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2.72 Elements of Mechanical Design  
Spring 2009

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*2.72*

*Elements of  
Mechanical Design*

*Lecture 03: Shafts*

# Schedule and reading assignment

## Reading quiz

## Hand forward lathe exercise quiz

## Topics

- ❑ Finish matrices, errors
- ❑ Shaft displacements
- ❑ Stiffness exercise

## Reading assignment

- ❑ Shigley/Mischke
  - *Sections 6.1–6.4: 10ish pages & Sections 6.7–6.12: 21ish pages*
  - *Pay special attention to example 6.12 (modified Goodman portion)*

*Deflection within  
springs and shafts*

# Shafts, axles and rails

## Shafts

- ❑ Rotating, supported by bearings/bushings
- ❑ Dynamic/fluctuating analysis

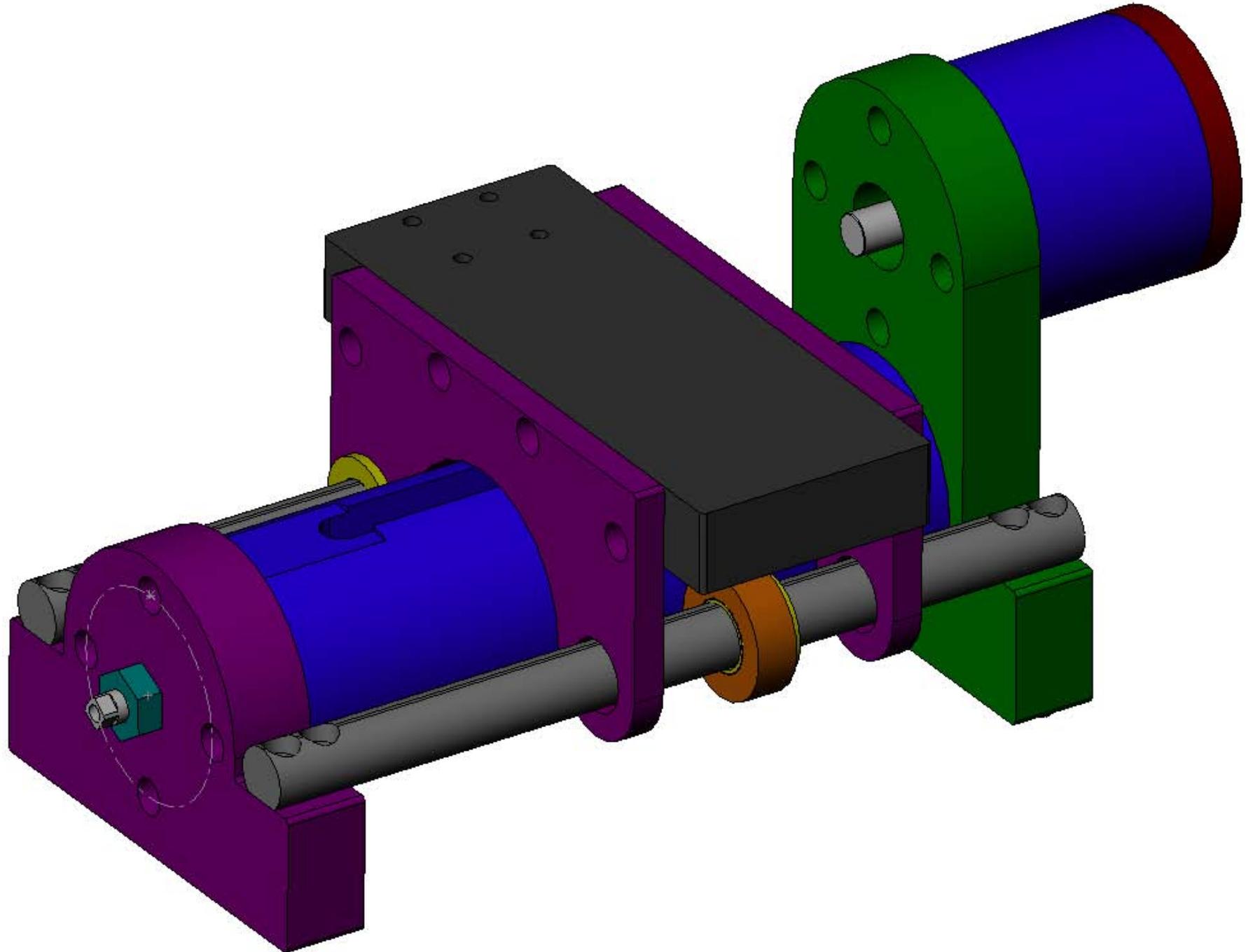
## Axles

- ❑ Non-rotating, supported by bearings/bushings
- ❑ Static analysis

## Rails

- ❑ Non-rotating, supports bearings/bushings
- ❑ Static analysis

# Examples drawn from your lathe





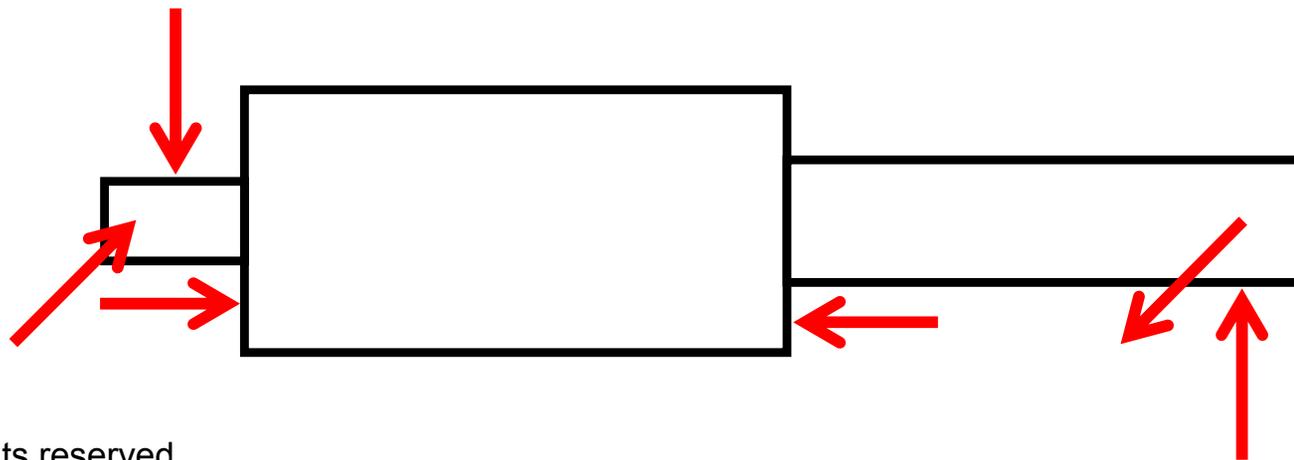
# In practice, we are concerned with

## Deflection

- ❑ Stiffness
- ❑ Bearings and stiffness of connectivity points
- ❑ Function of global shaft geometry, sometimes adjacent components

## Stress

- ❑ Catastrophic failure:      Ductile                      Brittle                      Fatigue
- ❑ Function of local shaft geometry



# What is of concern?

## Deflection and stiffness

- ❑ Beam bending models
- ❑ Superposition

## Load and stress analysis

- ❑ Bending, shear & principle stresses
- ❑ Endurance limit
- ❑ Fatigue strength
- ❑ Endurance modifiers
- ❑ Stress concentration
- ❑ Fluctuating stresses

## Failure theories

- ❑ Von Mises stress
- ❑ Maximum shear stress

# Materials

## Steel vs. other materials

- ❑ Aluminum
- ❑ Brass
- ❑ Cast iron

## Important properties

- ❑ Modulus                      Yield stress                      Fatigue life                      CTE
- ❑ Is density important?

## Material treatment – Hardening

- ❑ What does hardening do the material properties
- ❑ It is expensive
- ❑ Affects final dimensions
- ❑ You can usually design without this

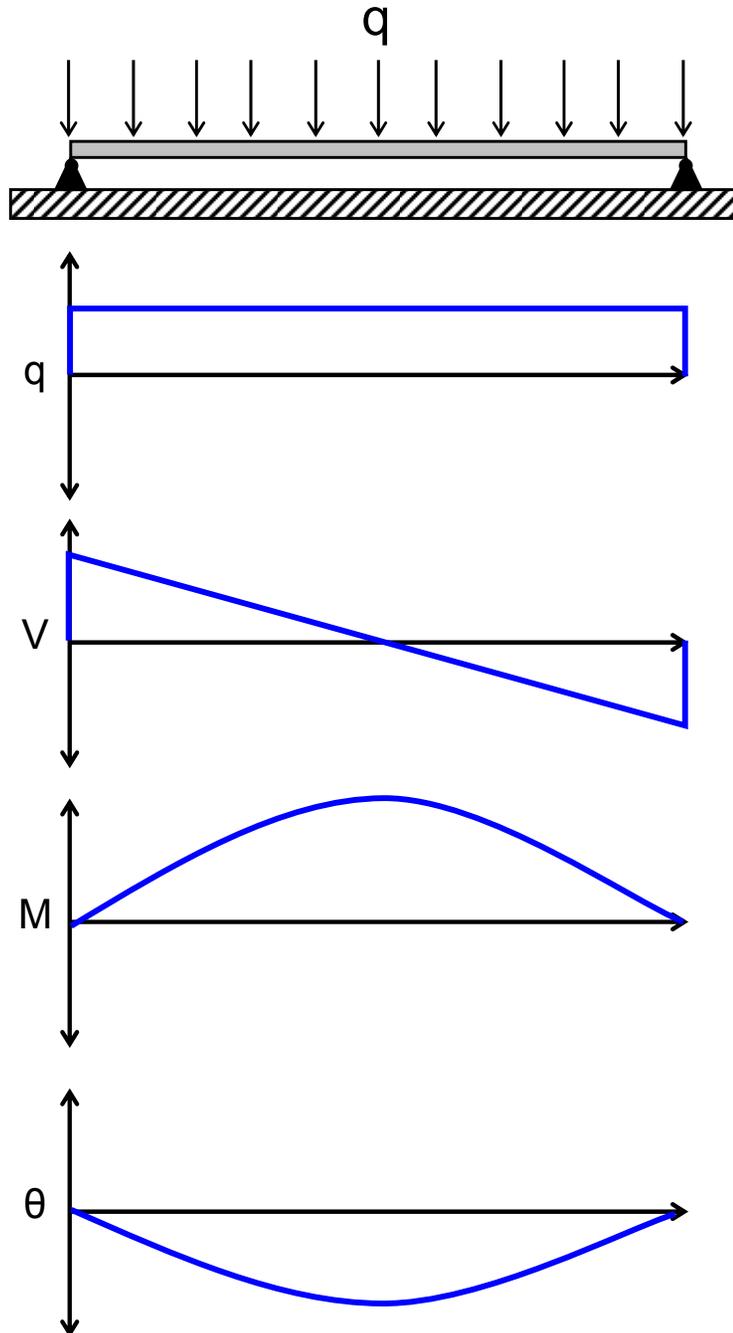
# Principles of stiffness: Relationships

$$\frac{q}{EI} = \frac{d^4 y}{dx^4}$$

$$\frac{V}{EI} = \frac{d^3 y}{dx^3}$$

$$\frac{M}{EI} = \frac{d^2 y}{dx^2}$$

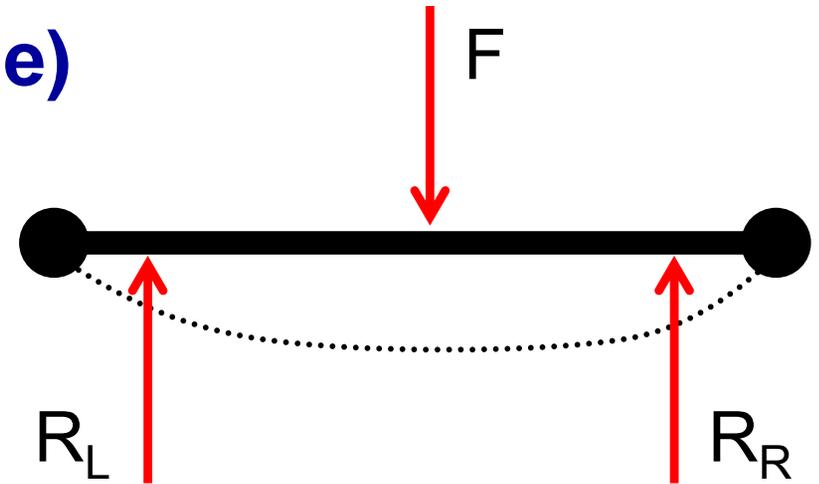
$$\theta = \frac{dy}{dx}$$



# Modeling: General forms of equations

## Lateral bending deflection (middle)

$$\delta = \frac{F L^3}{48 E I} \text{Const} \frac{F L^3}{E I}$$



## Axial deflection

$$\delta = \frac{F L}{A E}$$

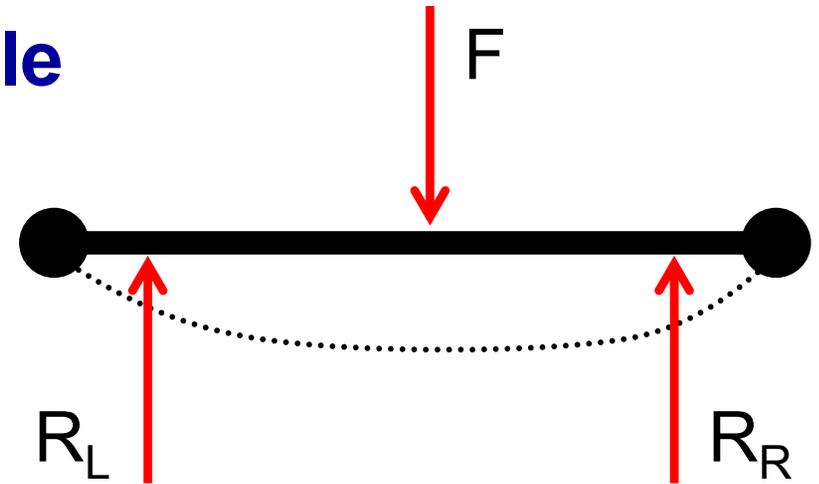
## Lateral bending angles (at ends)

$$\delta = \frac{F L^2}{6 E I} = \frac{F L^2}{\text{Const} E I} \text{ or } \frac{M L}{\text{Const} E I}$$

# Modeling: Stiffness

## Lateral bending stiffness at middle

$$k_b = 48 \frac{(E I)}{L^3} = \text{Const} (E I) L^n$$

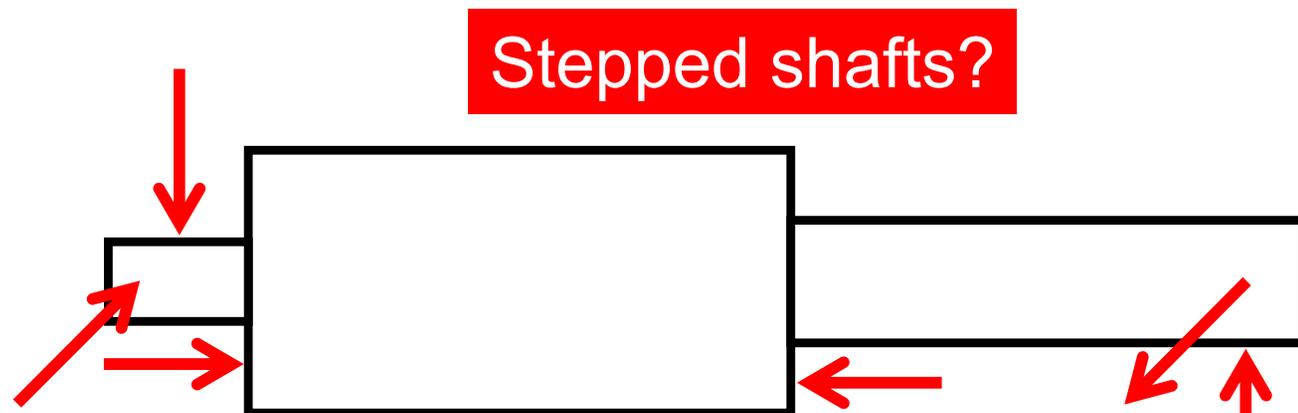


## Axial stiffness

$$k_A = \frac{A E}{L}$$

## Torsional stiffness

$$k_\theta = \frac{J G}{L}$$



# Modeling: Stiffness

These pop up in many places, memorize them

- Square cross section

$$I = \frac{1}{12}bh^3$$

- Circular cross sections

$$I = \frac{\pi}{64} \left[ (d_{outer})^4 - (d_{inner})^4 \right]$$

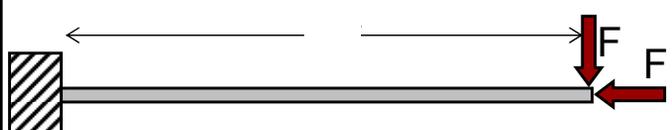
$$J = \frac{\pi}{32} \left[ (d_{outer})^4 - (d_{inner})^4 \right]$$

# Principles of stiffness: Ratios

## Everything deforms

- ❑ Impractical to model the stiffness of everything
- ❑ Mechanical devices modeled as high, medium & low stiffness elements
- ❑ Stiffness ratios show what to model as high-, medium, or low stiffness

## Stiffness ratio


$$R_k = \frac{k_{1st}}{k_{2nd}}$$
$$k_{axial} = \frac{AE}{l}$$
$$k_{lateral} = \frac{3EI}{l^3}$$
$$R_k = \frac{\frac{AE}{l}}{\frac{3EI}{l^3}} = 4 \frac{l^2}{h^2}$$

## Building intuition for stiffness

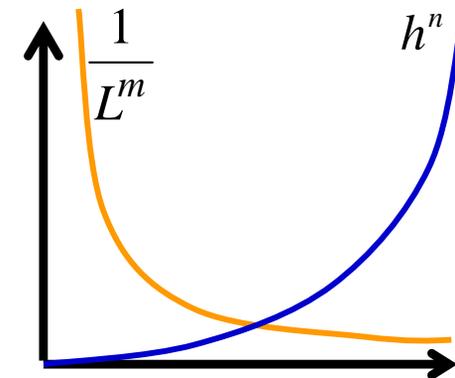
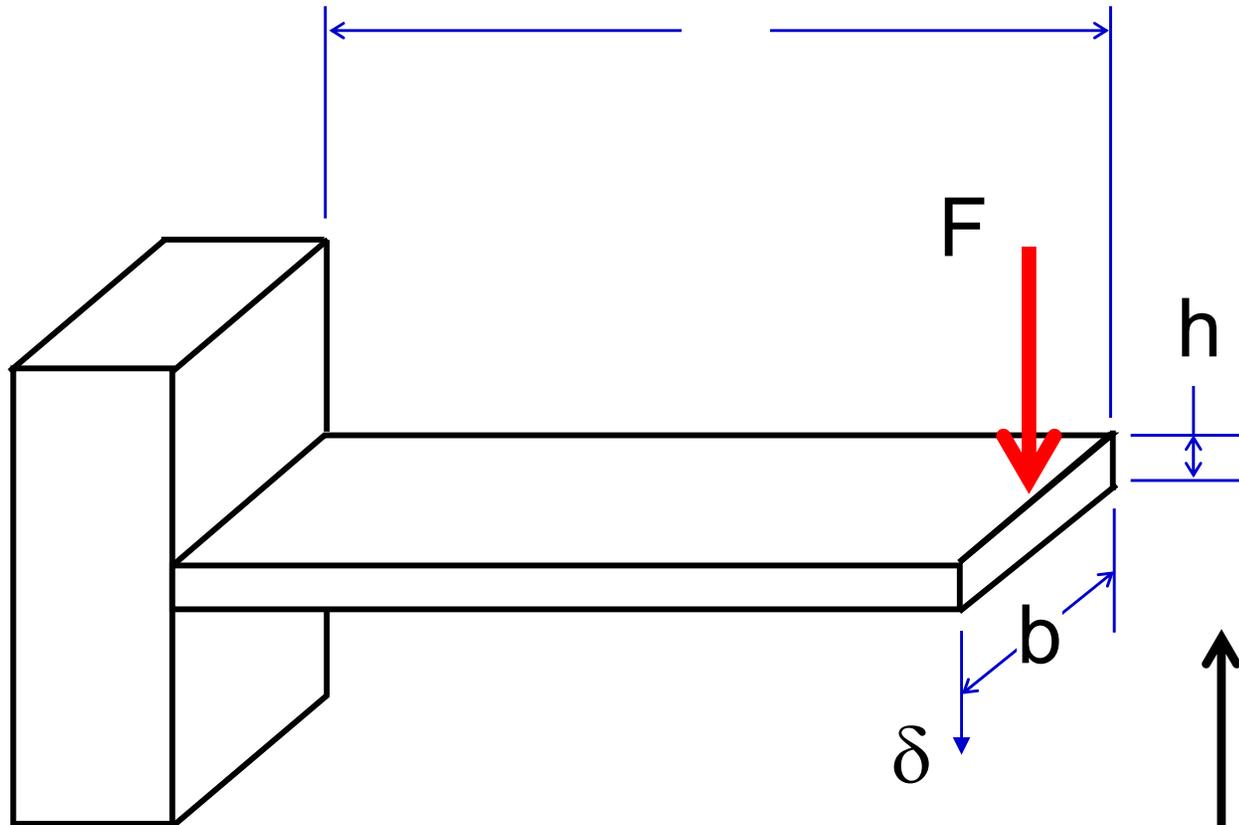
- ❑ You can't memorize/calculate everything
- ❑ Engineers must be reasonable "instruments"
- ❑ Car suspension is easy, but flexed muscle vs. bone?

# Principles of stiffness: Sensitivity

## Cantilever

$$\delta = \frac{F \cdot L^3}{3 \cdot E \cdot I}$$

$$I = \frac{1}{12} \cdot b \cdot h^3$$



$$F = \left( \frac{E \cdot b}{4} \cdot \left[ \frac{h}{L} \right]^3 \right) \cdot \delta$$

$$k = \frac{dF}{d\delta} = \frac{d}{d\delta} \left\{ \frac{E \cdot b}{4} \cdot \left[ \frac{h}{L} \right]^3 \cdot \delta \right\} \rightarrow \frac{E \cdot b}{4} \cdot \left[ \frac{h}{L} \right]^3$$

# Superposition

## You must be careful, following assumptions are needed

- ❑ Cause and effect are linearly related
- ❑ No coupling between loads, they are independent
- ❑ Geometry of beam does not change too much during loading
- ❑ Orientation of loads does not change too much during loading

## Use your head, when $M = 0$ , what is going on

## Superposition is not plug and chug

- ❑ You must visualize
- ❑ You must think

# Types of springs and behaviors

## Springs and stiffness

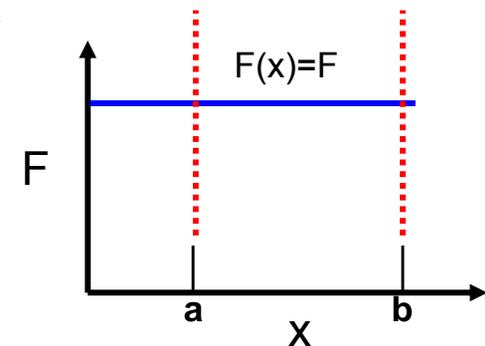
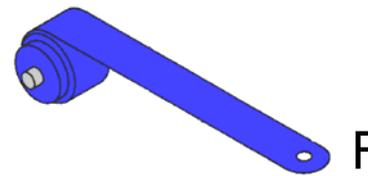
$$\square k_F = \frac{dF(x)}{dx}$$

### Constant force spring

$$\square k_F = \frac{dF(x)}{dx} = 0$$

$$\square \Delta E_{b-a} = F \cdot (x_b - x_a)$$

Force-Displacement Curve →

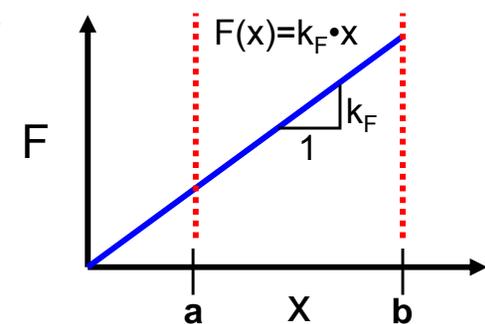
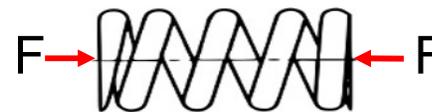


### Constant stiffness spring

$$\square k_F = \text{Constant}$$

$$\square \Delta E_{b-a} = 0.5 \cdot k_F \cdot (x_b^2 - x_a^2)$$

Force-Displacement Curve →

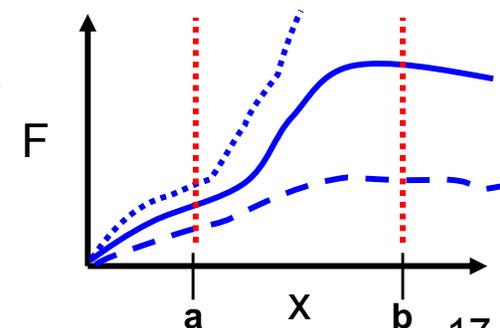
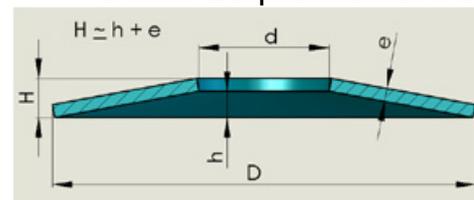


### Non-linear force spring

$$\square k_F = \text{function of } x$$

$$\square \Delta E_{b-a} = \int F(x) \cdot dx$$

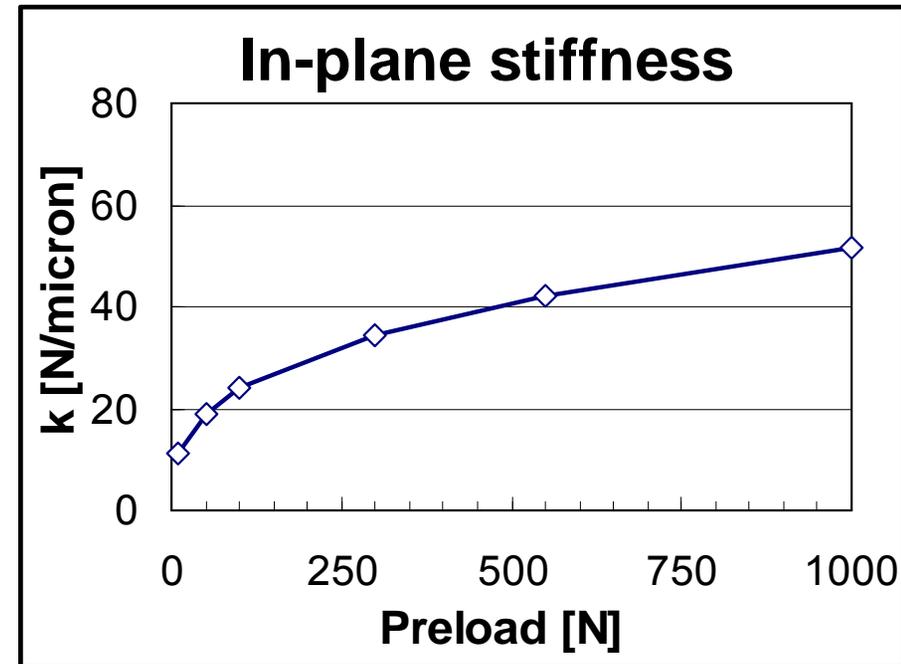
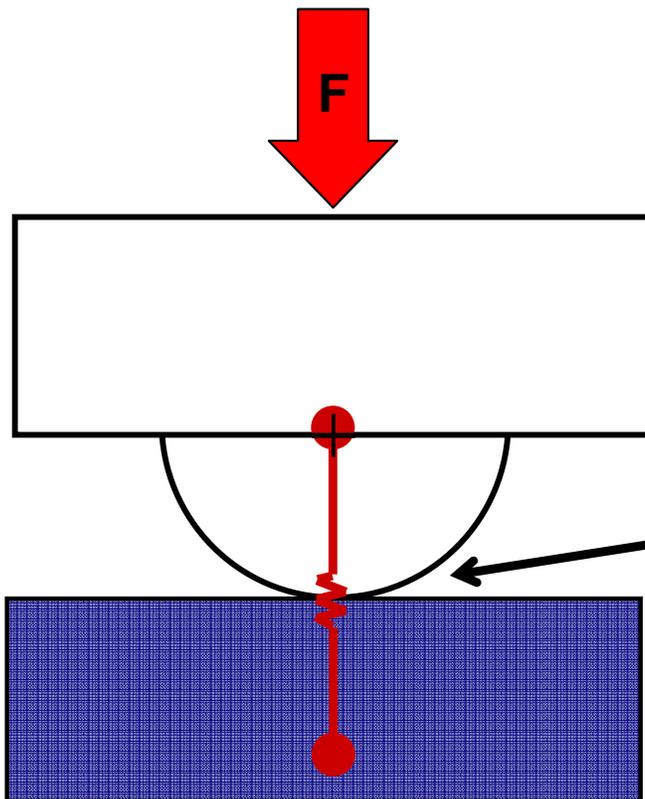
Force-Displacement Curve →



# Non-conformal contact – ball on flat

## Non-conformal contacts often non-linear

- Example: bearings, belleville washers, structural connections
- Is anything ever perfectly conformal?
- Specific case: Hertzian contact



$$k_n(F) = \text{Constant} \cdot \left( R^{1/3} \cdot E^{2/3} \right) \cdot F^{1/3}$$

# Linearization of non-linear springs

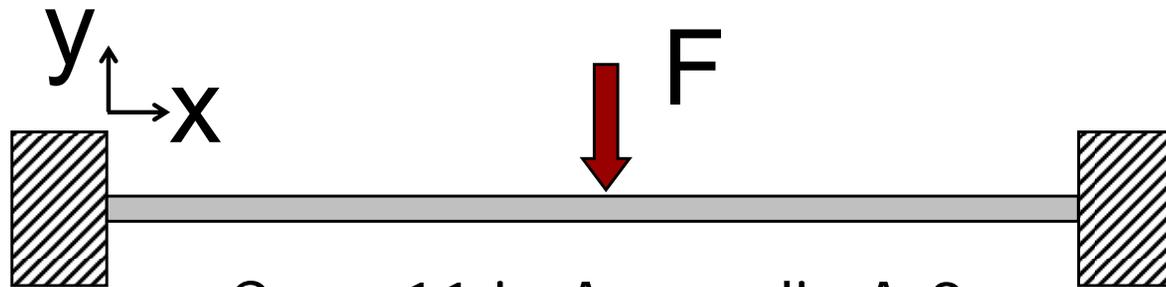
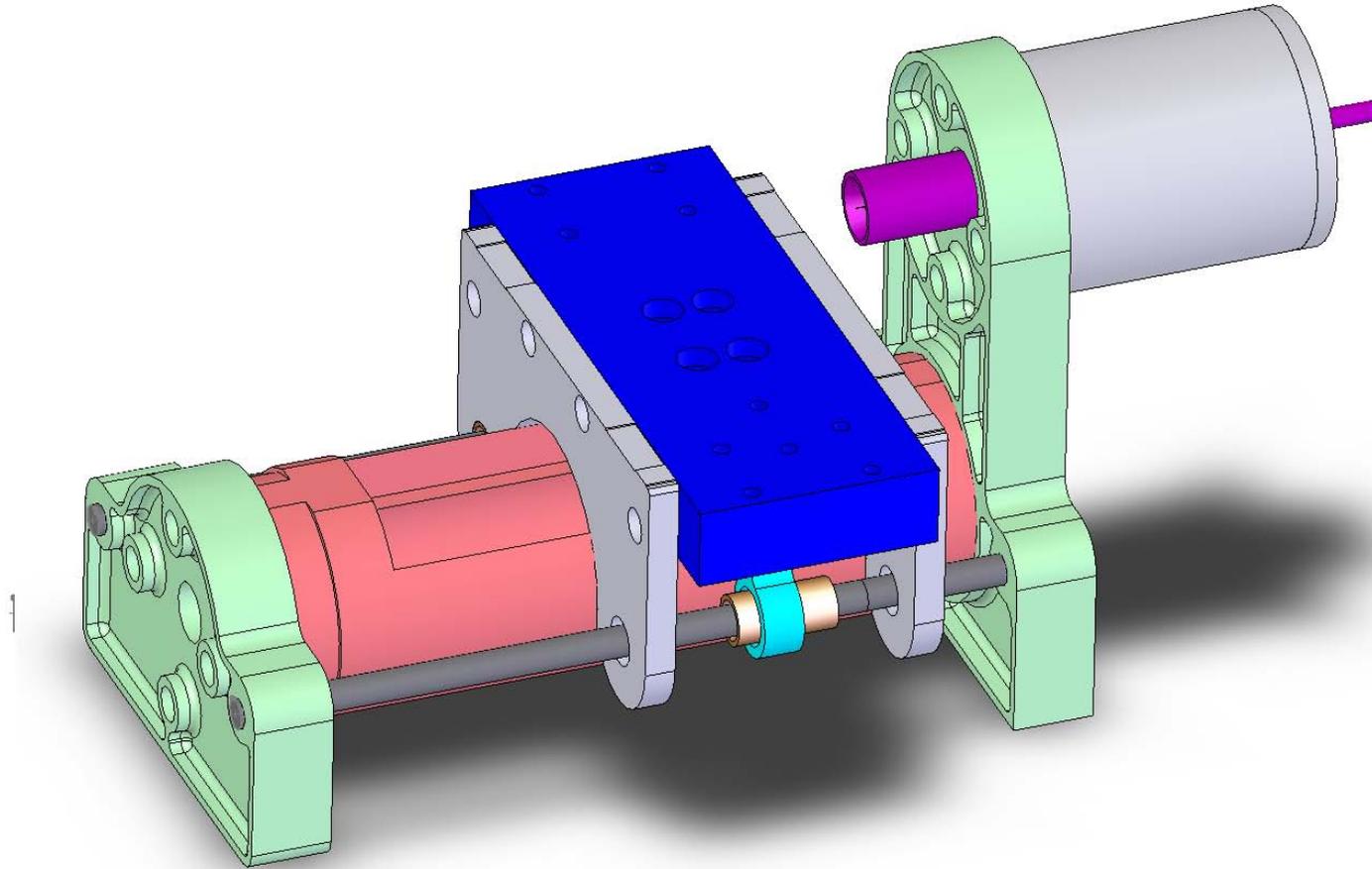
If you can linearize over the appropriate range... then you can use superposition

**So how would, and when could, you do this?**

- ❑  $R$  = ball radius
- ❑  $E$  = modulus of both materials (both steel)
- ❑  $F$  = contact load

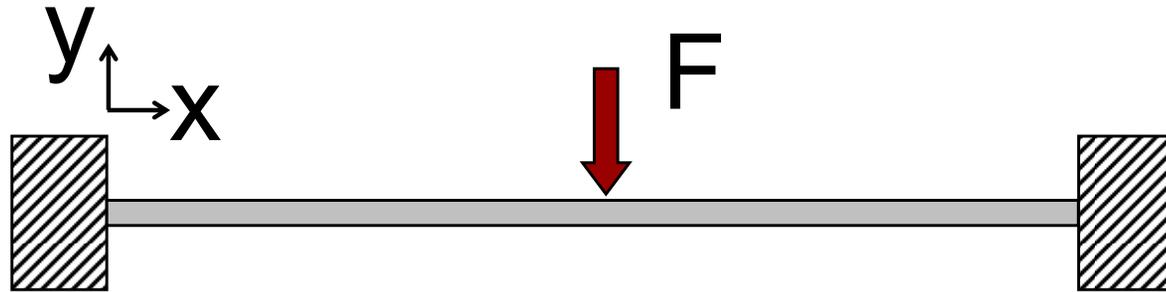
$$\frac{dF}{d\delta} = k_n(F) = \text{Constant} \cdot \left( R^{1/3} \cdot E^{2/3} \right) \cdot F^{1/3}$$

# Practical application to the lathe problem



Case 11 in Appendix A-9

# Practical application to the lathe problem



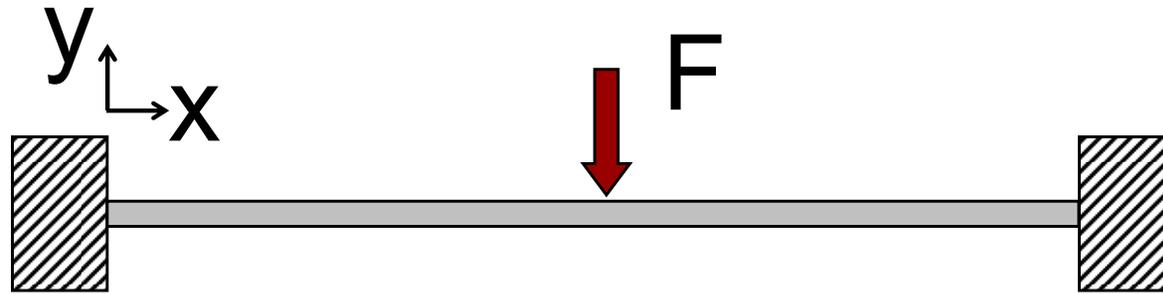
$$y(x)|_{A \rightarrow B} = \frac{1}{96EI} \cdot F \cdot x^2 (11x - 9l)$$

$$y\left(\frac{l}{2}\right) = \frac{1}{96EI} \cdot F \cdot \frac{7}{8} l^3$$

$$k|_{Beam} = \frac{768}{7} \cdot \frac{EI}{l^3}$$

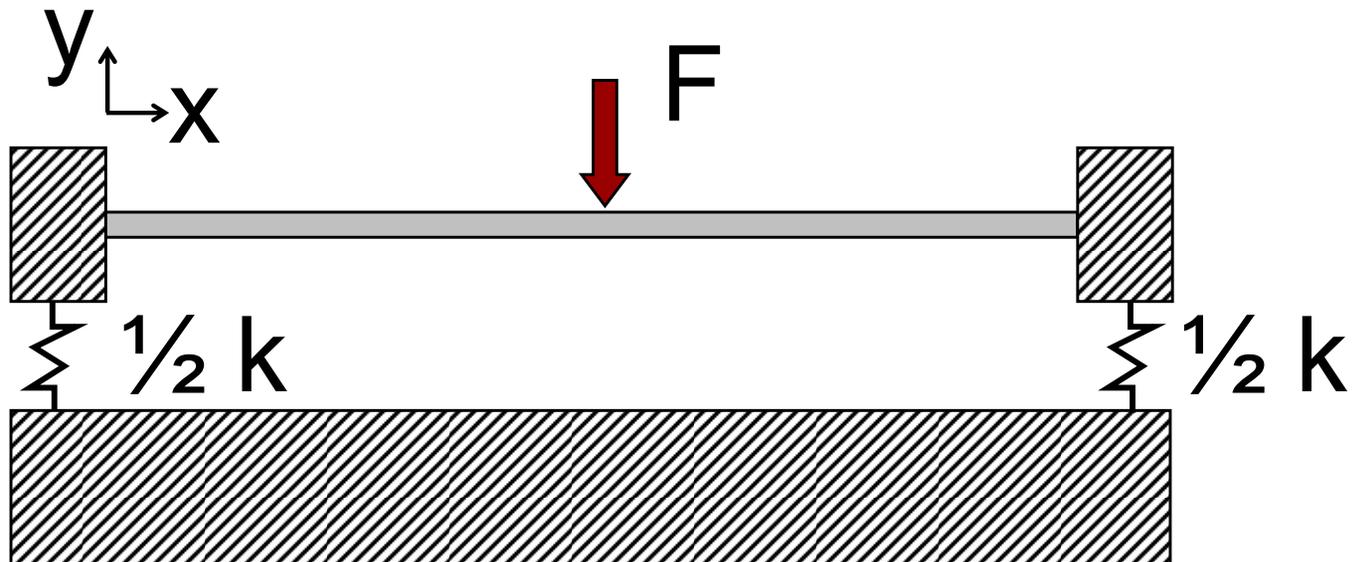
But, is this really what is going on?

# Practical application to the lathe problem

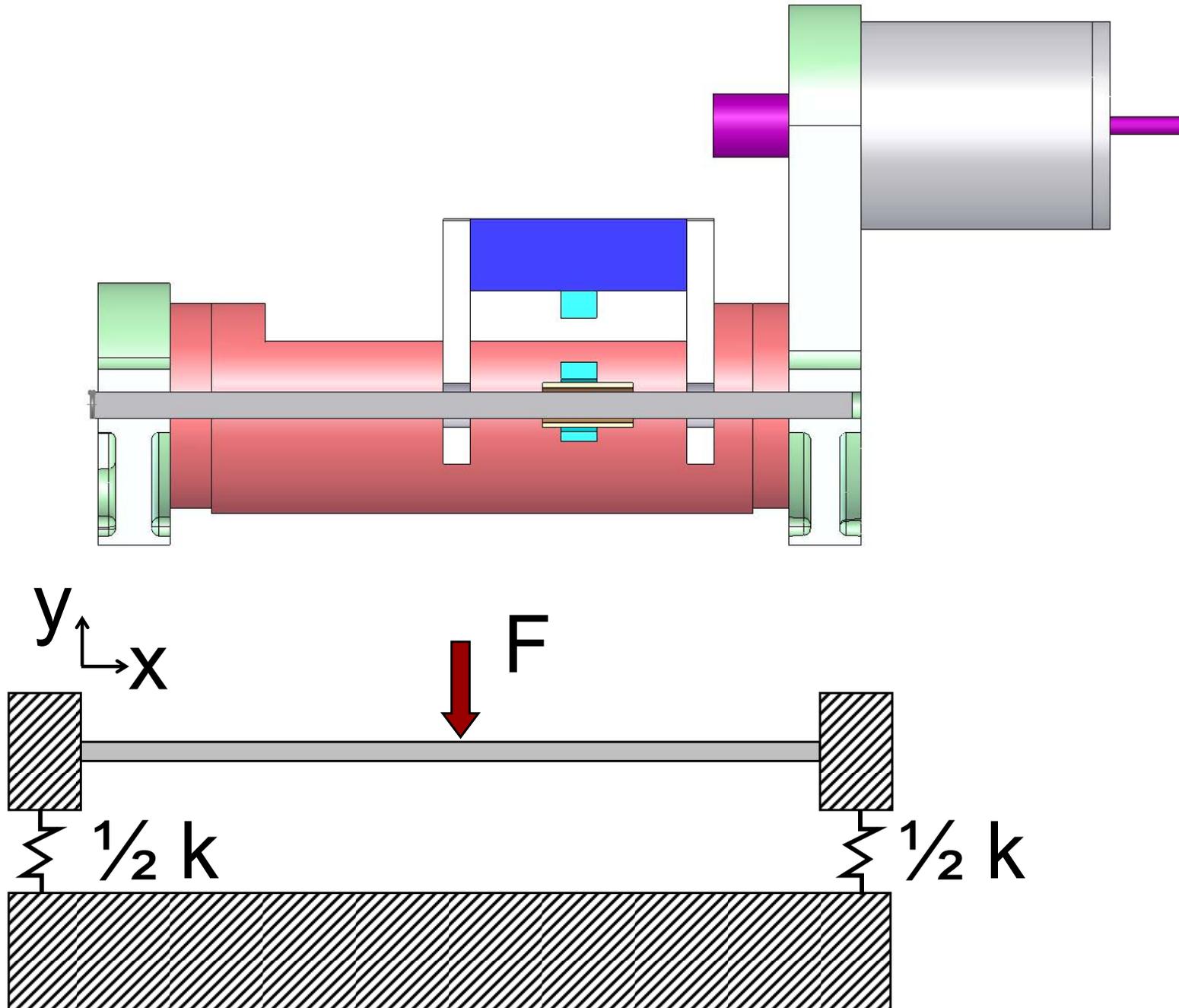


$$k|_{Beam} = \frac{768}{7} \cdot \frac{E I}{l^3}$$

**Vs. ?**



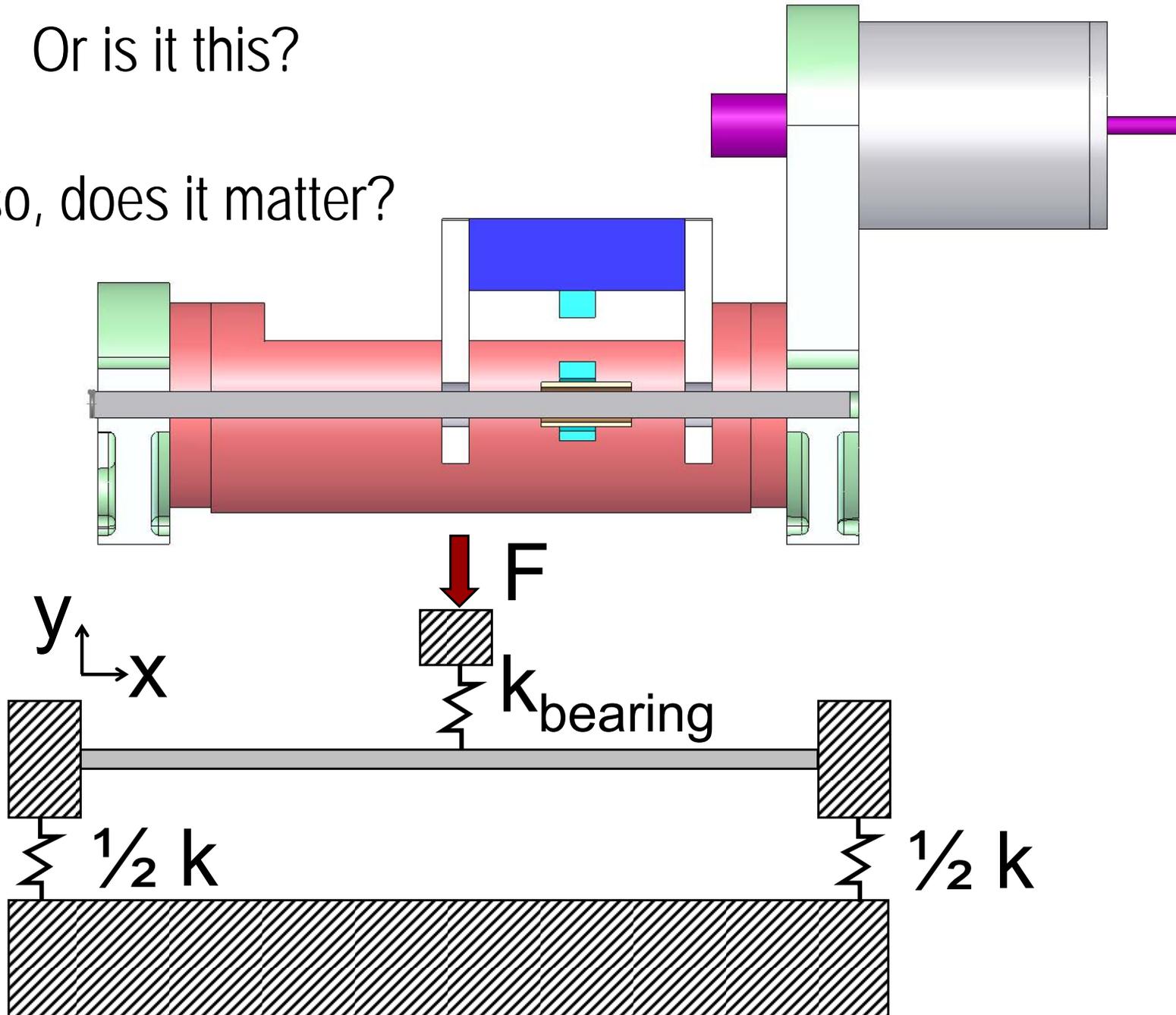
# Practical application to the lathe problem



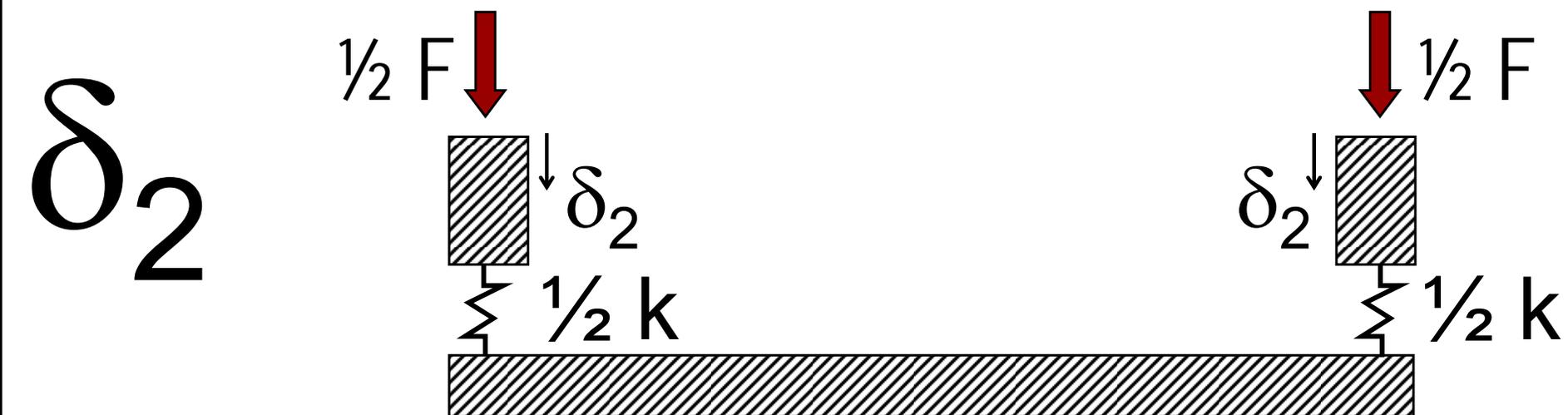
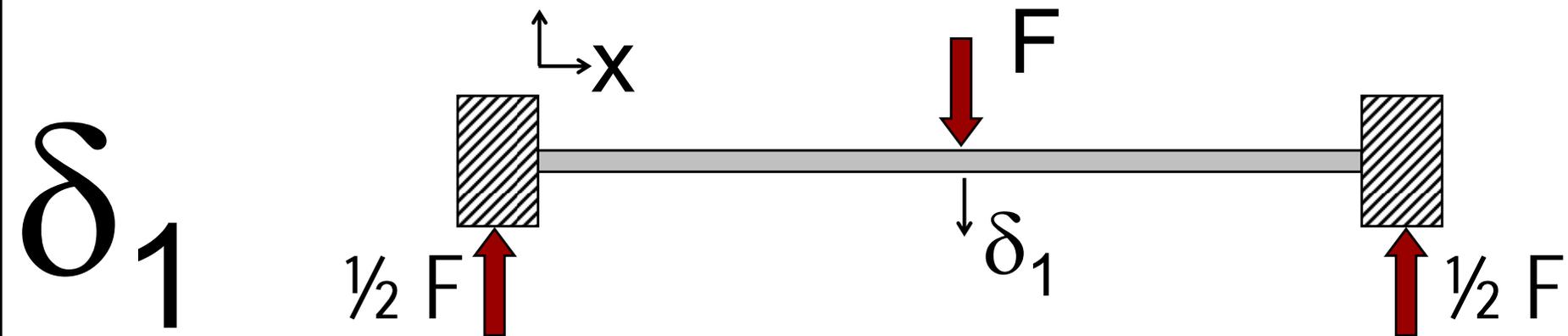
# Practical application to the lathe problem

Or is it this?

If so, does it matter?



# Practical application to the lathe problem



# Group work

**Obtain an equation for  $\delta_{\text{total}}$  in terms of  $F$ ,  $k$  and  $l$**

**Estimate when  $k$  is important / should be considered?**

**What issue/scenario would cause  $k$  not to be infinite?**

**Look at these causes, if a stiffness is involved, would linearity, and therefore superposition apply?**