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2.72 Elements of Mechanical Design  
Spring 2009

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*2.72*

*Elements of  
Mechanical Design*

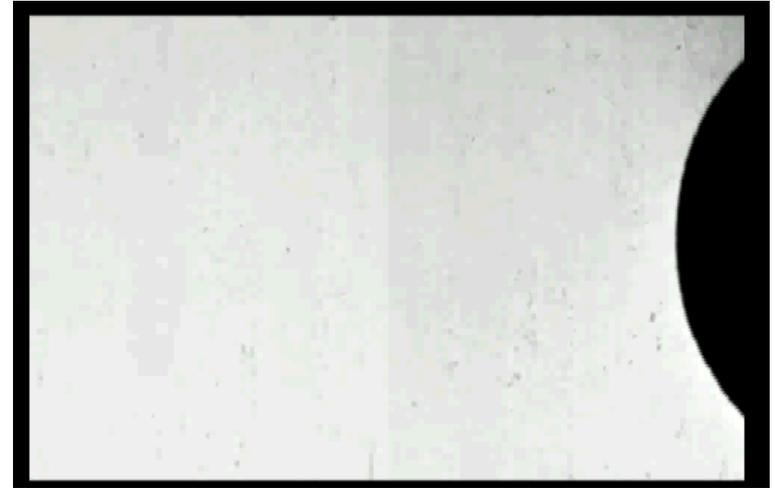
*Lecture 04: Fatigue*

# Schedule and reading assignment

## Reading quiz

## Announcements

- ❑ Shaft due date
- ❑ Shaft exercise
- ❑ Goodman diagram quiz (Tuesday)
- ❑ Shear-moment qualifying quiz (Tuesday)



Please see unterhausen. "fatigue crack." March 27, 2008. YouTube. Accessed October 28, 2009.

<http://www.youtube.com/watch?v=iBuuVd0JIIM>

## Topics

- ❑ Discuss stiffness exercises
- ❑ Start fatigue

## Reading

- ❑ None, for Tuesday, prep for quizzes in lab time (Given lounge, top of 35)

*Reading quiz*

# Discuss stiffness exercises

## Answers

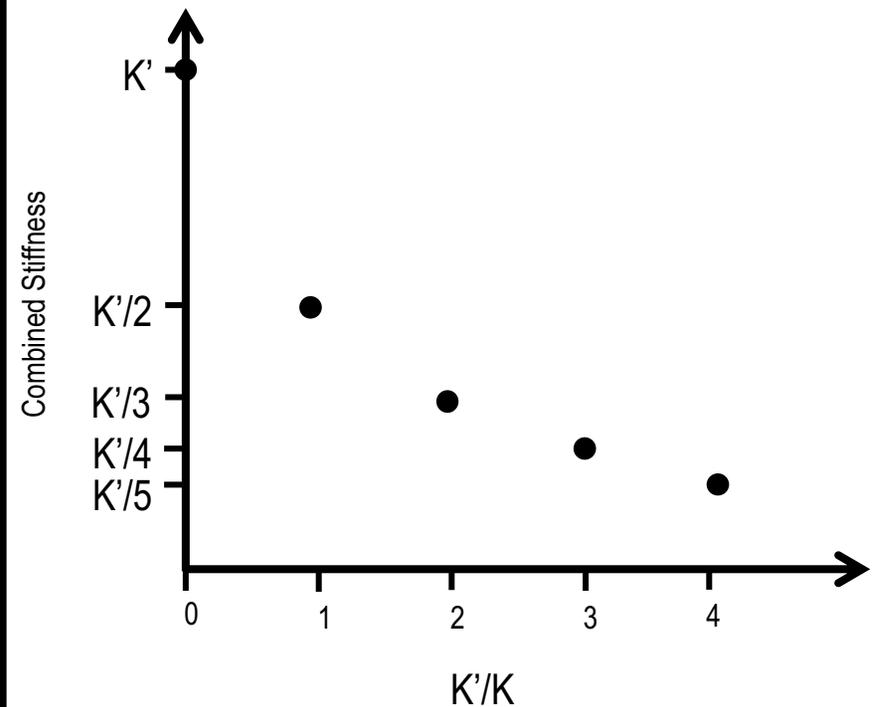
### Intuition about stiffness

- Part
- Spindle
- Carriage-rail
- Etc...

### Insight and perspective



## Carriage bearing-rail



*Shaft exercise*

*Are you on top of this!?*

# *Fatigue part I*

*At what critical time in  
engineering history did  
fatigue become  
relevant?*

*Why does fatigue  
failure generate serious  
concern?*

*What type of warnings  
does one receive?*

# Fire plane wing failure

## July 18, 2002 near Estes Park, Colorado

- ❑ Both crew members killed
- ❑ Delivered in July, 1945 to the U.S. Navy
- ❑ Logged 8000+ flight hours

## Investigation

- ❑ NTSB found extensive fatigue
- ❑ Cracks hidden from view



# Comet airplane failures

## BOAC Flight 781 crashes on 10 January 1954

- ❑ Concluded fire was most likely cause
- ❑ Resumed on 23 March 1954

## Comet G-ALYY crashes on 8 April 1954

- ❑ Pressure tests revealed fatigue
- ❑ Windows to be glued & riveted, but riveted only
- ❑ Square windows → oval
- ❑ Skin thickened
- ❑ Service in 1958



# I-35 bridge failure

*By Laurie Blake, Paul Mcenroe, Pat Doyle and Tony Kennedy, Star Tribune*

## MnDOT's options:

- ❑ Make repairs or find flaws & bolt on steel plating
- ❑ Fueled emotional debate



Image from Wikimedia Commons, <http://commons.wikimedia.org>

## MNDOT's action:

- ❑ Thousands of bolt holes would weaken bridge
- ❑ Launched inspection, interrupted by work on bridge surface

## The state's top bridge engineer:

- ❑ "We chose the inspection route..... We thought we had done all we could, but obviously something went terribly wrong."
- ❑ "Up until the late 1960s, it was thought that fatigue was not a phenomenon you would see in bridges."

*How much do engineers  
know about fatigue?*

*How “exact” are  
fatigue models?*

# Experimental data

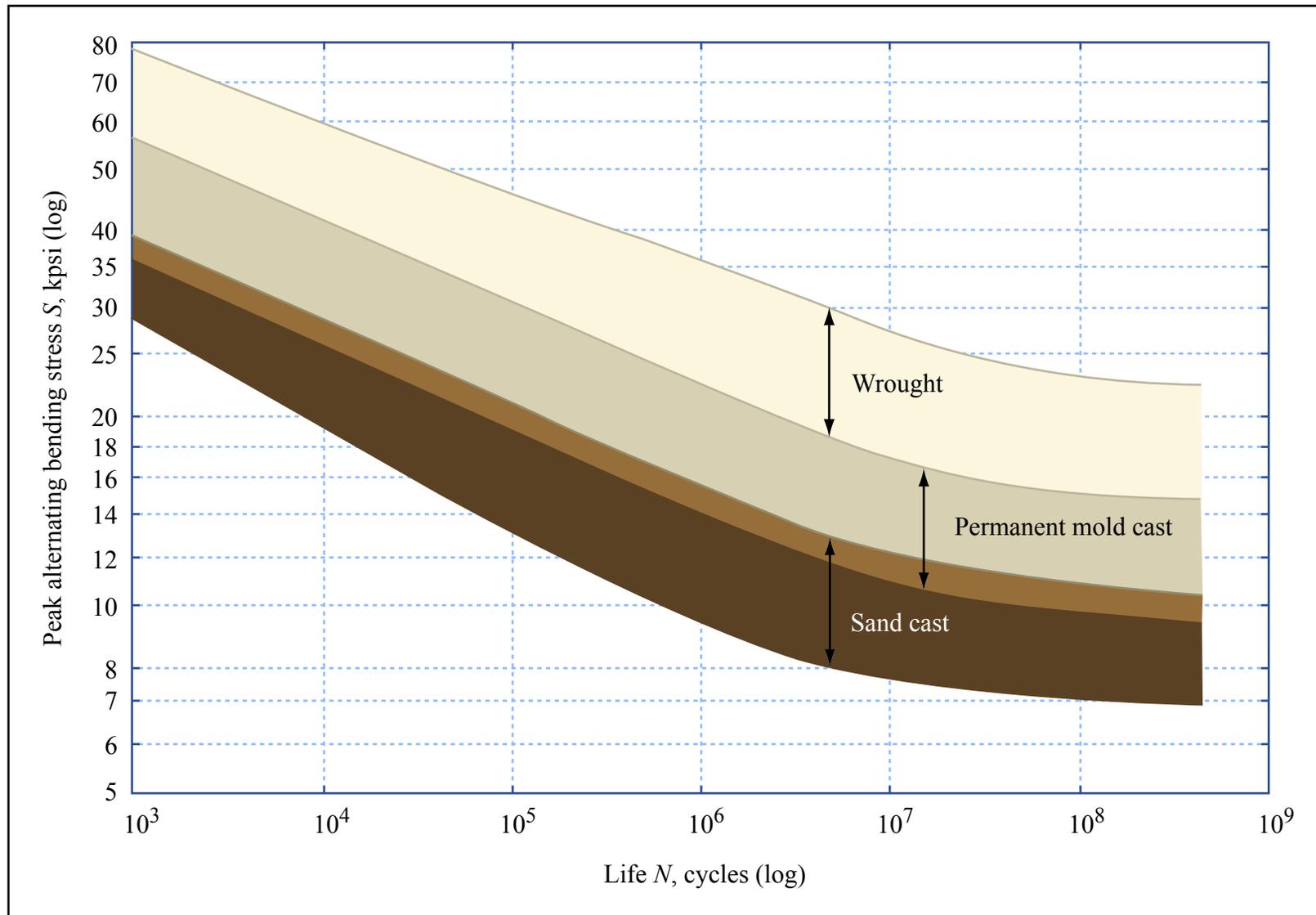


Figure by MIT OpenCourseWare. Adapted from Fig. 6-11 in Shigley & Mischke.

# Experimental data

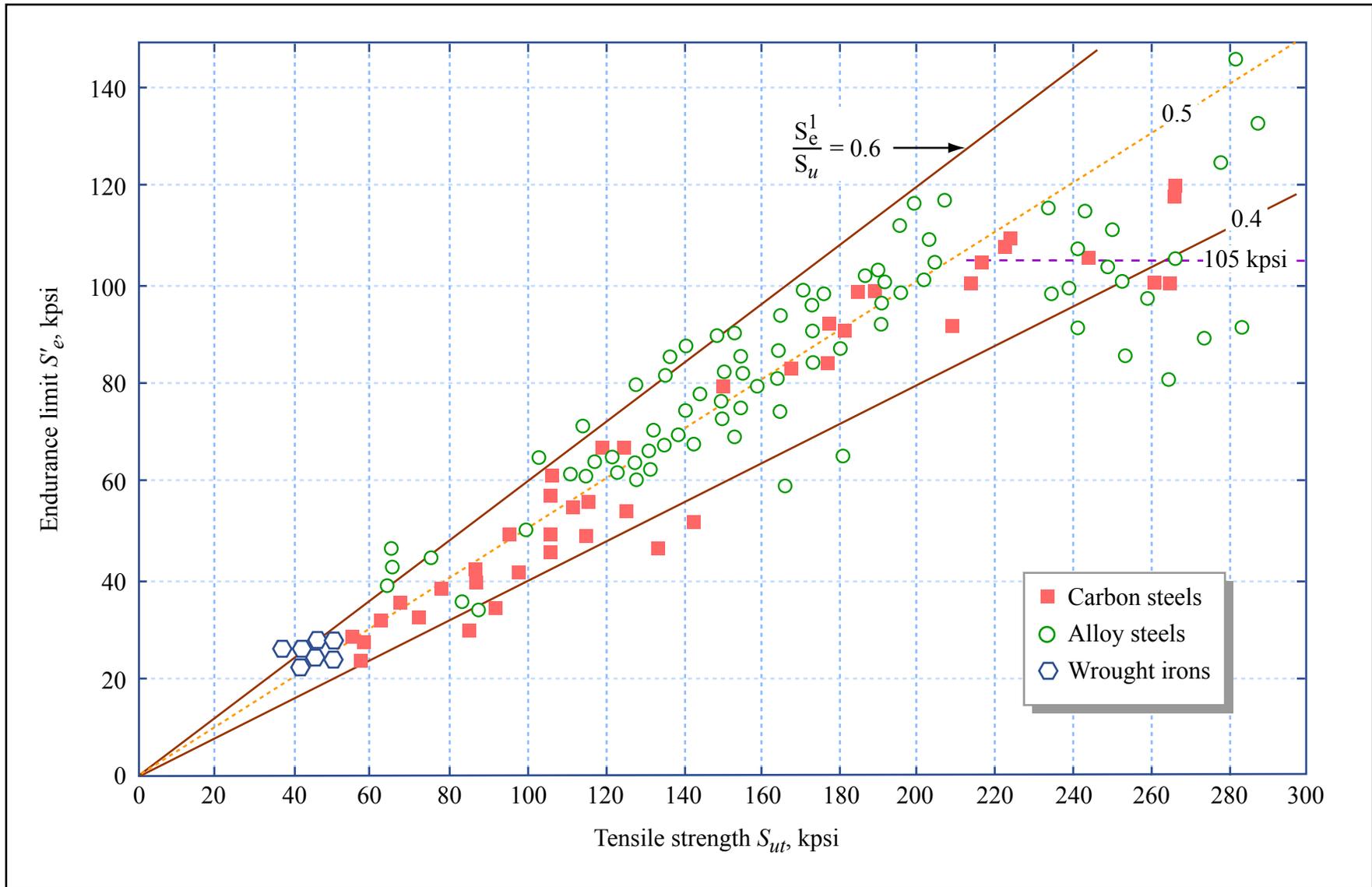


Figure by MIT OpenCourseWare. Adapted from Fig. 6-17 in Shigley & Mischke.

*What actions and/or  
practices should be put  
in place as a result?*

# Testing and prevention

## Where life-limb-\$ are important

- ❑ It is your job to spec out test type and procedure
- ❑ Balance of cost vs. risk

## Example types

- ❑ Ultrasonic
- ❑ Liquid penetrant
- ❑ Stiffness/impulse
- ❑ Eddy-current
- ❑ Leaks
- ❑ Visual

Many people listen to REAL data

Few people listen to Eqxns

A choice: Job vs. safety

Images removed due to copyright restrictions.

Please see [http://www.labino.com/bilder/applications/00533\\_RT8.jpg](http://www.labino.com/bilder/applications/00533_RT8.jpg)  
<http://www.riverinaairmotive.com.au/img/mpi001.jpg>

## On foreseeable use

- ❑ Common sense
- ❑ Legal

*Where do cracks come  
from?*

# Potential crack origins/causes

## Inherent to material

- ❑ Imperfections, e.g. castings
- ❑ Precipitates, e.g. Al 6061 T6
- ❑ Coalescing of internal dislocations
- ❑ Grain boundaries

Image removed due to copyright restrictions. Please see <http://www.emeraldinsight.com/fig/2190080205007.png>

## Fabrication-related

- ❑ Tool marks
- ❑ Improper assembly, e.g. forcing (car suspension-cast materials)
- ❑ Thermally induced - Weld cracks and related HAZ problems

## Use-related

- ❑ High stress areas
- ❑ Scratches
- ❑ Unintended use/damage/loading (e.g. 3 finger tight and paint lid)

# Fatigue: Origin of problem

Images removed due to copyright restrictions. Please see:

<http://www.metallographic.com/Images/Zn-Al.jpg>

[http://corrosionlab.com/Failure-Analysis-Studies/Failure-Analysis-Images/  
20030.SCC.304H-pipeline/20030.microstructure-ditched-grain-boundaries.jpg](http://corrosionlab.com/Failure-Analysis-Studies/Failure-Analysis-Images/20030.SCC.304H-pipeline/20030.microstructure-ditched-grain-boundaries.jpg)

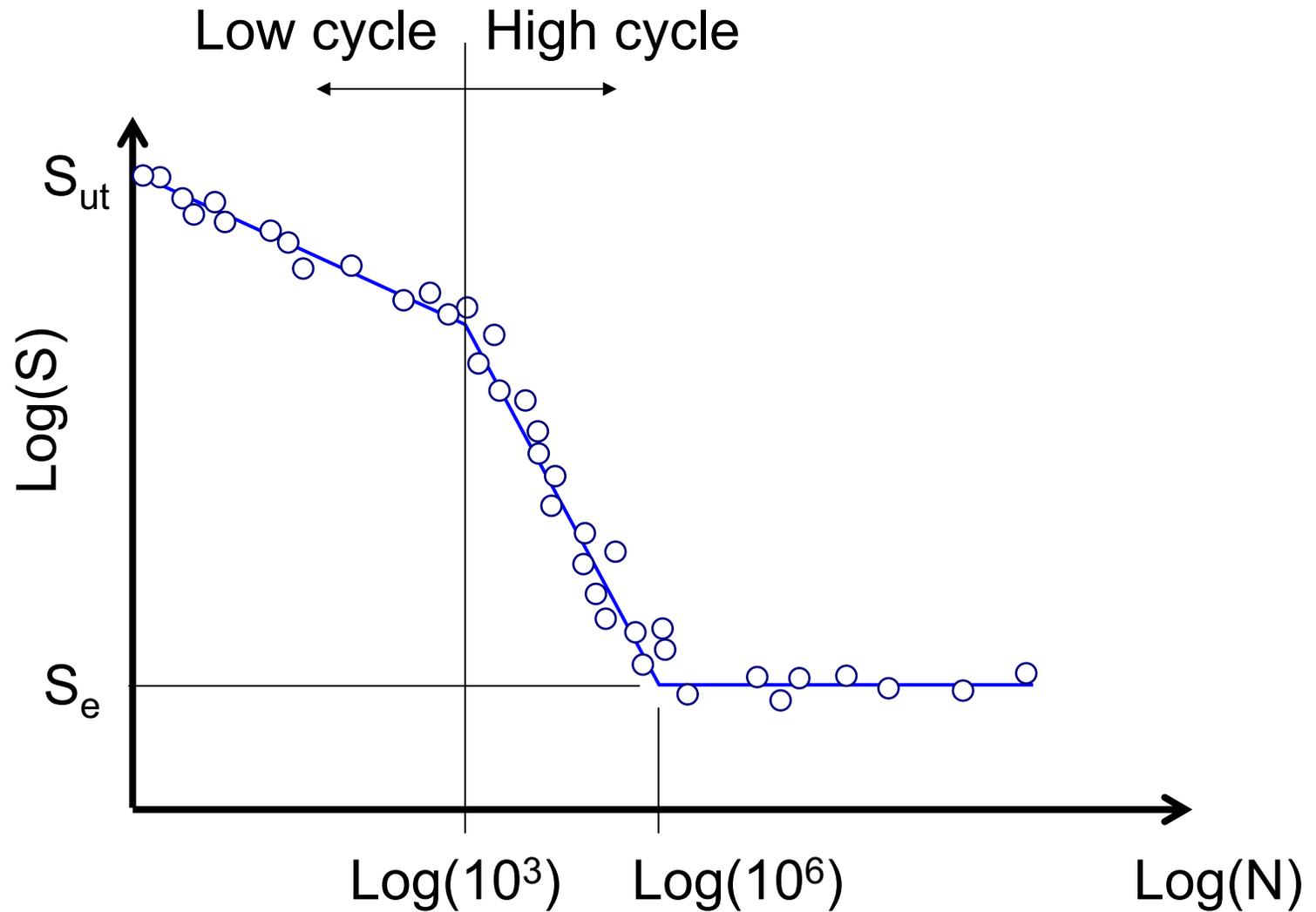
and

Fig. 4b in Henderson, Donald W., et al. "The Microstructure of Sn in Near-Eutectic Sn-Ag-Cu Alloy Solder Joints and its Role in Thermomechanical Fatigue." *Journal of Materials Research* 19 (June 2004): 1608-1612

or

Slide 36 in Kang, Sung K. "[Near-Ternary Sn-Ag-Cu Solder Joints; Microstructure, Thermal Fatigue, and Failure Mechanisms.](#)" Pb-Free Workshop, TMS Annual Meeting, February 2005.

# Fatigue life review



# Fatigue life review

**Ferrous materials/allows:  $S_e \sim 1\,000\,000 - 10\,000\,000$**

- ❑ Under ideal conditions

**Non-ferrous (i.e. aluminum) generally no  $S_e$ ...**

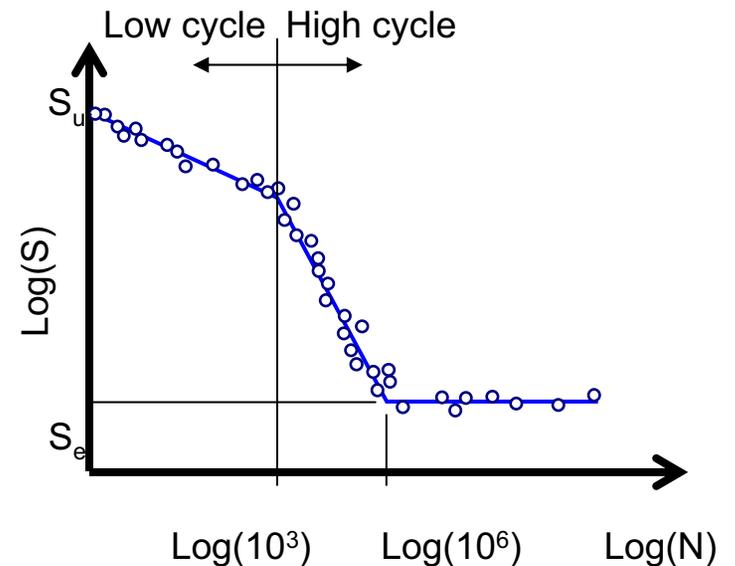
**Do we use Al in places where fatigue is important?...**

- ❑ Aircraft...
- ❑ History Channel Boneyard...

**Science vs. engineering...**

## Methods

- ❑ Stress
- ❑ Strain
- ❑ Fracture mechanics



# Fatigue and ethical responsibility

**You will be criminally negligent if you do not augment calculations with TESTING for critical fatigue applications**

**Life-limb-\$**

# Real life



Please see datsun\_laurel. "R06 Front Carbon ARB Fatigue Test." Photobucket. Accessed October 14, 2009.  
[http://s23.photobucket.com/albums/b388/datsun\\_laurel/FSAE/?action=view&current=ARB\\_Test.flv](http://s23.photobucket.com/albums/b388/datsun_laurel/FSAE/?action=view&current=ARB_Test.flv)

# Real life



<http://video.google.com> (author?)

Please see SmithersMpls. "Carbon Frame Fatigue Test." February 9, 2007. YouTube.  
Accessed October 14, 2009. [http://www.youtube.com/watch?v=QHO\\_VjVhaE8](http://www.youtube.com/watch?v=QHO_VjVhaE8)

# Real life



<http://yourdailymedia.com>

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Please see motocross. "The Nitro Circus: Channel 9 Action News." March 3, 2009. YouTube. Accessed October 14, 2009.

<http://www.youtube.com/watch?v=kOaYruVcvm4>

*What reasonable hypotheses could one hold for identifying important factors?*

# Fatigue life modifiers

Experimental results are used to obtain modifiers

$$S_e = \left( k_a k_b k_c k_d k_e k_f \right) S'_e$$

**Where:**

- $k_a$  = Surface condition modification factor
- $k_b$  = Size modification factor
- $k_c$  = Load modification factor
- $k_d$  = Temperature modification factor
- $k_e$  = Reliability modification factor
- $k_f$  = Others...
  
- $S'_e$  = Rotary-beam test endurance limit
- $S_e$  = Predicted endurance limit for your part

# Endurance limit depends on many factors

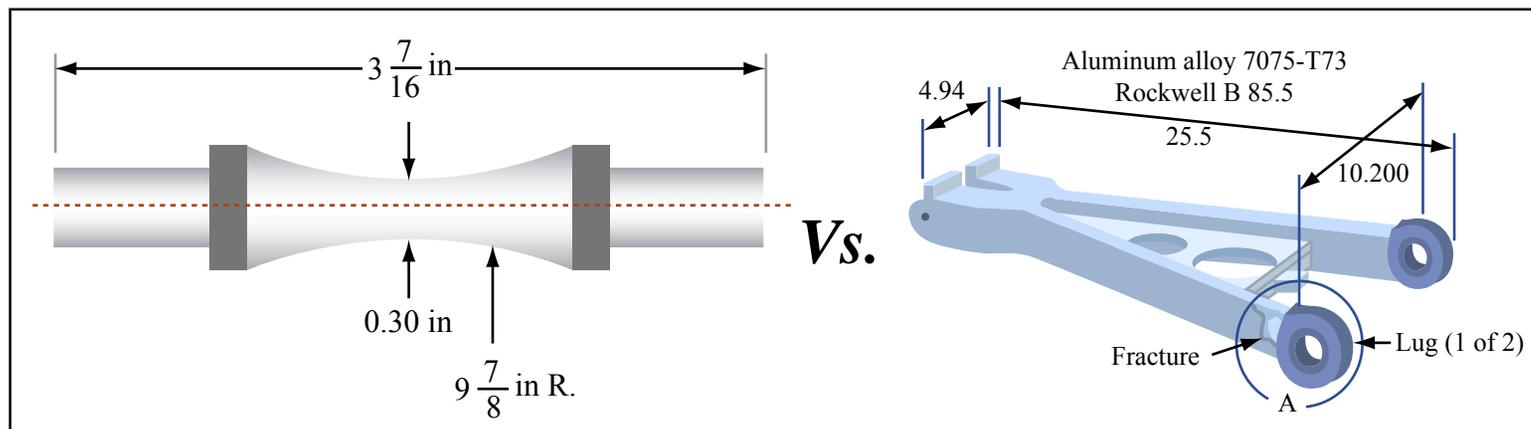
For ferrous materials, the following approximations may be used for first pass design

$$0.5 S_{ut} \quad S_{ut} \leq 200 \text{ kpsi}$$

$$S'_e = 100 \text{ kpsi} \quad S_{ut} > 200 \text{ kpsi}$$

$$700 \text{ MPa} \quad S_{ut} > 1400 \text{ MPa}$$

This is for ideal conditions... but designs are never ideal



# Experimental data

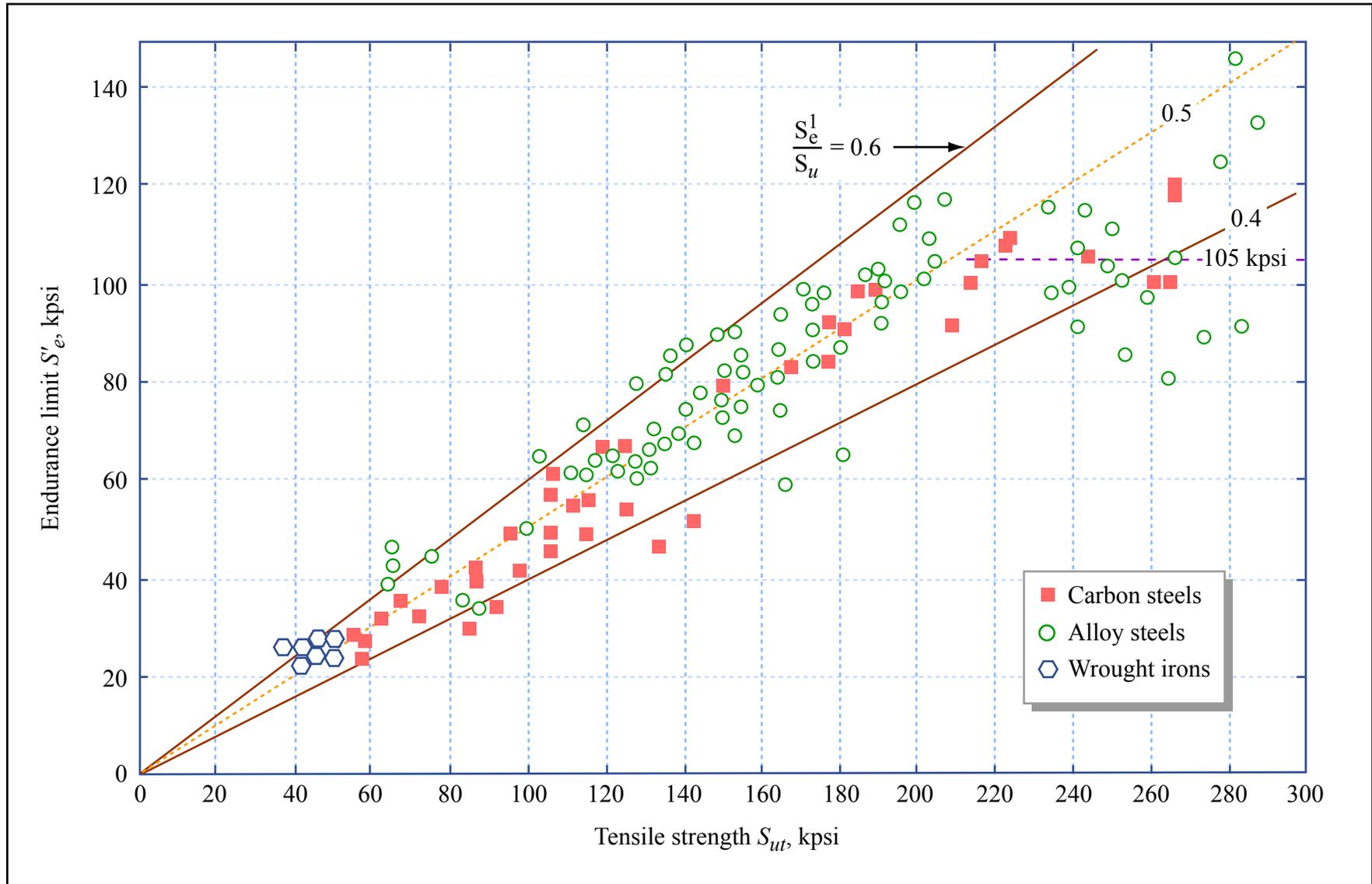


Figure by MIT OpenCourseWare. Adapted from Fig. 6-17 in Shigley & Mischke.

# Fatigue life modifiers: Surface condition

Experimental results are used to obtain modifiers

$$k_a = a S_{ut}^b$$

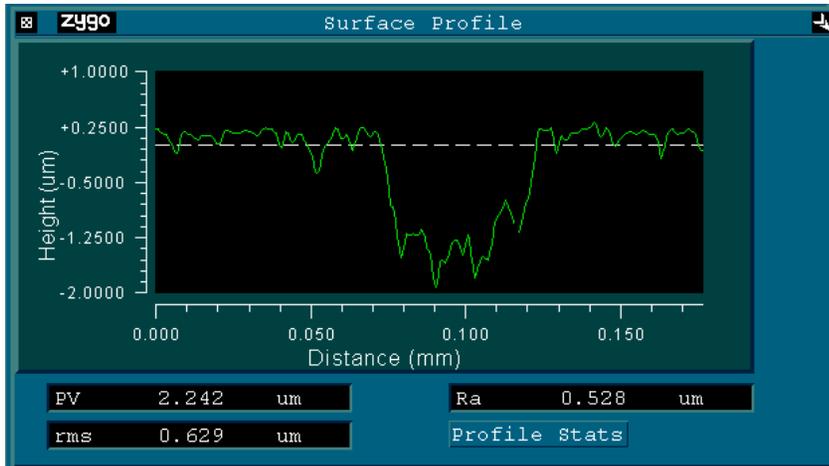
**Where:**

- a = function of fabrication process
- b = function of fabrication process
  - *Why does finish matter?*

Surface finish	Factor a		Exponent b
	$S_{ut}$ kpsi	$S_{ut}$ MPa	
Ground	1.34	1.58	-0.085
Machined or cold-drawn	2.70	4.51	-0.265
Hot-rolled	14.4	57.7	-0.718
As-forged	39.9	272.	-0.995

*Why would surface  
condition matter?*

# Surface roughness review



$$R_a = \frac{1}{L} \cdot \int_0^L |y| dx$$

## Common surface roughness ( $R_a$ in micro-inches)

Process	2000	1000	500	250	125	63	32	16	8	4	2	1	1/2
Sawing	[Bar spanning from 2000 to 32]												
Drilling			[Bar spanning from 500 to 32]										
Milling		[Bar spanning from 1000 to 8]											
Turning		[Bar spanning from 1000 to 1]											
Grinding			[Bar spanning from 250 to 1]										
Polishing							[Bar spanning from 32 to 1/2]						

**Only specify what you need & know your processes**

*Why would part size  
matter?*

# Fatigue life modifiers: Size factor

**For bending and torsion of a round bar:**

$$k_b = \begin{array}{ll} 0.879 d^{-0.107} & \text{for } 0.11in < d < 2.00in \\ 0.910 d^{-0.157} & \text{for } 2.00in < d < 10.0in \end{array}$$

**For axial loading:**

$$k_b = 1$$

**What if the bar is not round?**

- ❑ Use a 95 percent stress area
- ❑ Equate volumes, length drops out
- ❑ Relate cross sectional area of round and square bar

$$d_e = 0.808(hb)^{0.5}$$

*Why would the type of  
loading matter?*

# Fatigue life modifiers: Loading factor

For bending and torsion of a round bar:

1.00

*bending*

$k_c = 0.85$

*axial*

0.59

*torsion*

*Why would temperature  
matter?*

# Fatigue life modifiers: Temperature factor

## The effect of increasing temperature

- ❑ Yield strength typically decreases
- ❑ May be no fatigue limit for material-temperature combos

## The temperature factor

- ❑ May be ESTIMATED from existing tables
- ❑ Should ALWAYS BE DETERMINED EXPERIMENTALLY FOR YOUR GIVEN MATERIAL.

## Relate strength at temperature to room temp. strength

$$k_d = \frac{S_T}{S_{RT}}$$

# Fatigue life modifiers: For an example steel

Temperature, °C	$S_T/S_{RT}$	Temperature, °F	$S_T/S_{RT}$
20	1.000	70	1.000
50	1.010	100	1.008
100	1.020	200	1.020
150	1.025	300	1.024
200	1.020	400	1.018
250	1.000	500	0.995
300	0.975	600	0.963
350	0.943	700	0.927
400	0.900	800	0.872
450	0.843	900	0.797
500	0.768	1000	0.698
550	0.672	1100	0.567
600	0.549		

Figure by MIT OpenCourseWare. Adapted from Table 6-4 in Shigley & Mischke.

*Part II*

*Calculations*

*How do statistics and  
probability come into  
play?*

# Standard normal distribution, mean = 0

## Standard normal distribution curve generated via the probability distribution

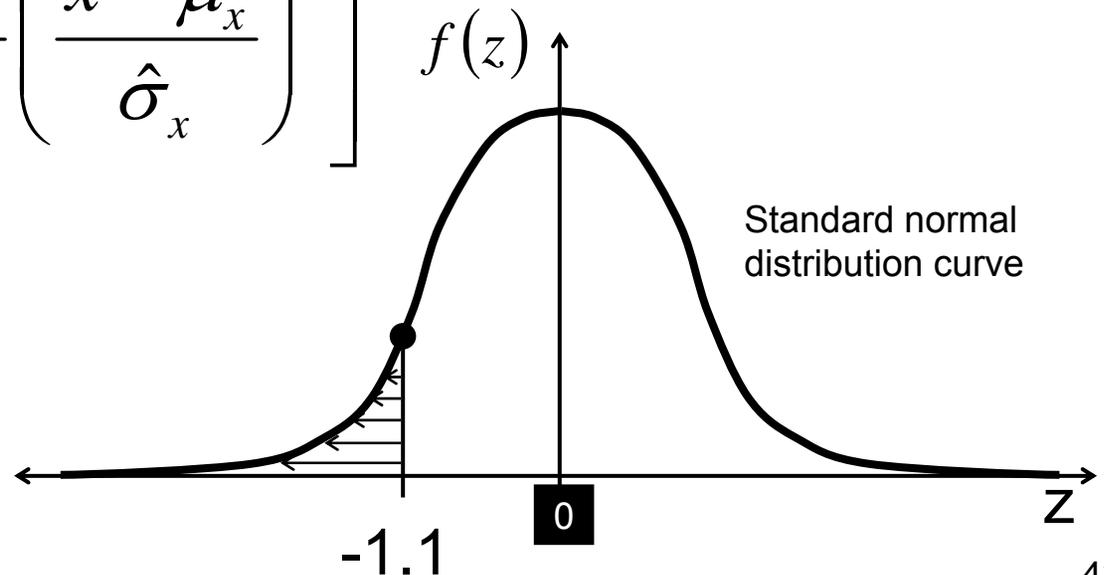
- Area under the curve = 1

$$f(z) = \frac{1}{\hat{\sigma}_x \sqrt{2\pi}} \exp\left[-\frac{1}{2}(z)^2\right]$$

This will be covered  
in the 2<sup>nd</sup> design lab

## What if mean is not 0?

$$f(x) = \frac{1}{\hat{\sigma}_x \sqrt{2\pi}} \exp\left[-\frac{1}{2}\left(\frac{x - \mu_x}{\hat{\sigma}_x}\right)^2\right]$$



# Non-zero means in Gaussian distributions

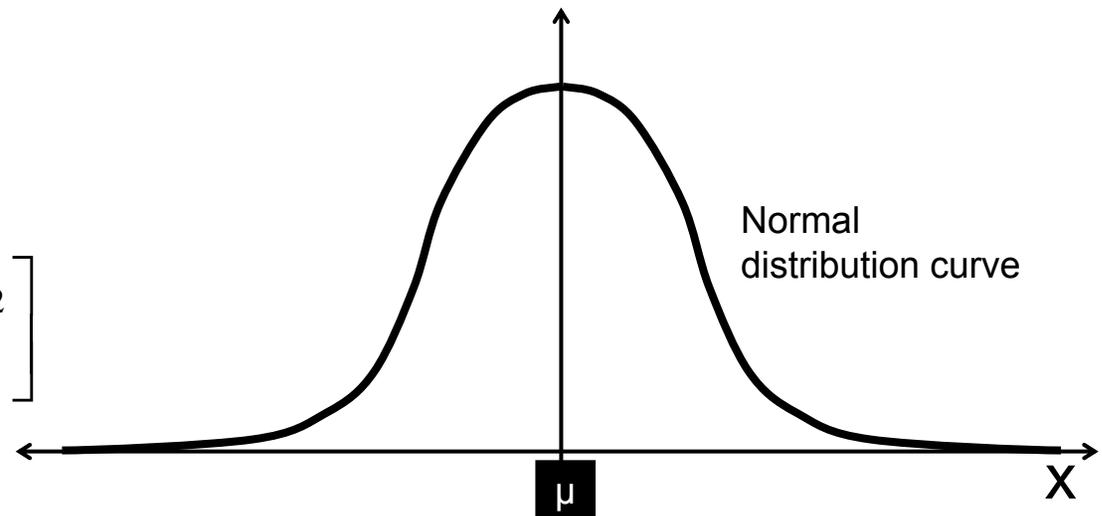
A normal Gaussian distribution is typically observed in fatigue behavior of parts

□  $x$  = variate =  $x$      $z$  = transformation variate     $\sigma$  = standard deviation

$$f(x) = \frac{1}{\hat{\sigma}_x \sqrt{2\pi}} \exp \left[ -\frac{1}{2} \left( \frac{x - \mu_x}{\hat{\sigma}_x} \right)^2 \right]$$

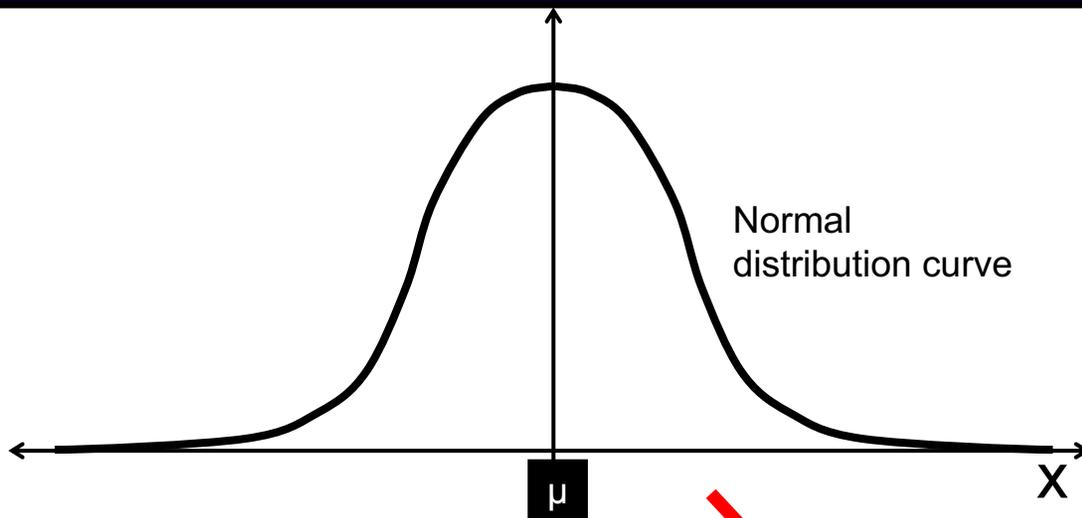
$$z = \frac{x - \mu_x}{\hat{\sigma}_x}$$

$$f(z) = \frac{1}{\hat{\sigma}_x \sqrt{2\pi}} \exp \left[ -\frac{1}{2} (z)^2 \right]$$

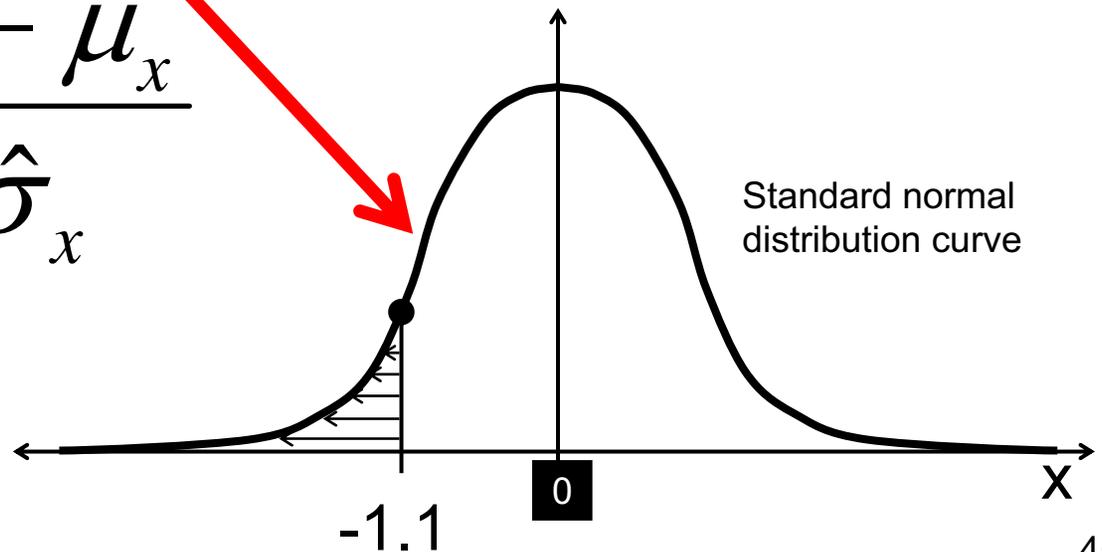


Only one table for values needed to find the area  
between z values...

# Fatigue life modifiers: Reliability factor



$$Z = \frac{X - \mu_x}{\hat{\sigma}_x}$$



# Example use of standard normal distribution

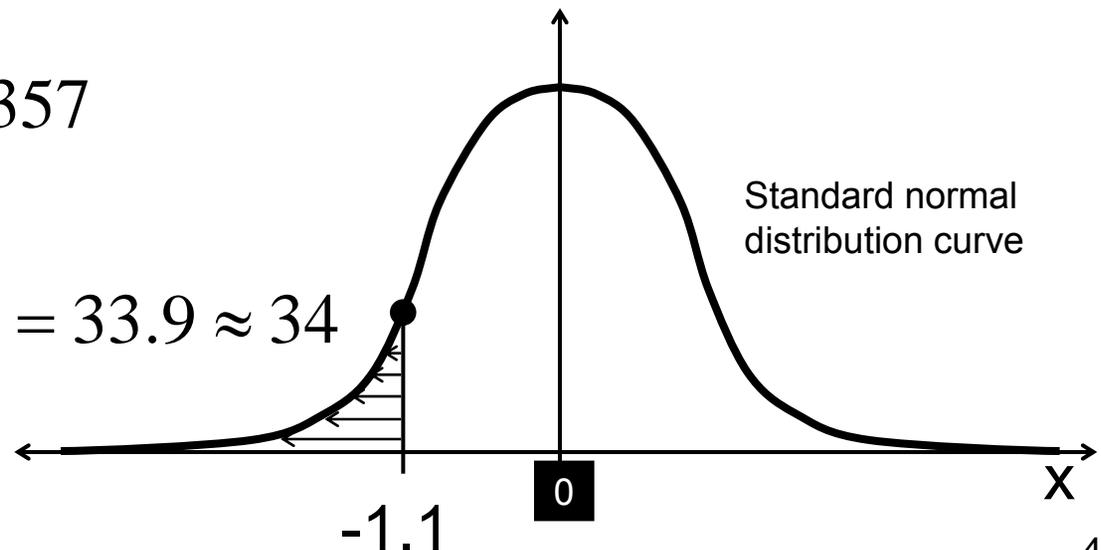
In a shipment of 250 connecting rods, the mean tensile strength is 45 kpsi and the standard deviation is 5 kpsi

- (a) Assuming a normal distribution, how many rods may be expected to have a strength less than 39.5 kpsi?
- (b) How many are expected to have a strength between 39.5kpsi and 59.5kpsi?

$$z_{39.5} = \frac{x - \mu_x}{\hat{\sigma}_x} = \frac{39.5 - 45.0}{5.0} = -1.10$$

$$\Phi(z_{39.5}) = \Phi(-1.10) = 0.1357$$

$$N \cdot \Phi(z_{39.5}) = 250 \times 0.1357 = 33.9 \approx 34$$

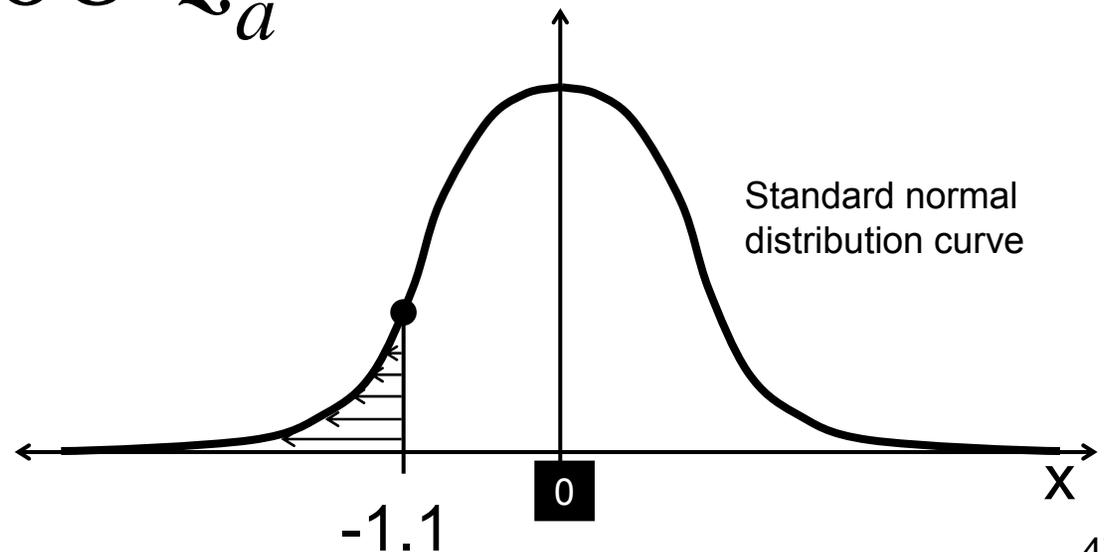


# Fatigue life modifiers: Reliability factor

## Most strength data is reported as mean values

- ❑ Standard deviations typically less than 8%, but you MUST KNOW what it is... run experiments...
- ❑ 68% of all measurements fall within one standard deviation
- ❑ 95% of all measurements fall within two standard deviations
  
- ❑ For  $\sigma \sim 8\%$

$$k_e = 1 - 0.08 z_a$$



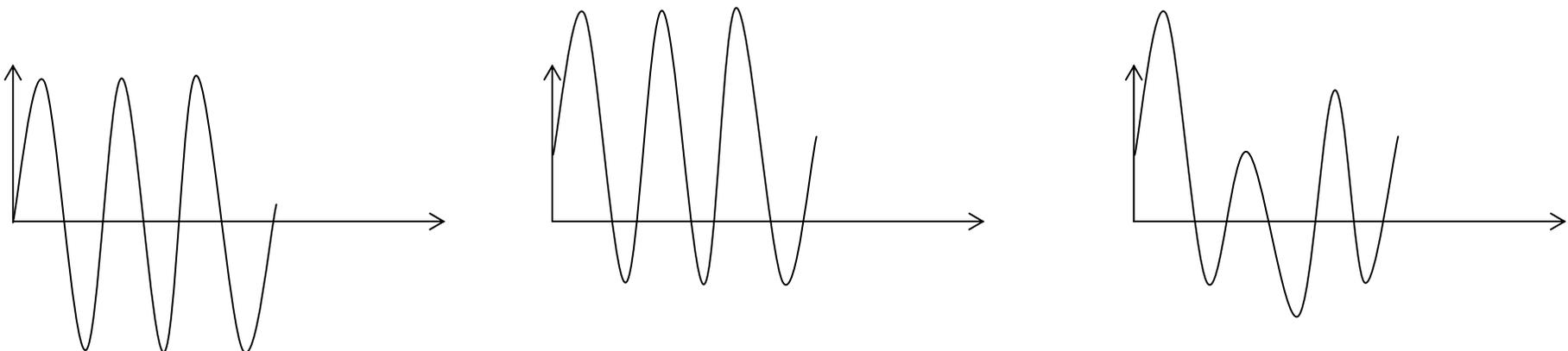
*How do we do  
1<sup>st</sup> order fatigue  
modeling/analysis?*

# Fluctuating stresses

## Stress values of concern

- $\sigma_{\min}$       Minimum stress
- $\sigma_{\max}$       Maximum stress
- $\sigma_a$           Amplitude component =  $(\sigma_{\max} - \sigma_{\min})/2$
- $\sigma_m$           Midrange component =  $(\sigma_{\max} + \sigma_{\min})/2$
- $\sigma_s$           Steady component
  
- $R$               Stress ratio =  $\sigma_{\min} / \sigma_{\max}$
- $A$               Amplitude ratio =  $\sigma_a / \sigma_m$

Note the correction to  
 $\sigma_a$  and  $\sigma_m$



# Fluctuating stresses

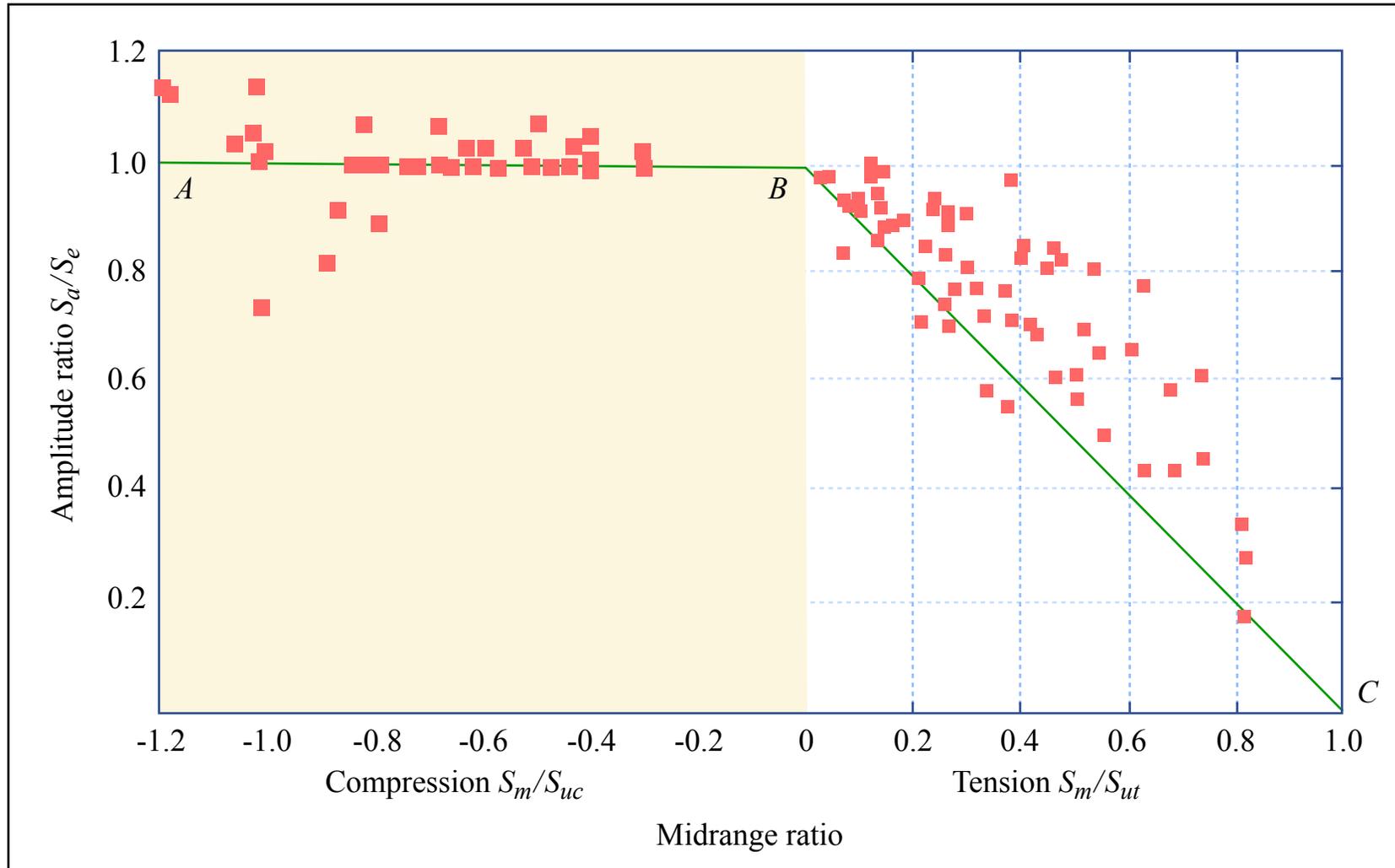


Figure by MIT OpenCourseWare. Adapted from Fig. 6-25 in Shigley & Mischke.

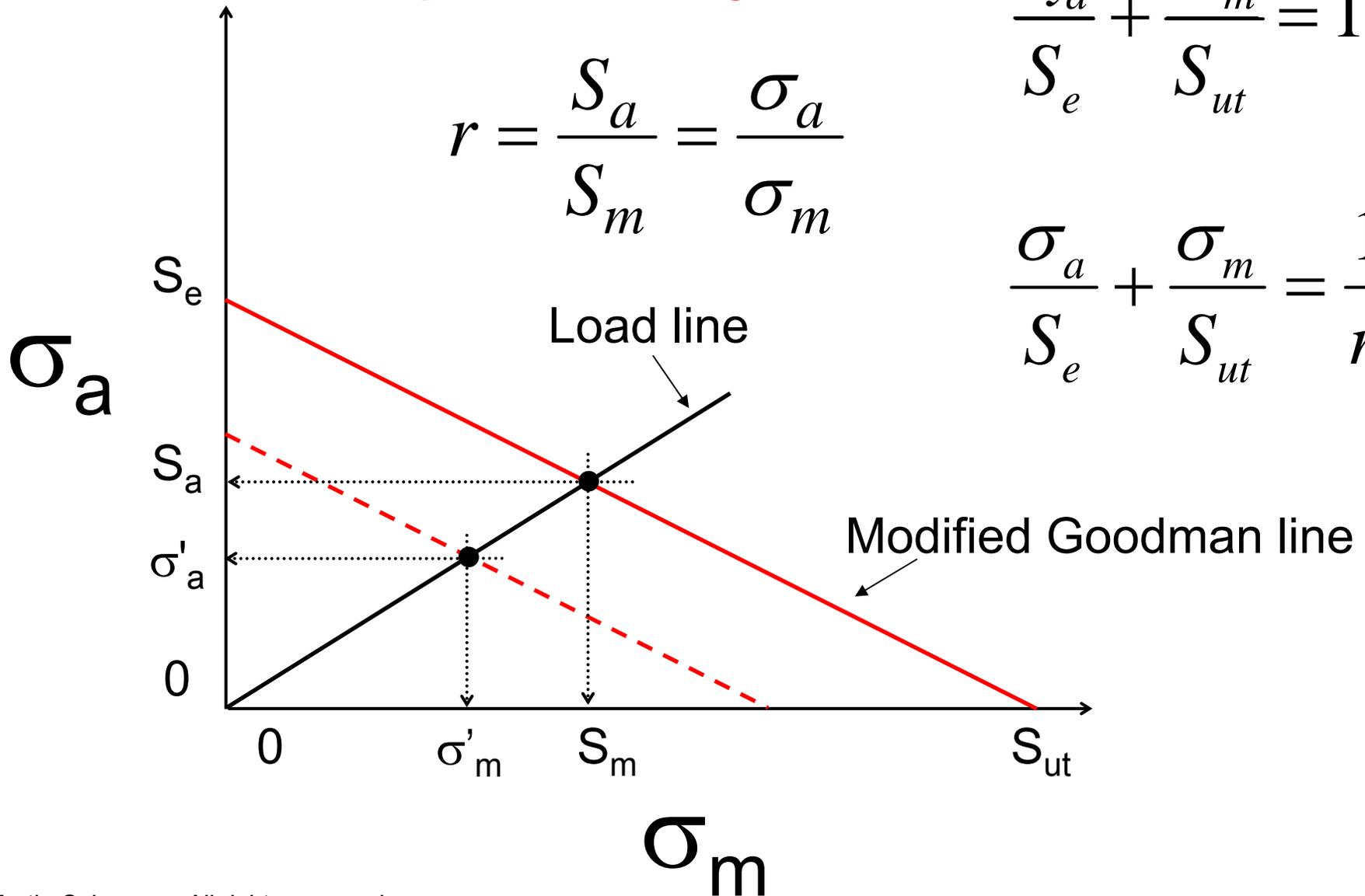
# Fatigue diagram: Goodman

Capital S = strength!

$$\frac{S_{y_a}}{S_e} + \frac{S_{x_m}}{S_{ut}} = 1$$

$$r = \frac{S_a}{S_m} = \frac{\sigma_a}{\sigma_m}$$

$$\frac{\sigma_a}{S_e} + \frac{\sigma_m}{S_{ut}} = \frac{1}{n}$$



# Stress concentration and notch sensitivity

Fatigue is due to crack propagation, hence notch sensitivity is important

- Max stress

$$\sigma_{\max} = K_f \sigma_o$$

$K_t$  from table A-15

$$\tau_{\max} = K_{fs} \tau_o$$

- Notch sensitivity,  $q$  (usually  $0 < q < 1$ ) accounts for material sensitivity

- $K_f = 1 + q(K_t - 1)$

*Table 6-20*

- $K_{fs} = 1 + q_{shear}(K_{ts} - 1)$

*Table 6-21*

**It is always safe to use  $K_t$**

**$K_t$  rarely  $> 3$  for good/practical designs, but check!**

# Example

1.5 in diameter AISI 1050 cold drawn steel ( $S_y = 84\text{kpsi}$ ,  $S_{ut} = 100\text{ kpsi}$ ) withstands a tensile load that ranges from 0 to 16000 lbf.  $K_f = 1.85$ ,  $k_a = 0.797$ ,  $k_b = 1$ ,  $k_d = 1$ ,  $k_c = 0.923$ . (8<sup>th</sup> edition has  $k_c = 0.85$ )

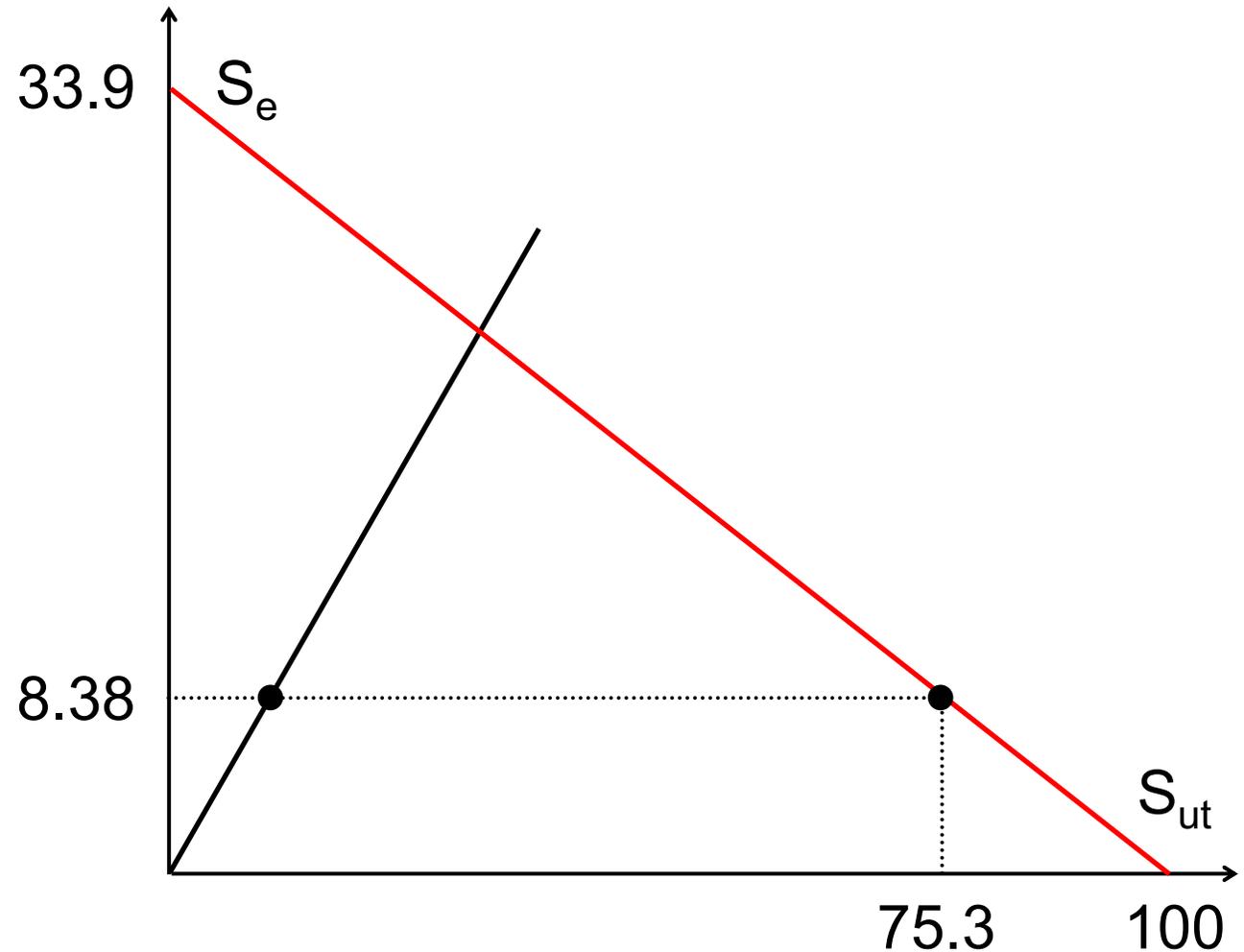
## Modifications in example:

- ❑  $k_c = 0.85$  in 8<sup>th</sup> edition Example modified for 8<sup>th</sup> edition
- ❑  $S_e = \frac{1}{2} S_{ut}$  in 8<sup>th</sup> edition
  
- ❑ a. Factor of safety if  $\sigma_a$  held constant
- ❑ b. Factor of safety if  $\sigma_m$  held constant
- ❑ c. Factor of safety if  $\sigma_a/\sigma_m = \text{constant}$
  
- ❑  $S_e = k_a k_b k_c k_d S'_e = k_a k_b k_c k_d (0.5 S_{ut}) = 33.9\text{kpsi}$

## Part b: $\sigma_a$ held constant

Before applying  $K_f$   
 $\sigma = 4.5 \text{ kpsi}$   
After applying  $K_f$   
 $\sigma = 8.38 \text{ kpsi}$

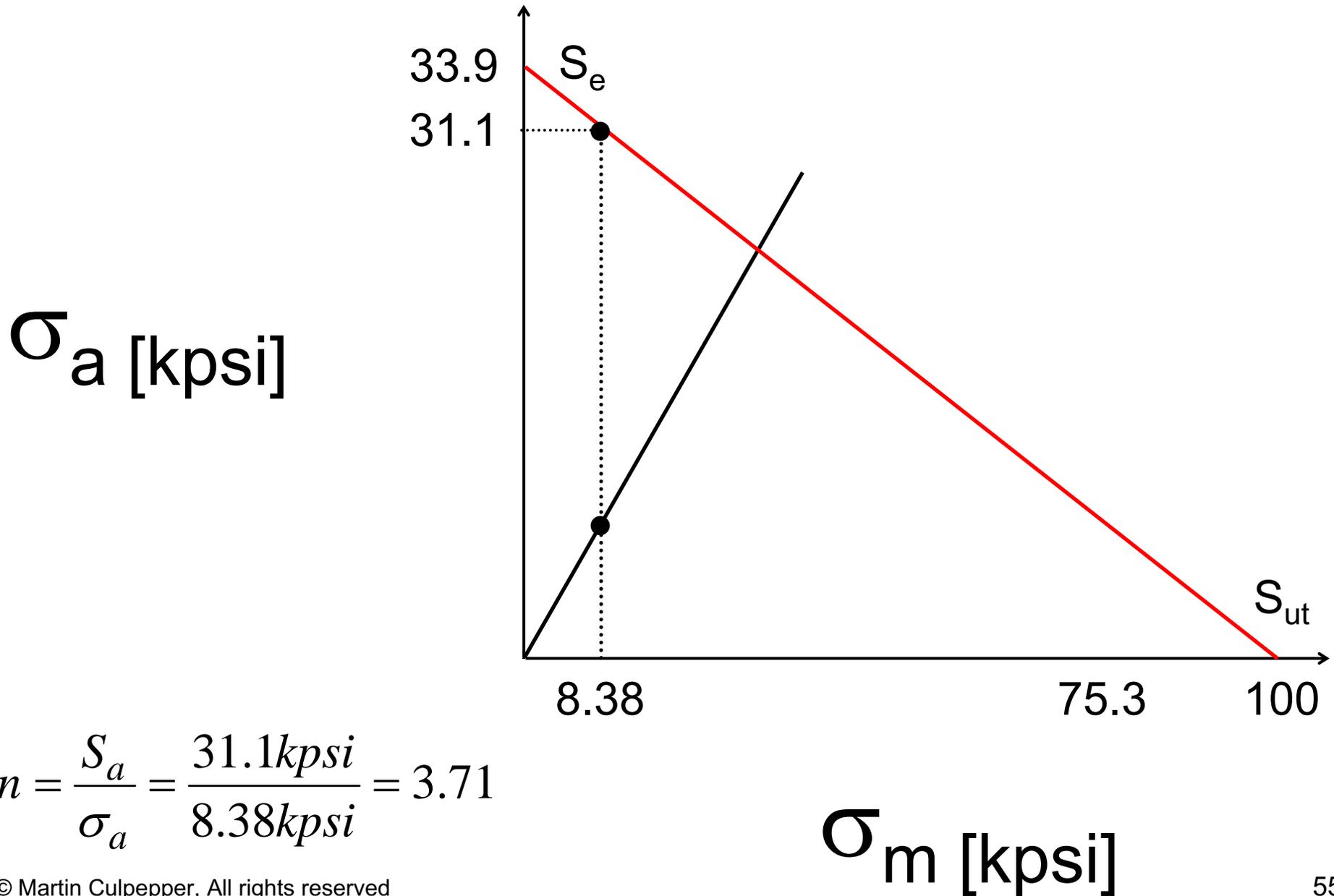
$\sigma_a$  [kpsi]



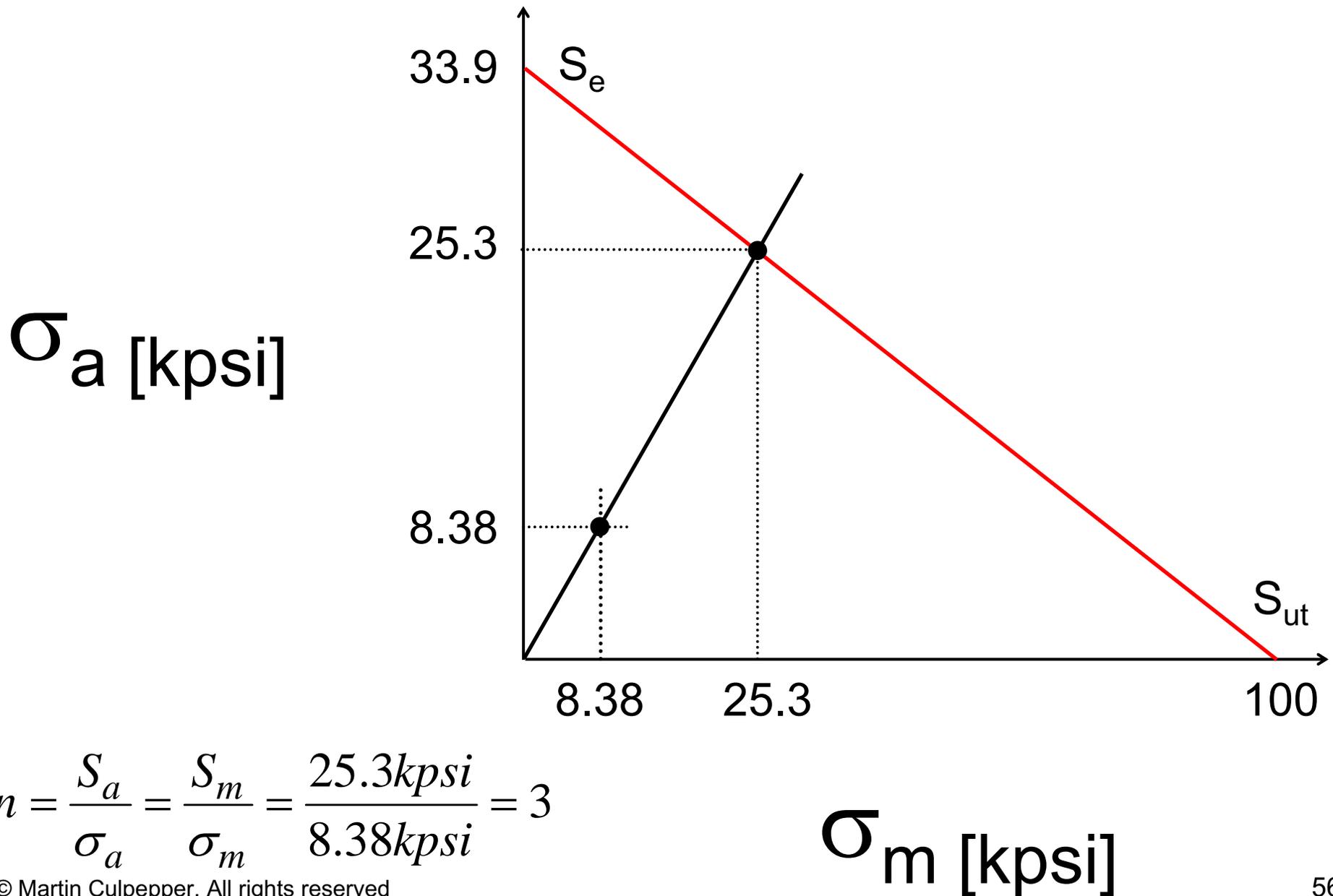
$$n = \frac{S_a}{\sigma_a} = \frac{75.3 \text{ kpsi}}{8.38 \text{ kpsi}} = 8.98$$

$\sigma_m$  [kpsi]

# Part a: $\sigma_m$ held constant



## Part c: $\sigma_a / \sigma_m$ held constant



# What about your shaft?

## Step 1: Free body diagram

- ❑ Cutting forces (2.008 person and/or next week)
- ❑ Driving loads
- ❑ Reaction loads
- ❑ Preloads
- ❑ Others... OS! loads?

I can be here  
Saturday to help,  
if people ask!!!

## Step 2: Parametric geometry & load variables

## Step 3: Material properties

## Step 4: Force magnitudes estimates/calculations

## Step 5: Stress & fatigue

- ❑  $\sigma_x, \sigma_y, \tau_{xy}, K_t, q, K_f, \sigma_a, \sigma_m, \sigma_s, \sigma_x,$

## In the end, SH... so you should program this into excel:

- ❑ In case you need to change variables... there are always changes!
- ❑ Optimization in excel.