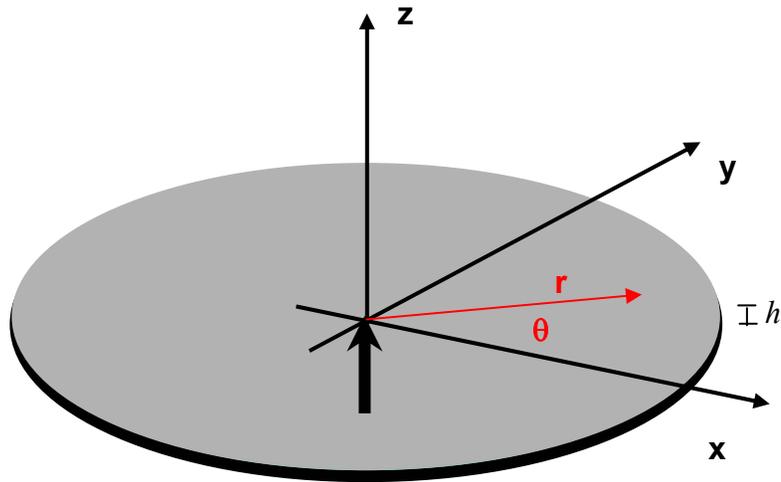


Plate Equation of Motion

$$D \left(\frac{d^2}{dr^2} + \frac{d}{rdr} \right)^2 w_\omega - \rho_s h \omega^2 w_\omega = F_\omega \frac{\delta(r)}{2\pi r} - p_a(r)$$

Fourier Transform

$$D \nabla^4 w_\omega(k_r) - \rho_s h \omega^2 w_\omega(k_r) = F_\omega - p_\omega(k_r)$$

$$p_\omega(k_r) = \frac{\rho \omega}{k_z} \dot{w}_\omega(k_r) = \frac{-i \rho \omega^2}{k_z} w_\omega(k_r)$$

$$D \nabla^4 w_\omega(k_r) - [\rho_s h + i \rho k_z^{-1}] \omega^2 w_\omega(k_r) = F_\omega$$

Vertical Plate Displacement

$$w_\omega(k_r) = \frac{F(\omega)}{2\pi D [k_r^4 - k_f^4(k_r)]}$$

$k_r < k$: Radiation Damping
 $k_r > k$: Added Mass

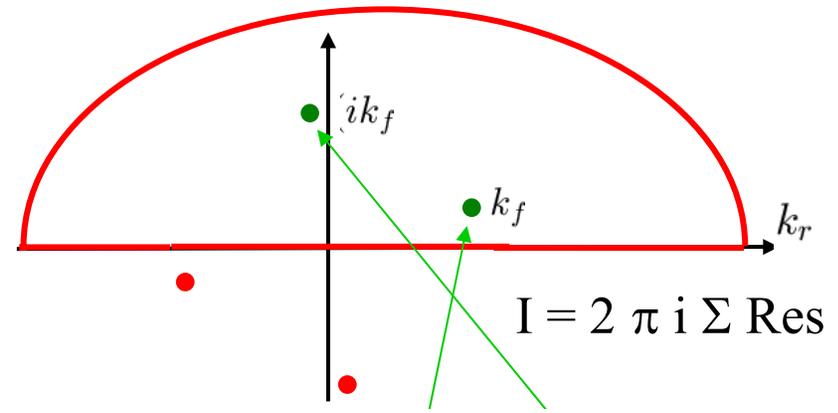
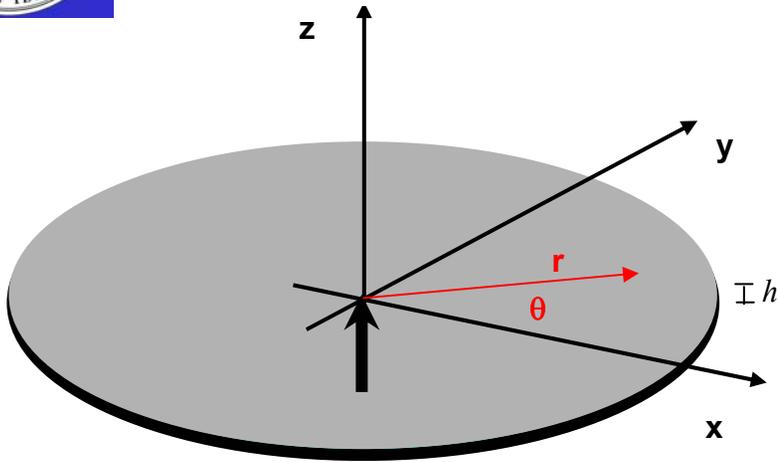
$$k_f(k_r) = \left(\frac{(m_s + i m_a(k_r)) \omega^2}{D} \right)^{1/4} = \left(\frac{(\rho_s h + i \rho k_z^{-1}) \omega^2}{D} \right)^{1/4}$$

Vertical Plate Velocity

$$\dot{w}_\omega(k_r) = \frac{-i \omega F_\omega}{2\pi D [k_r^4 - k_f^4(k_r)]}$$



Point-driven Fluid-loaded Plate Exact Formulation



Complex Contour Integration

Inverse Hankel Transform

$$\begin{aligned} \dot{w}_\omega(r) &= \frac{-i\omega F_\omega}{2\pi D} \int_0^\infty \frac{J_0(k_r r)}{k_r^4 - k_f^4(k_r)} k_r dk_r \\ &= \frac{-i\omega F_\omega}{2\pi D} \int_{-\infty}^\infty \frac{H_0^{(1)}(k_r r)}{k_r^4 - k_f^4(k_r)} k_r dk_r \end{aligned}$$

$$\begin{aligned} \dot{w}_\omega(r) &= \frac{F_\omega}{8\alpha^2 m_s} \left[H_0^{(1)}(k_f r) - H_0^{(1)}(ik_f r) \right] \\ &= \frac{F_\omega}{8\alpha^2 m_s} \left[H_0^{(1)}(k_f r) - \frac{2i}{\pi} K_0(k_f r) \right] \end{aligned}$$

$$H_0^{(1)}(k_r r) \rightarrow \sqrt{\frac{2}{\pi k_r r}} e^{i(k_r r - \pi/4)}$$

Flexural Wavenumber Equation

$$k_f = \left(\frac{(m_s + im_a(k_f))\omega^2}{D} \right)^{1/4} = \left(\frac{(\rho_s h + i\rho(k^2 - k_f^2)^{-1/2})\omega^2}{D} \right)^{1/4}$$

Directivity Function

$$D_\omega(\theta, \phi) = -\frac{\rho\omega}{2\pi} \dot{w}_\omega(k_r) = \frac{-\rho\omega^2 F_\omega}{4\pi^2 D [k_r^4 - k_f^4(k_r)]}$$



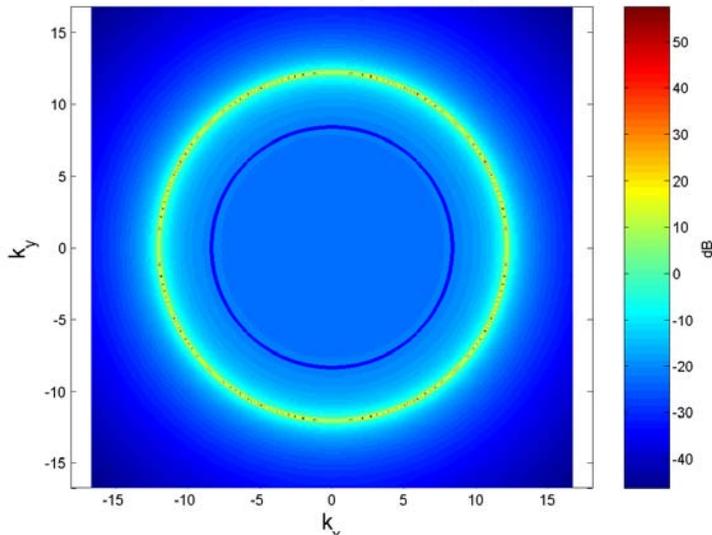
Point-driven Plate Evanescent Frequency Regime

Light Fluid Loading

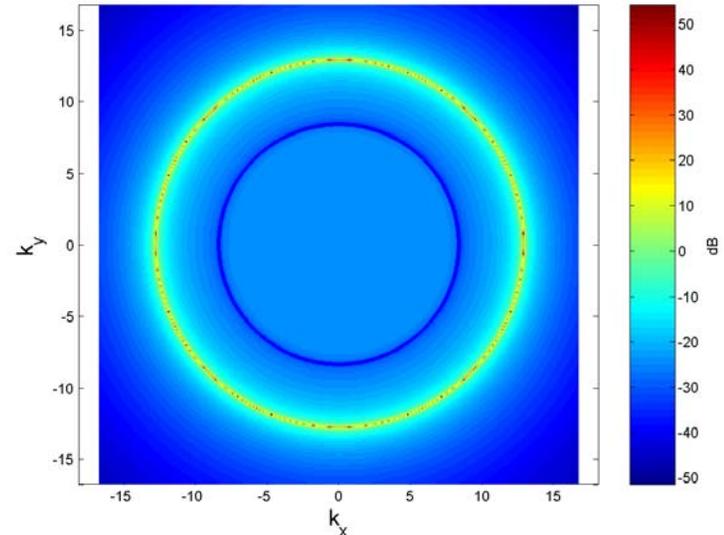
2 kHz

Exact

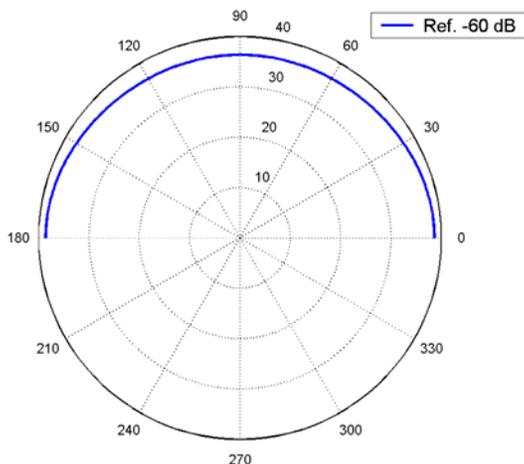
Point Driven LFL-Plate, $h = 0.05$, $f = 2000$



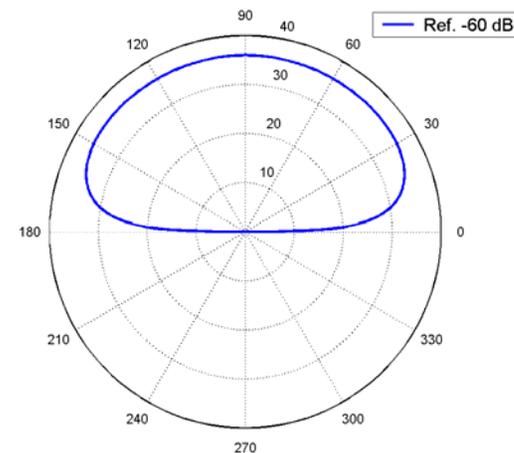
Point Driven Plate, $h = 0.05$, $f = 2000$



Point Driven LFL-Plate, $h = 0.05$, $f = 2000$



Point Driven Plate, $h = 0.05$, $f = 2000$





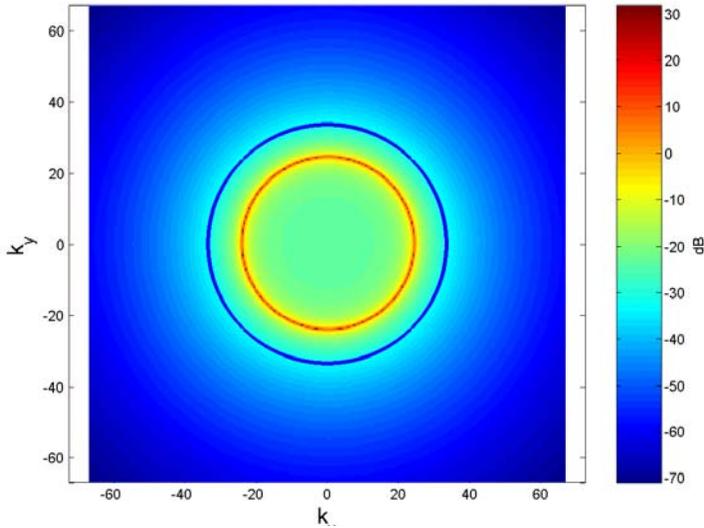
Point-driven Plate Radiation Frequency Regime 8 kHz

Light Fluid Loading

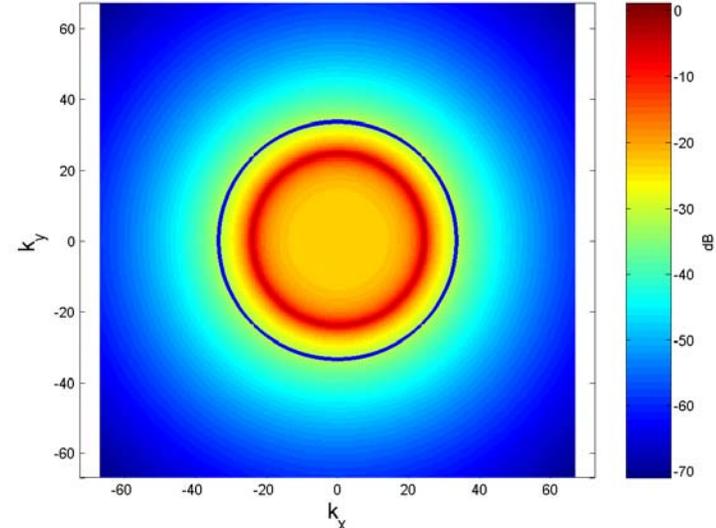
8 kHz

Exact

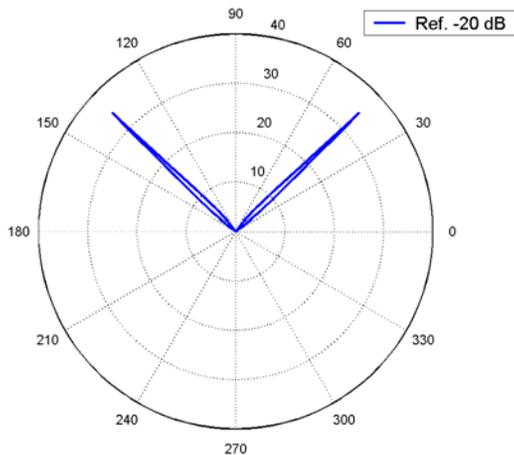
Point Driven LFL-Plate, $h = 0.05$, $f = 8000$



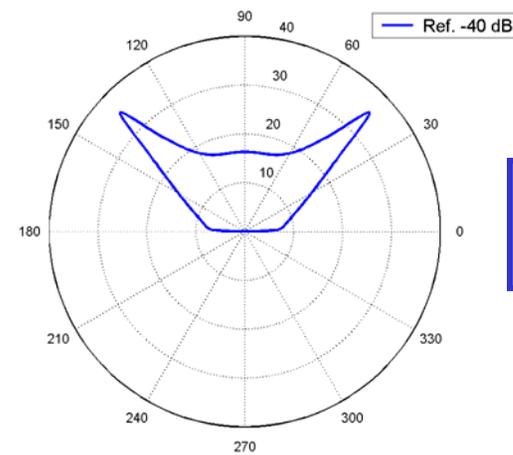
Point Driven Plate, $h = 0.05$, $f = 8000$



Point Driven LFL-Plate, $h = 0.05$, $f = 8000$



Point Driven Plate, $h = 0.05$, $f = 8000$



Radiation Damping



```
% MATLAB script for plotting the directivity function for
% a pointdriven elastic plate
%
% Parameters:
% f      Frequency
% rho    Density
% c      Speed of Sound
% h      Plate thickness
% E      Young's modulus
% nu     Poisson's ratio
% rhos   Plate density
clear
rhos=7700;
cp=5600;
h=0.05;
E=rhos*cp^2;
nu=0.33;
D= E *h^3/(12*(1-nu^2));
rho=1000;
c=1500;
f=8000;
omega=2*pi*f;
k=omega/c;
ka=k;
figure(1);
hold off
kxm=2*ka;
nkx=300;
dkx=2*kxm/(nkx-1);
x=[-kxm:dkx:kxm];
y=x;
o=ones(1,nkx);
kx=x' * o;
ky=(y' *o)';
kr=abs(complex(kx,ky));
kfa= ( (rhos*h+i*rho./sqrt(k^2-complex(kr,0.0).^2))*omega^2/D).^0.25;
kfa=kf*a;
ss=-rho*omega^2./(D*(2*pi)^2 *(complex(kr,0).^4 -kfa.^4));
wavei(dba(ss)',x,y)
shading('flat')
axis('equal')
b=xlabel('k_x')
set(b,'FontSize',16);
b=ylabel('k_y')
set(b,'FontSize',16);
tit=['Point Driven Plate, h = ' num2str(h) ', f = ' num2str(f)]
b=title(tit);
set(b,'FontSize',20);
nphi=361;
dphi=2*pi/(nphi-1);
phi=[0:dphi:2*pi];
xx=k*a*cos(phi);
yy=k*a*sin(phi);
hold on
b=plot(xx,yy,'b');
```

plate.m

```
figure(2)
nphi=361.
dphi=2*pi/(nphi-1)
nth=181;
dth=0.5*pi/(nth-0.5);

phi=[0:dphi:(nphi-1)*dphi]' * ones(1,nth);
th=([dth/2:dth:pi/2]'*ones(1,nphi))';
kx=ka*sin(th).*cos(phi);
ky=ka*sin(th).*sin(phi);
kr=ka*sin(th);
kf= ( (rhos*h+i*rho./sqrt(k^2-complex(kr,0.0).^2))*omega^2/D).^0.25;
kfa=kf*a;

ss=-rho*omega^2./(D*(2*pi)^2 *(complex(kr,0).^4 -kfa.^4));

ss=dba(ss);
sm=10.0*(ceil(0.1*max(max(ss)))));
for i=1:size(ss,1)
    for j=1:size(ss,2)
        ss(i,j)=max(ss(i,j),sm-40.0)-(sm-40.0);
    end
end

xx=ss.*sin(th).*cos(phi);
yy=ss.*sin(th).*sin(phi);
zz=ss.*cos(th);

surfl(xx,yy,zz);
colormap('copper');
shading('flat');
axis('equal');
tit=['Point Driven Plate, h = ' num2str(h) ', f = '
    num2str(omega/(2*pi)) ]

b=title(tit);
set(b,'FontSize',20);

figure(3)
b=polar([pi/2-fliplr(th(1,:)) pi/2+th((nphi-1)/2+1,:)],
    [fliplr(ss(1,:)) ss((nphi-1)/2+1,:)]);
set(b,'LineWidth',2)
b=legend(['Ref. ' num2str(sm-40.0) ' dB']);
set(b,'FontSize',14);

tit=['Point Driven Plate, h = ' num2str(h) ', f = '
    num2str(omega/(2*pi)) ]
b=title(tit);
set(b,'FontSize',20);
```



Simply-supported Elastic Plate

Homogeneous Equation of Motion

$$D \left[\frac{\partial^4 w_\omega}{\partial x^4} + 2 \frac{\partial^4 w_\omega}{\partial x^2 \partial y^2} + \frac{\partial^4 w_\omega}{\partial y^4} \right] - \rho_s h \omega^2 w_\omega = 0$$

$$\nabla^4 w_\omega(x, y) - k_f^4 w_\omega(x, y) = 0$$

$$k_f = (\rho_s h \omega^2 / D)^{1/4} = \frac{\omega}{\alpha}$$

Moments

$$M_x = -D \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right)$$

$$M_y = -D \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right)$$

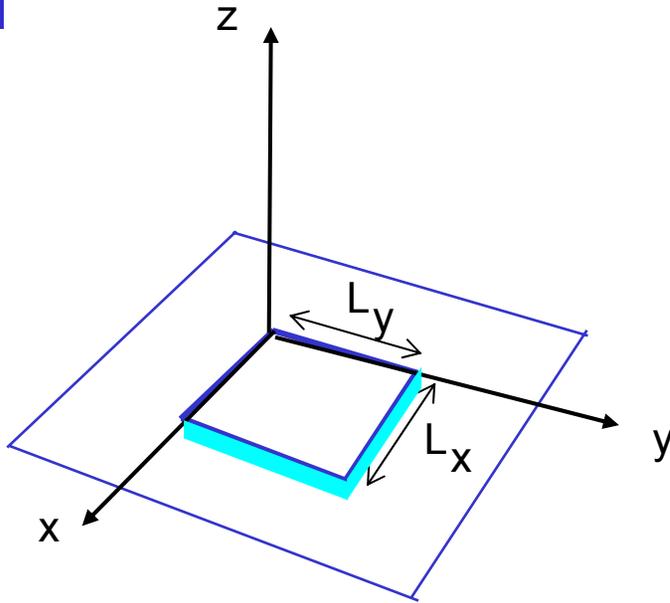
Boundary Conditions

$$w(x, y), M_x(x, y) = 0, \quad x = 0, L_x$$

$$w(x, y), M_y(x, y) = 0, \quad y = 0, L_y$$

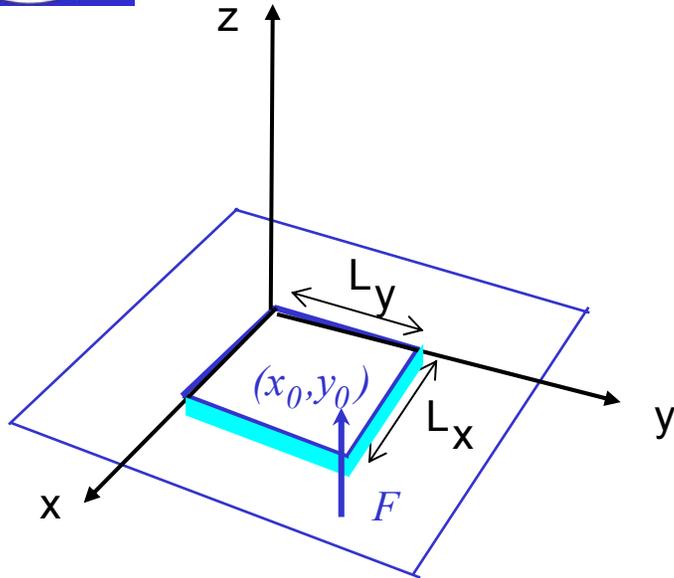
$$w_\omega(x, y), \frac{\partial^2 w_\omega(x, y)}{\partial x^2} \equiv 0, \quad x = 0, L_x$$

$$w_\omega(x, y), \frac{\partial^2 w_\omega(x, y)}{\partial y^2} \equiv 0, \quad y = 0, L_y$$





Point-driven Rectangular Elastic Plate



Homogeneous Equation of Motion

$$\nabla^4 w_\omega(x, y) - k_f^4 w_\omega(x, y) = 0$$

$$k_f = (\rho_s h \omega^2 / D)^{1/4} = \frac{\omega}{\alpha}$$

Normal Modes

$$\Phi_{mn}(x, y) = \frac{2}{\sqrt{L_x L_y}} \sin(m\pi x / L_x) \sin(n\pi y / L_y), \quad m, n = 1, 2, 3 \dots$$

Solutions for

$$(m\pi / L_x)^2 + (n\pi / L_y)^2 = k_f^2$$

Orthogonality Relation

$$\int_0^{L_x} \int_0^{L_y} \Phi_{mn}(x, y) \Phi_{pq}(x, y) dx dy = \delta_{mp} \delta_{nq}$$

Dispersion Relation

$$\omega_{mn} = \alpha^2 [(m\pi / L_x)^2 + (n\pi / L_y)^2]$$

Light Fluid Loading

$$D [\nabla^4 w_\omega(x, y) - k_f^4 w_\omega(x, y)] = F_\omega \delta(x - x_0) \delta(y - y_0) - p_\omega(x, y, 0)$$

$$w_\omega(x, y) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn}(\omega) \Phi_{mn}(x, y)$$

$$D \nabla^4 \Phi_{mn}(x, y) = \rho_s h \omega_{mn} \Phi_{mn}(x, y)$$

$$\rho_s h (\omega_{mn}^2 - \omega^2) A_{mn} = \int_0^{L_x} \int_0^{L_y} \Phi_{mn}(x, y) F_\omega \delta(x - x_0) \delta(y - y_0) dx dy = F_\omega \Phi_{mn}(x_0, y_0)$$

Normal Mode Solution

$$w_\omega(x, y) = -\frac{F_\omega}{\rho_s h} \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{\Phi_{mn}(x_0, y_0) \Phi_{mn}(x, y)}{\omega^2 - \omega_{mn}^2}$$

Transfer Mobility

$$Y_\omega = \frac{\dot{w}(x, y)}{F_\omega} = \frac{i\omega}{\rho_s h} \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{\Phi_{mn}(x_0, y_0) \Phi_{mn}(x, y)}{\omega^2 - \omega_{mn}^2}$$

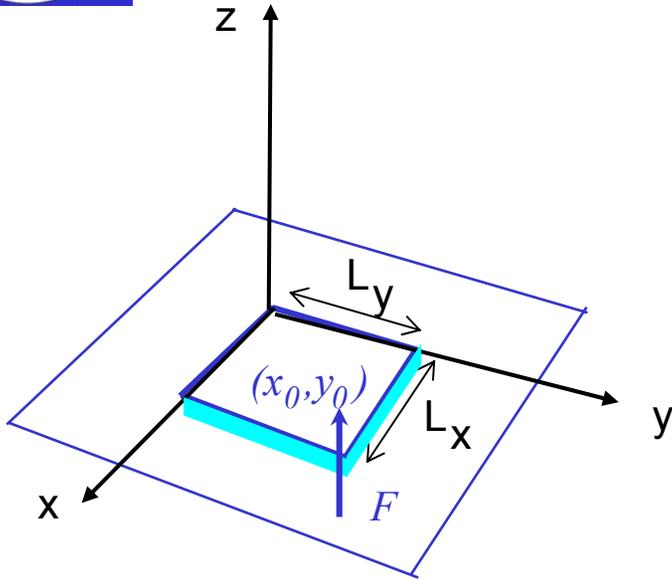


Normal Modes of Simply-supported Elastic Plate

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See Figure 2.26 in Williams, E. G. *Fourier Acoustics*.
London: Academic Press, 1999



Radiation from Point-driven Elastic Plate



$$\Phi_{mn}(x, y) = \frac{2}{\sqrt{L_x L_y}} \sin(k_{xm}x) \sin(k_{yn}y), \quad m, n = 1, 2, 3 \dots$$

$$k_{xm} = m\pi/L_x$$

$$k_{yn} = n\pi/L_y$$

$$k_{xm}^2 + k_{yn}^2 = k_f^2$$

$$\dot{w}_\omega(x, y) = \frac{i\omega \Pi((x - L_x/2)/L_x) \Pi((y - L_y/2)/L_y)}{2\sqrt{L_x L_y}}$$

$$\times \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn}(\omega) (e^{ik_{xm}x} - e^{-ik_{xm}x}) (e^{ik_{yn}y} - e^{-ik_{yn}y})$$

Fourier Transforms

$$\begin{aligned} & \int_{-\infty}^{\infty} \Pi((x - L_x/2)/L_x) e^{\pm ik_{xm}x} e^{-ik_x x} dx \\ &= \left[\int_{-\infty}^{\infty} \Pi((x - L_x/2)/L_x) e^{-i(k_x x)} dx \right] * \delta(k_x \mp k_{xm}) \\ &= \left[e^{-ik_x L_x/2} L \text{sinc}(k_x L_x/2) \right] * \delta(k_x \mp k_{xm}) \\ &= e^{-i(k_x \mp k_{xm})L/2} L \text{sinc}((k_x \mp k_{xm})L/2) \end{aligned}$$

$$\begin{aligned} \dot{w}_\omega(k_x, k_y) &= \frac{i\omega \sqrt{L_x L_y}}{2} \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn}(\omega) \left[\pm e^{-i(k_x \mp k_{xm})L_x/2} \text{sinc}\left(\frac{(k_x \mp k_{xm})L_x}{2}\right) \right] \\ &\quad \times \left[\pm e^{-i(k_y \mp k_{yn})L_y/2} \text{sinc}\left(\frac{(k_y \mp k_{yn})L_y}{2}\right) \right] \end{aligned}$$

Directivity Function

$$\begin{aligned} D_\omega(\theta, \phi) &= -\frac{i\rho\omega}{2\pi} \dot{w}(k_x, k_y) \\ &= \frac{\rho\omega^2 \sqrt{L_x L_y}}{4\pi} \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn}(\omega) \left[\pm e^{-i(k_x \mp k_{xm})L_x/2} \text{sinc}\left(\frac{(k_x \mp k_{xm})L_x}{2}\right) \right] \\ &\quad \times \left[\pm e^{-i(k_y \mp k_{yn})L_y/2} \text{sinc}\left(\frac{(k_y \mp k_{yn})L_y}{2}\right) \right] \end{aligned}$$



Radiation Efficiency

Low-order Modes – Square Plate

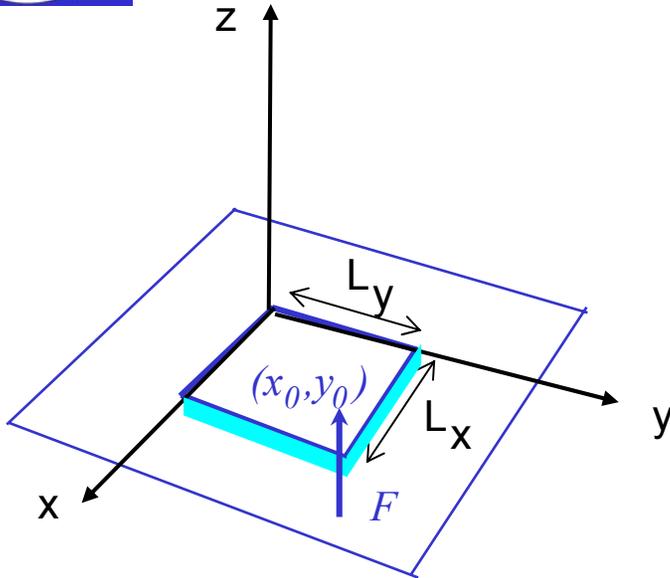


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See Figure 2.27 in [Williams].

Radiation Efficiency

$$S \equiv \frac{\Pi}{\Pi_0} \equiv \frac{\Pi}{\frac{1}{2}\rho c L_x L_y \langle |\dot{w}|^2 \rangle}$$

RMS Velocity

$$\langle |\dot{w}|^2 \rangle \equiv \frac{1}{L_x L_y} \int_0^{L_x} \int_0^{L_y} |\dot{w}(x, y)|^2 dx dy$$

Mode m,n

$$S_{mn} = \frac{\Pi}{\frac{1}{2}\rho c L_x L_y \langle |\dot{w}_{mn}|^2 \rangle}$$

$$k/k_f$$



Radiation Efficiency

High-order Modes – Square Plate

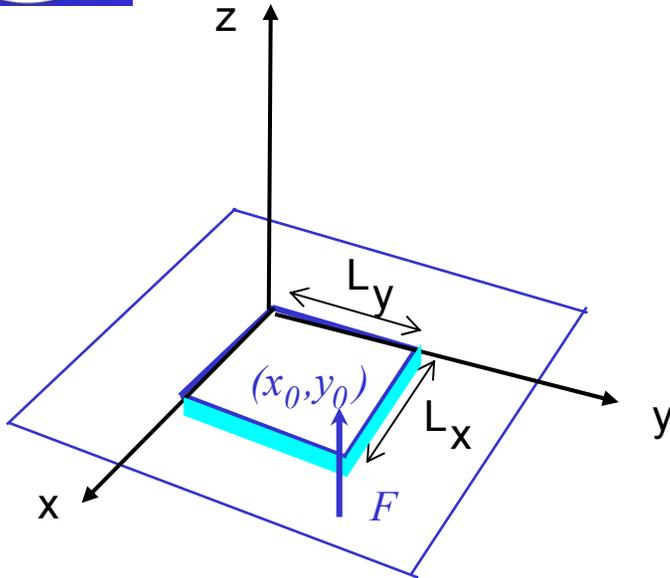


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See Figure 2.28 in [Williams].

Radiation Efficiency

$$S \equiv \frac{\Pi}{\Pi_0} \equiv \frac{\Pi}{\frac{1}{2}\rho c L_x L_y \langle |\dot{w}|^2 \rangle}$$

RMS Velocity

$$\langle |\dot{w}|^2 \rangle \equiv \frac{1}{L_x L_y} \int_0^{L_x} \int_0^{L_y} |\dot{w}(x, y)|^2 dx dy$$

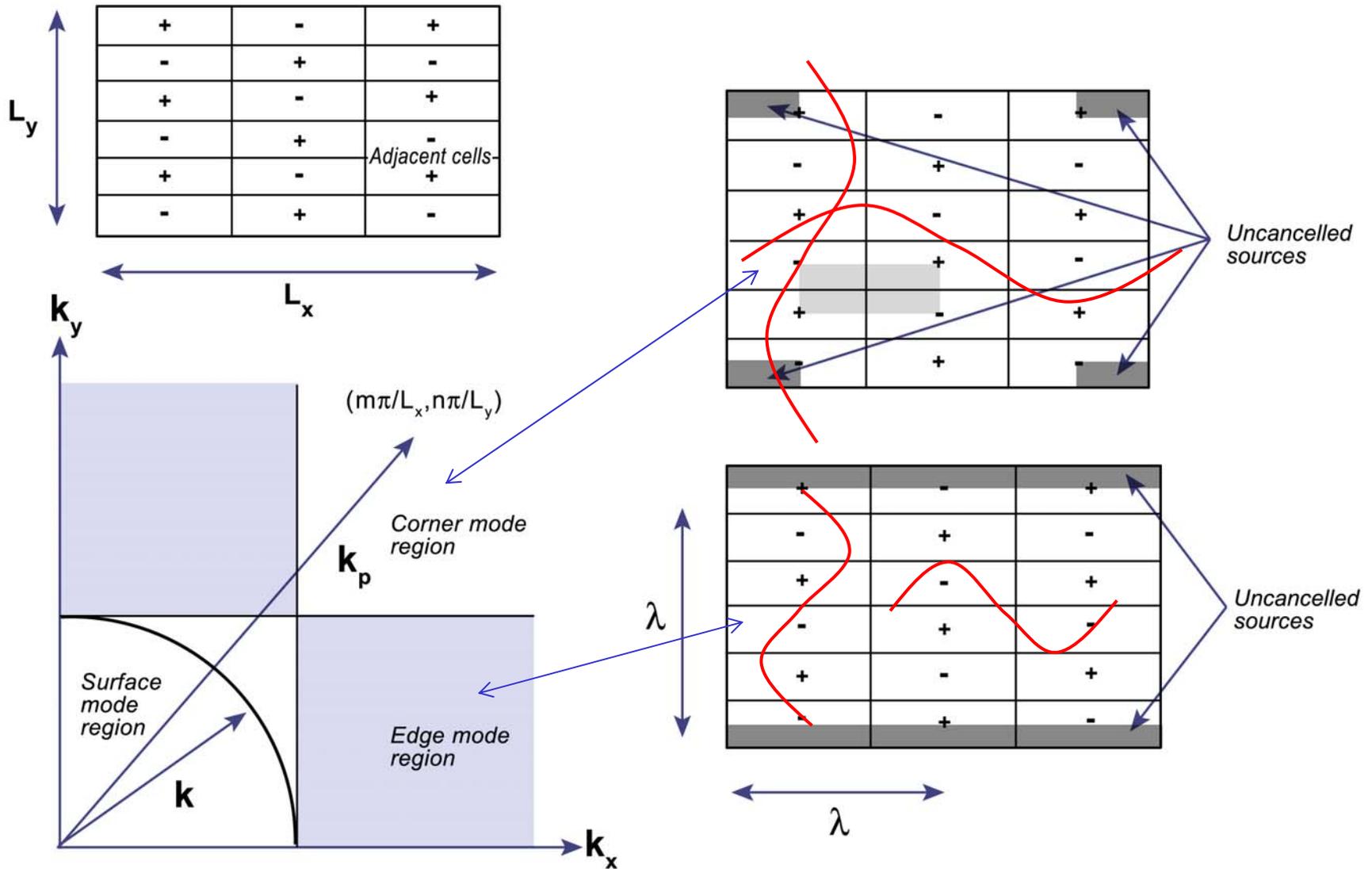
Mode m,n

$$S_{mn} = \frac{\Pi}{\frac{1}{2}\rho c L_x L_y \langle |\dot{w}_{mn}|^2 \rangle}$$

$$k/k_f$$



Rectangular Elastic Plate Radiation Mode Types





Rectangular Elastic Plate Radiation Mode Excitation

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See Figure 2.34 in [Williams].



Rectangular Elastic Plate Radiation Supersonic Intensity

$$M,n = 11,9 - kL/2 = 1 - k/k_f = 0.27$$

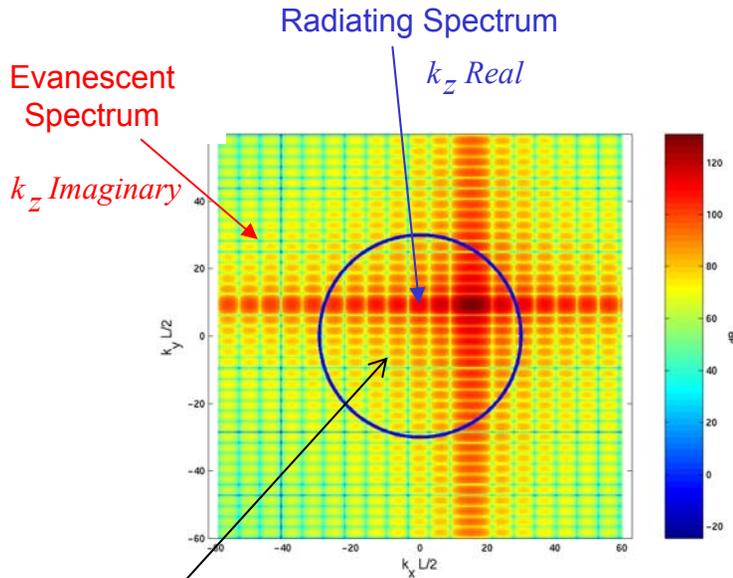


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See Figure 2.37 in [Williams].

Supersonic Intensity

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See Figure 2.38 in [Williams].

$$\Pi_{\omega}^{(s)}(x, y) = \frac{1}{2} \text{Re}[p_{\omega}^{(s)}(x, y) \dot{w}_{\omega}^{(s)}(x, y)^*]$$

Normal Acoustic Intensity

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See Figure 2.39 in [Williams].