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2.72 Elements of Mechanical Design
Spring 2009

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2.72

*Elements of
Mechanical Design*

*Lecture 16: Dynamics
and damping*

Schedule and reading assignment

Quiz

- None

Topics

- Vibration physics
- Connection to real world
- Activity

Reading assignment

- Skim last gear reading assignment... (gear selection)

Resonance

Basic Physics

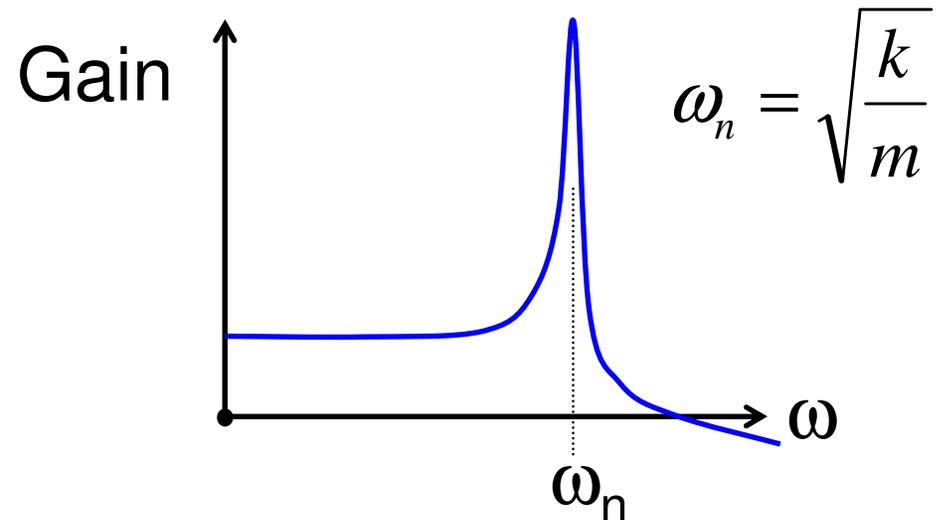
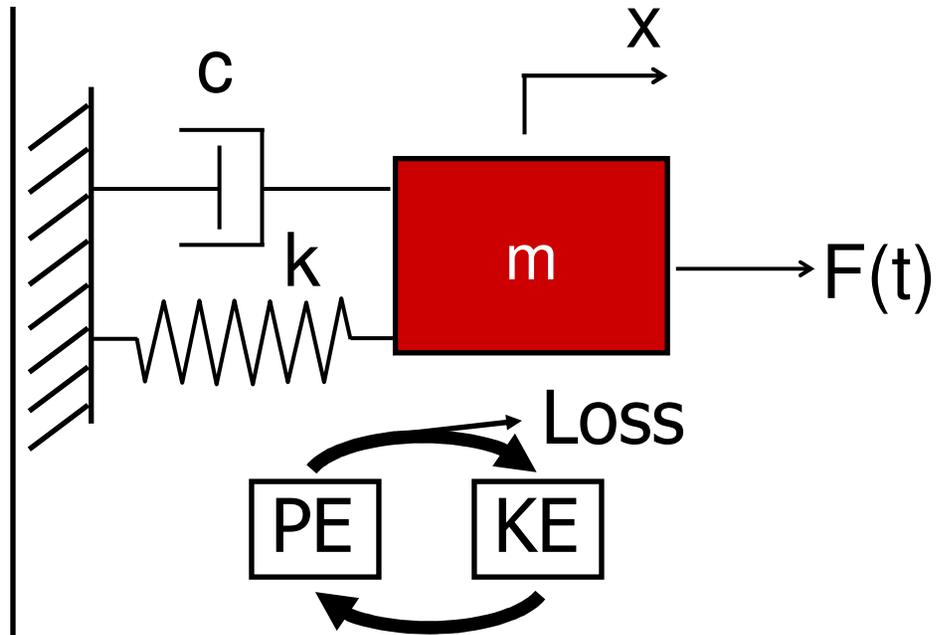
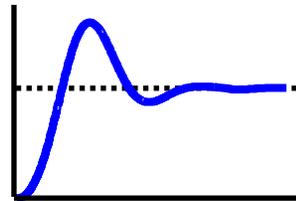
- ❑ Exchange potential-kinetic energy
- ❑ Energy transfer with loss

Modeling

- ❑ 2nd order system model
- ❑ Spring mass damper
- ❑ Differential equations, Laplace Transforms

Why Do We Care

- ❑ Critical to understanding motion of structures- desired and undesired
- ❑ Generally not steady state
- ❑ Location error
- ❑ Large forces, high fatigue



Vibrations - Input

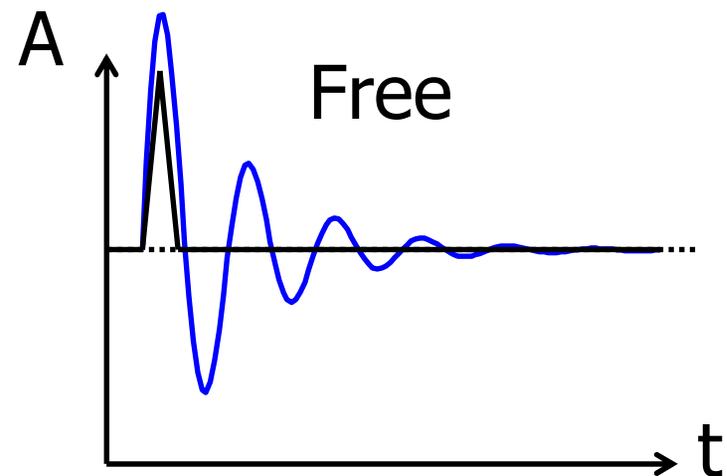
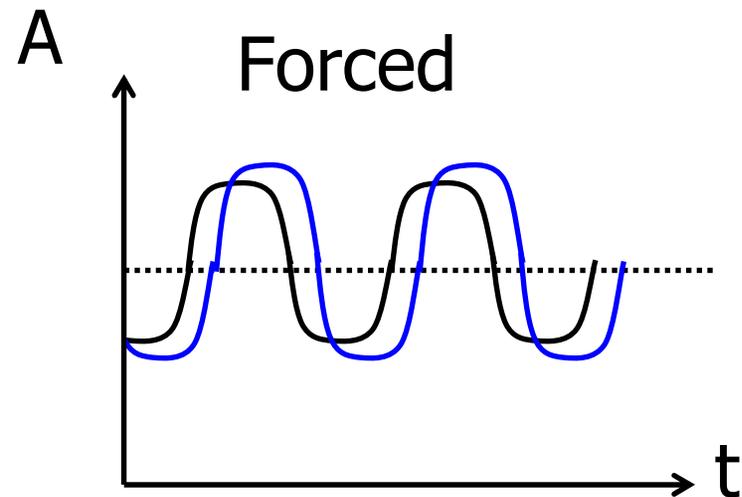
Oscillation of System

Why Categorize

- ❑ Different causes
- ❑ Different solutions

Input Form

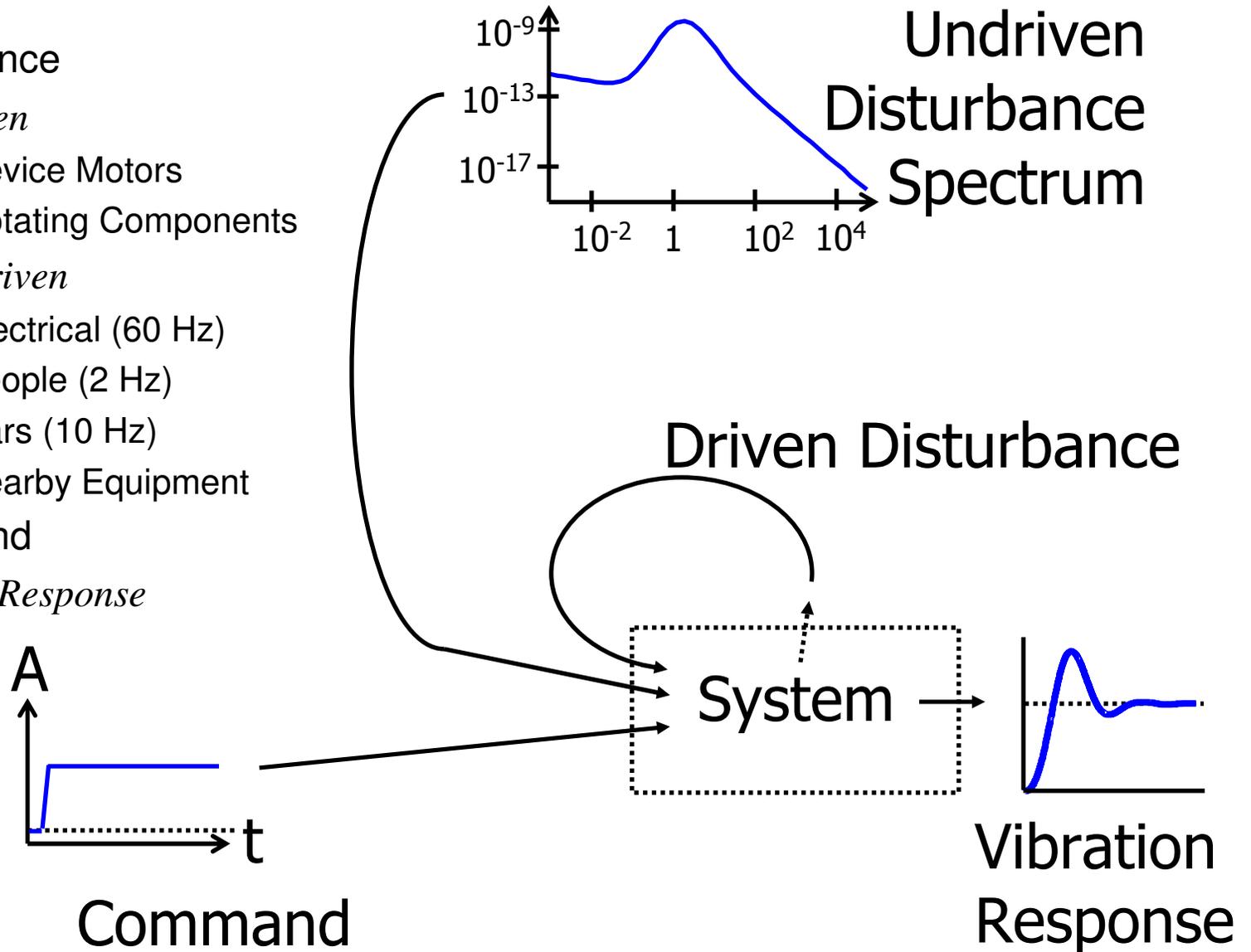
- ❑ Forced – Steady State
 - *Command Signal*
 - *Electrical (60 Hz)*
- ❑ Free – Transient
 - *Impacts*



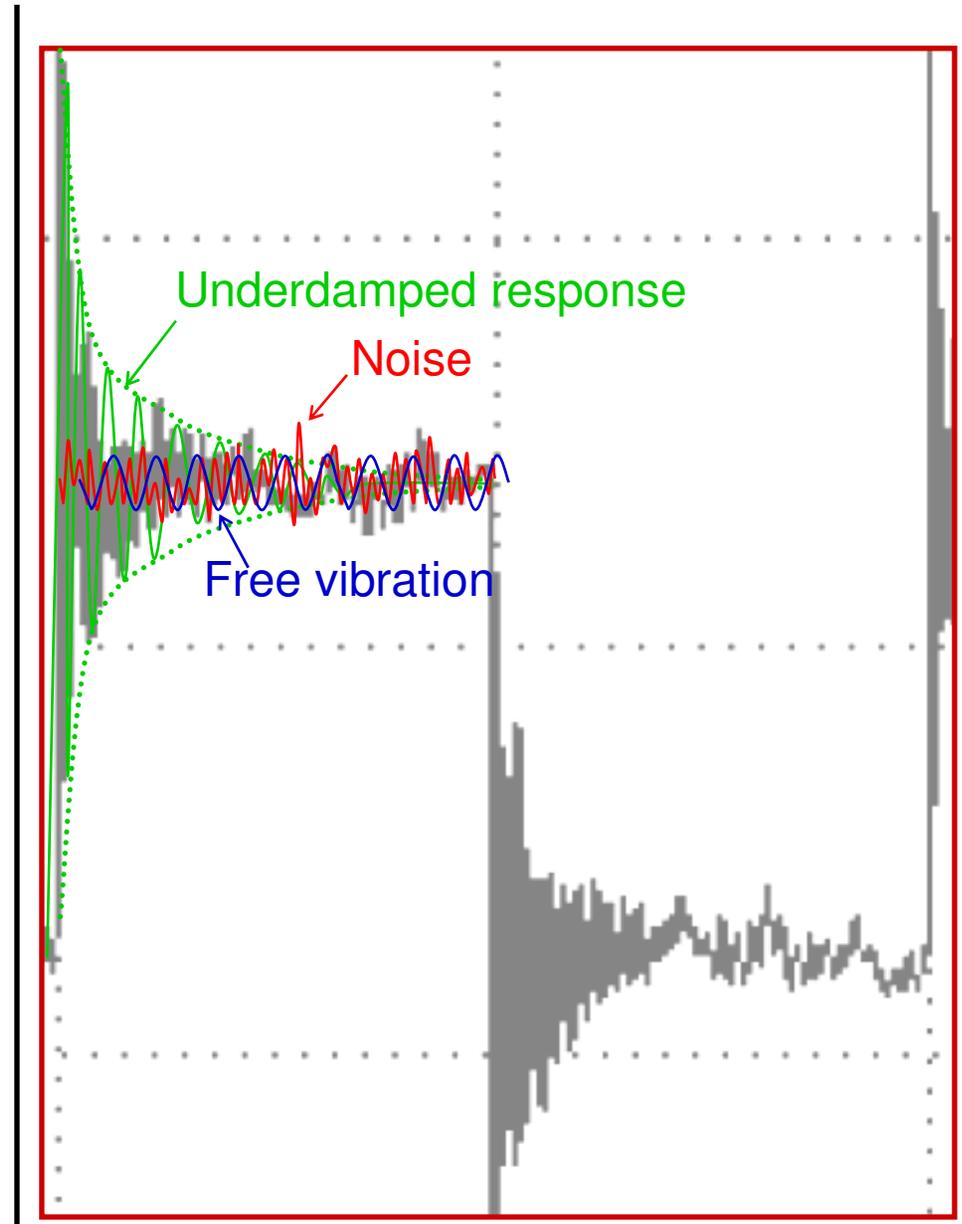
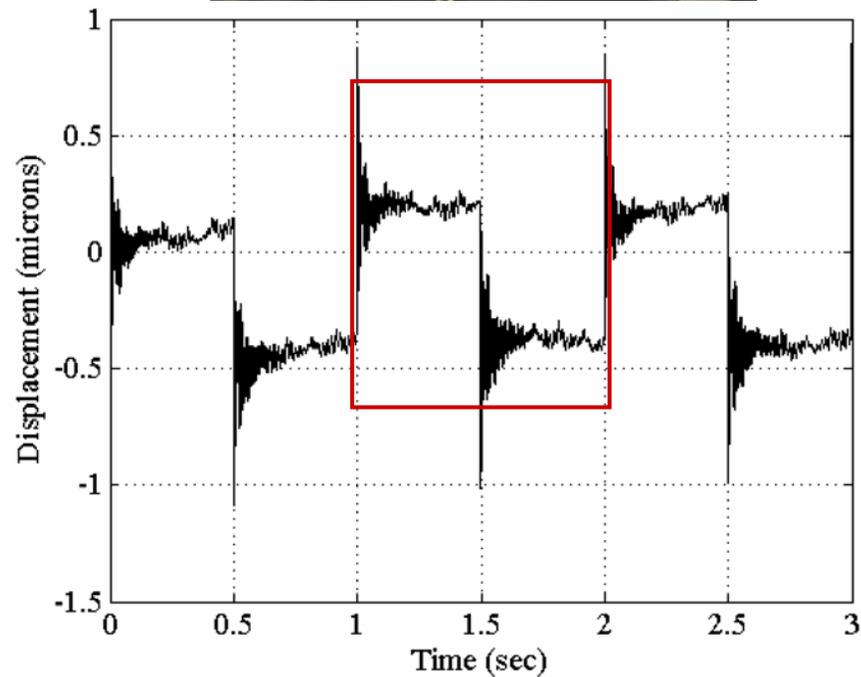
Vibrations - Source

Source

- Disturbance
 - *Driven*
 - Device Motors
 - Rotating Components
 - *Undriven*
 - Electrical (60 Hz)
 - People (2 Hz)
 - Cars (10 Hz)
 - Nearby Equipment
- Command
 - *Step Response*



Vibrations: Command vs. Disturbance

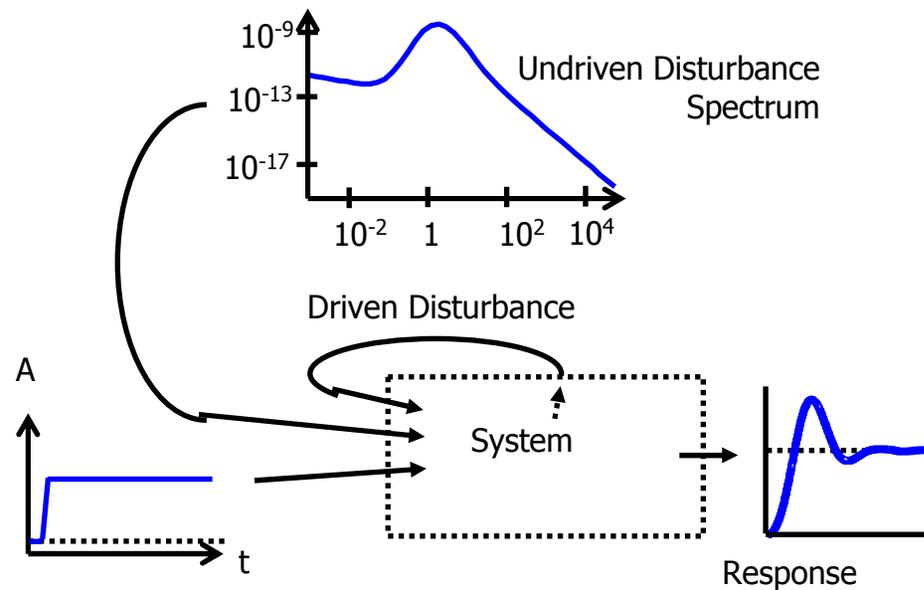
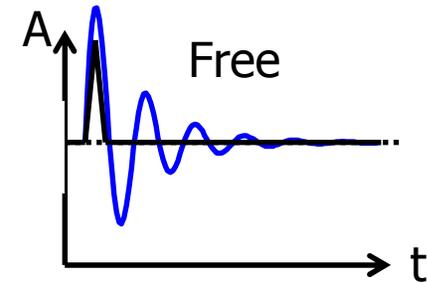
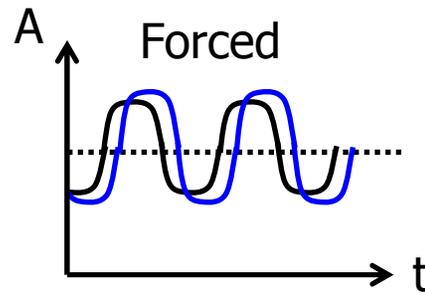


Golda, D. S., "Design of High-Speed, Meso-Scale Nanopositioners Driven by Electromagnetic Actuators," Ph.D. Thesis, Massachusetts Institute of Technology, 2008.

Vibrations - Example

Example

- ❑ Chinook
- ❑ Identify:
 - *Mode*
 - *Form*
 - *Source*
 - *Response*



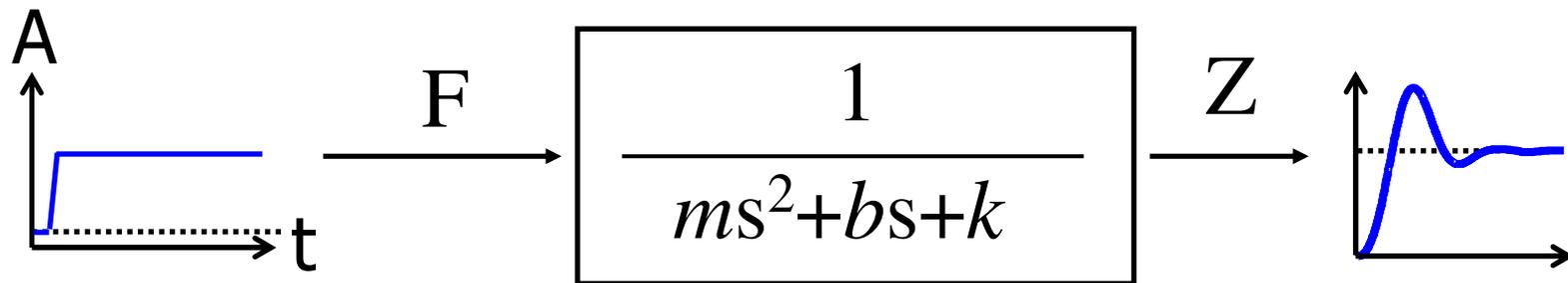
Attenuating Vibrations

Change System

- ❑ Mass, stiffness, **damping**
- ❑ Adjust mode shapes

Change Inputs

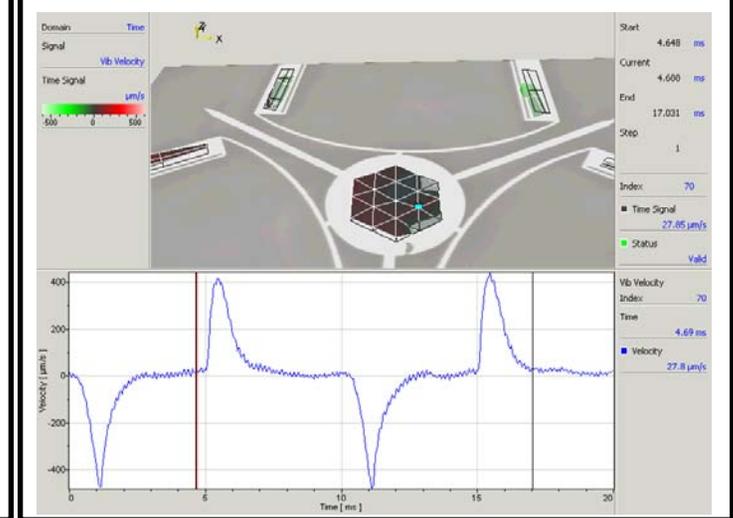
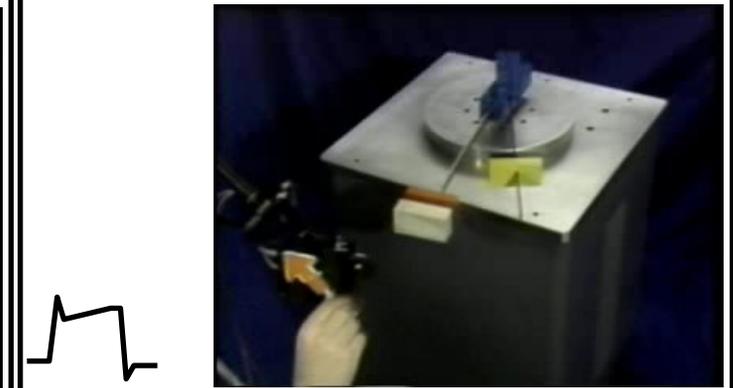
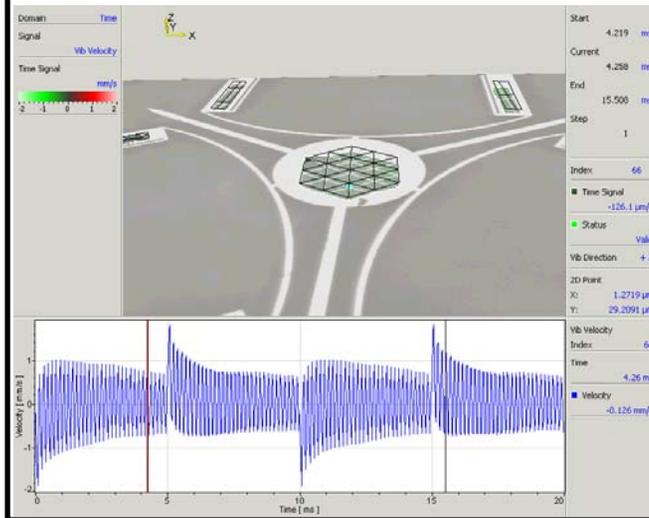
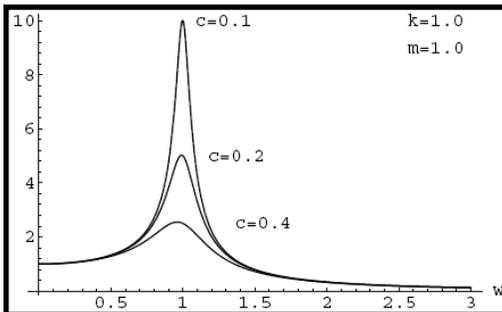
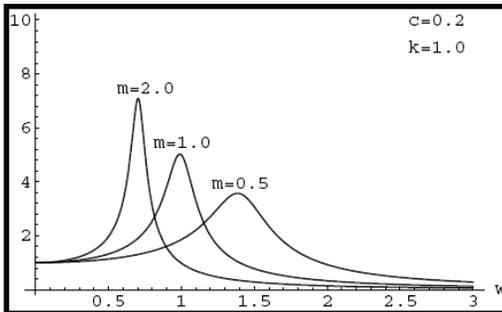
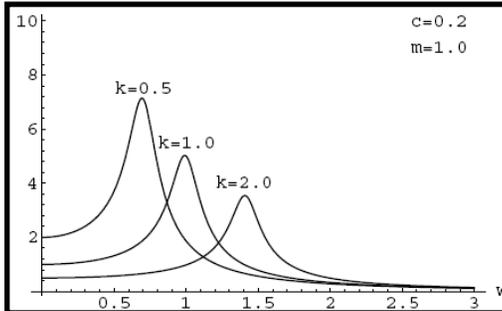
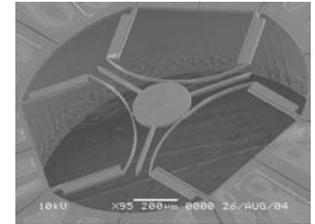
- ❑ Command: Input Modulation, Feedback
- ❑ Disturbance, reduce:
 - *undriven vibrations, e.g. optical table*
 - *driven vibrations – alter device structure (damping on motors, etc.)*



Modulating Command Vibrations

Change
m, k, c

Input shaping



Behavior

Regimes

- ❑ (1) Low Frequency ($\omega < \omega_n$)
- ❑ (2) Resonance ($\omega \approx \omega_n$)
- ❑ (3) High Frequency ($\omega > \omega_n$)
- ❑ Example – Spring/Mass demo

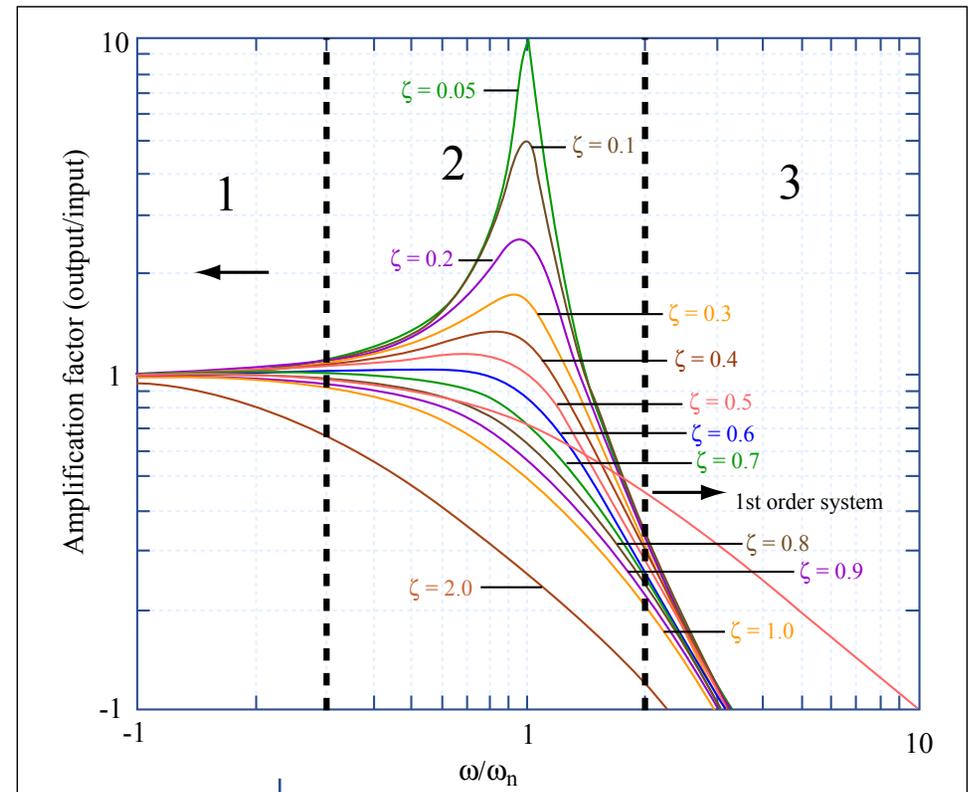


Figure by MIT OpenCourseWare.

$$\frac{x}{F} = \frac{1}{ms^2 + bs + k} = \frac{1}{k(\omega)}$$

Behavior – Low Frequency

Frequency Response Regimes

- ❑ (1) Low Frequency ($\omega < \omega_n$)
- ❑ (2) Resonance ($\omega \approx \omega_n$)
- ❑ (3) High Frequency ($\omega > \omega_n$)
- ❑ Example – Spring/Mass demo

Low Frequency ($\omega < \omega_n$)

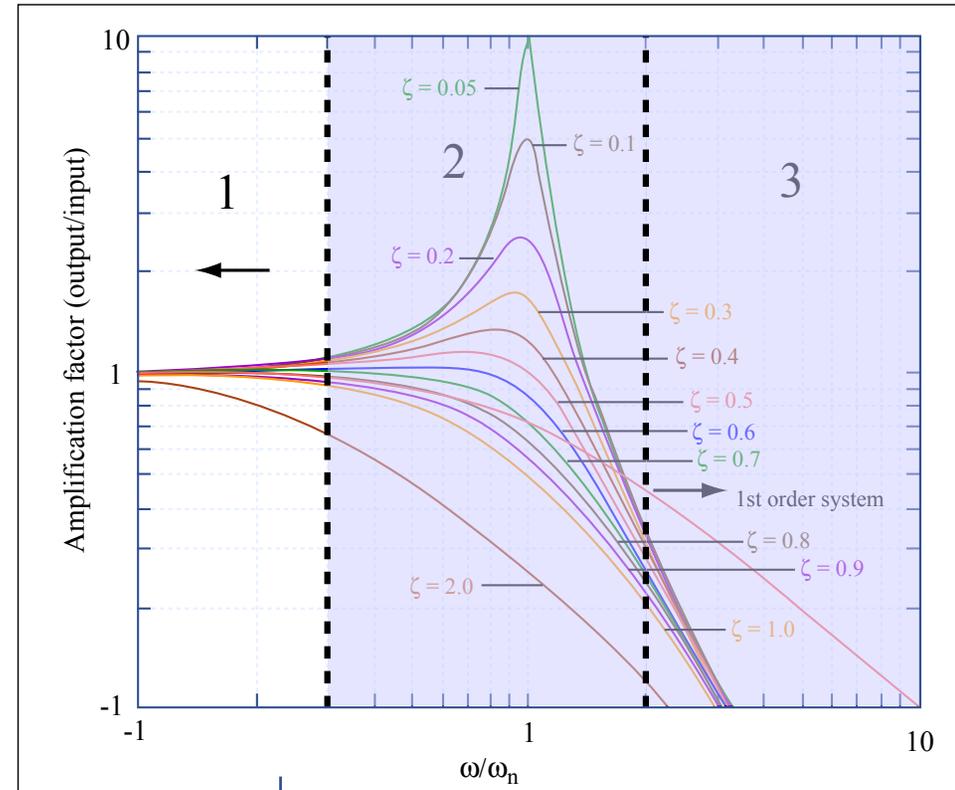
- ❑ System tracks commands
- ❑ Ideal operating range
- ❑ High disturbance rejection

$$\frac{x}{F} \approx \frac{1}{k}$$

Resonance Frequency ($\omega \approx \omega_n$)

- ❑ System Response \gg command
- ❑ $k_{\text{eff}} \downarrow$
- ❑ Disturbances will cause very large response
- ❑ Quality factor = magnitude of peak
- ❑ Damping $\uparrow = Q \downarrow$

Figure by MIT OpenCourseWare.



$$\frac{x}{F} = \frac{1}{ms^2 + bs + k}$$

High Frequency ($\omega \approx \omega_n$)

- ❑ System Response \ll command
- ❑ High disturbance rejection

Behavior - Resonance

Frequency Response Regimes

- ❑ (1) Low Frequency ($\omega < \omega_n$)
- ❑ (2) Resonance ($\omega \approx \omega_n$)
- ❑ (3) High Frequency ($\omega > \omega_n$)
- ❑ Example – Spring/Mass demo

Low Frequency ($\omega < \omega_n$)

- ❑ System tracks commands
- ❑ Ideal operating range
- ❑ High disturbance rejection

Resonance Frequency ($\omega \approx \omega_n$) $\frac{x}{k} < \frac{x}{F_1} \leq \frac{Q}{k}$

- ❑ System Response \gg command
- ❑ $k_{\text{eff}} \downarrow$
- ❑ Disturbances will cause very large response
- ❑ Quality factor = magnitude of peak
- ❑ Damping $\uparrow = Q \downarrow$

High Frequency ($\omega > \omega_n$)

- ❑ System Response \ll command
- ❑ High disturbance rejection

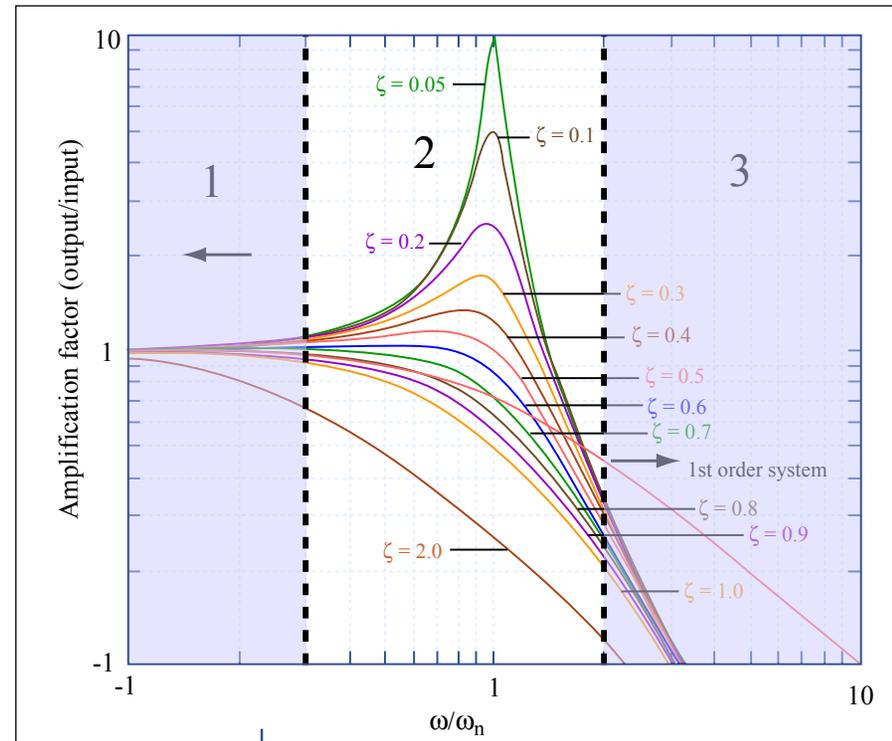


Figure by MIT OpenCourseWare.

$$\frac{x}{F} = \frac{1}{ms^2 + bs + k}$$

Behavior – High Frequency

Frequency Response Regimes

- ❑ (1) Low Frequency ($\omega < \omega_n$)
- ❑ (2) Resonance ($\omega \approx \omega_n$)
- ❑ (3) High Frequency ($\omega > \omega_n$)
- ❑ Example – Spring/Mass demo

Low Frequency ($\omega < \omega_n$)

- ❑ System tracks commands
- ❑ Ideal operating range
- ❑ High disturbance rejection

Resonance Frequency ($\omega \approx \omega_n$)

- ❑ System Response \gg command
- ❑ $k_{\text{eff}} \downarrow$
- ❑ Disturbances will cause very large response
- ❑ Quality factor = magnitude of peak
- ❑ Damping $\uparrow = Q \downarrow$

High Frequency ($\omega \approx \omega_n$)

- ❑ System Response \ll command
- ❑ Poor disturbance rejection

$$\frac{x}{F} \approx \frac{1}{m\omega^2}$$

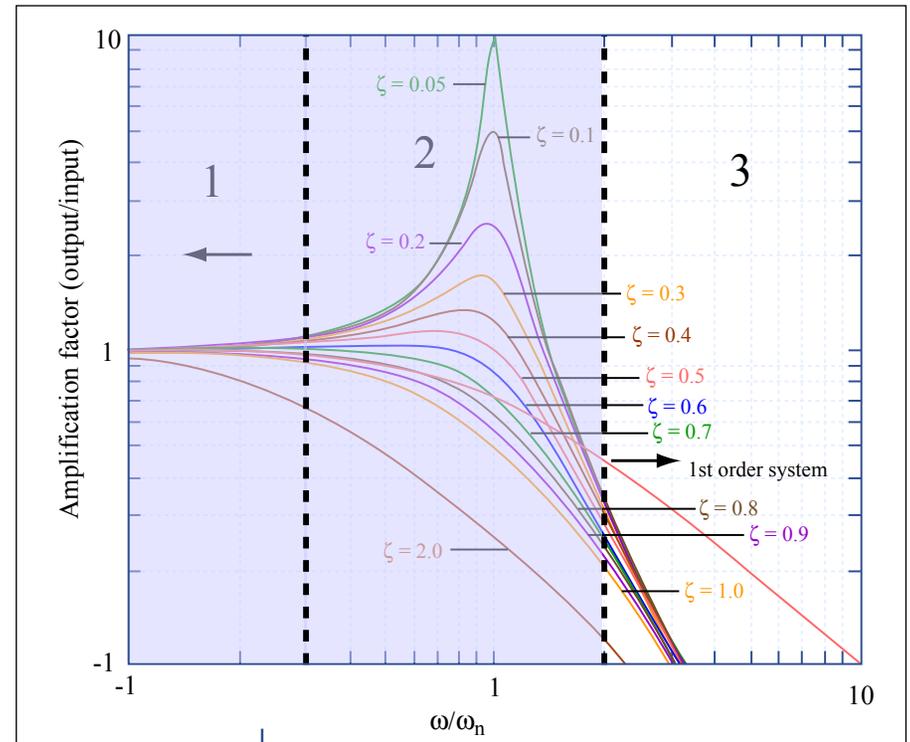


Figure by MIT OpenCourseWare.

$$\frac{x}{F} = \frac{1}{ms^2 + bs + k}$$

Constitutive Relations

Relevant equations

□ Damping ratio $\rightarrow \zeta = \frac{c}{2\sqrt{km}}$

□ ω_n $\longrightarrow \omega_n = \sqrt{\frac{k}{m}} \quad \omega_d = \omega_n \sqrt{1 - \zeta^2}$

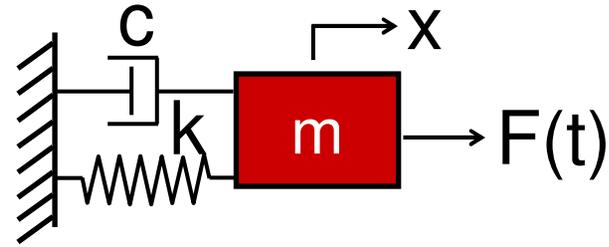
□ Gain $\longrightarrow G_P = \frac{1}{2\zeta \sqrt{1 - \zeta^2}} \quad \zeta < \frac{1}{\sqrt{2}}$

□ Quality factor $\longrightarrow Q = \frac{1}{2\zeta(1 - \zeta^2)}$

Application of Theory

Relate Variables to Actual Parameters

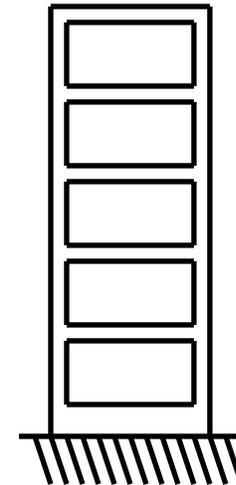
- ❑ Vibrational Mode
- ❑ Mass
- ❑ Stiffness
- ❑ Damping



Transfer between Model and Reality

- ❑ Iterative
- ❑ Start simple (1 mass, 1 spring)
- ❑ Add complexity
- ❑ Limits

Example – building (video)



Mode?
k?
m?
c?

Strategies for damping

Material

- ❑ Grain boundary
- ❑ Internal lattice
- ❑ Viscoelastic (elastomers/goo)

Pros and cons of each

Viscous

- ❑ Air
- ❑ Fluid

Electromagnetic

Friction

Active

Combinations

- ❑ Sponge

Example: Couette flow relationships

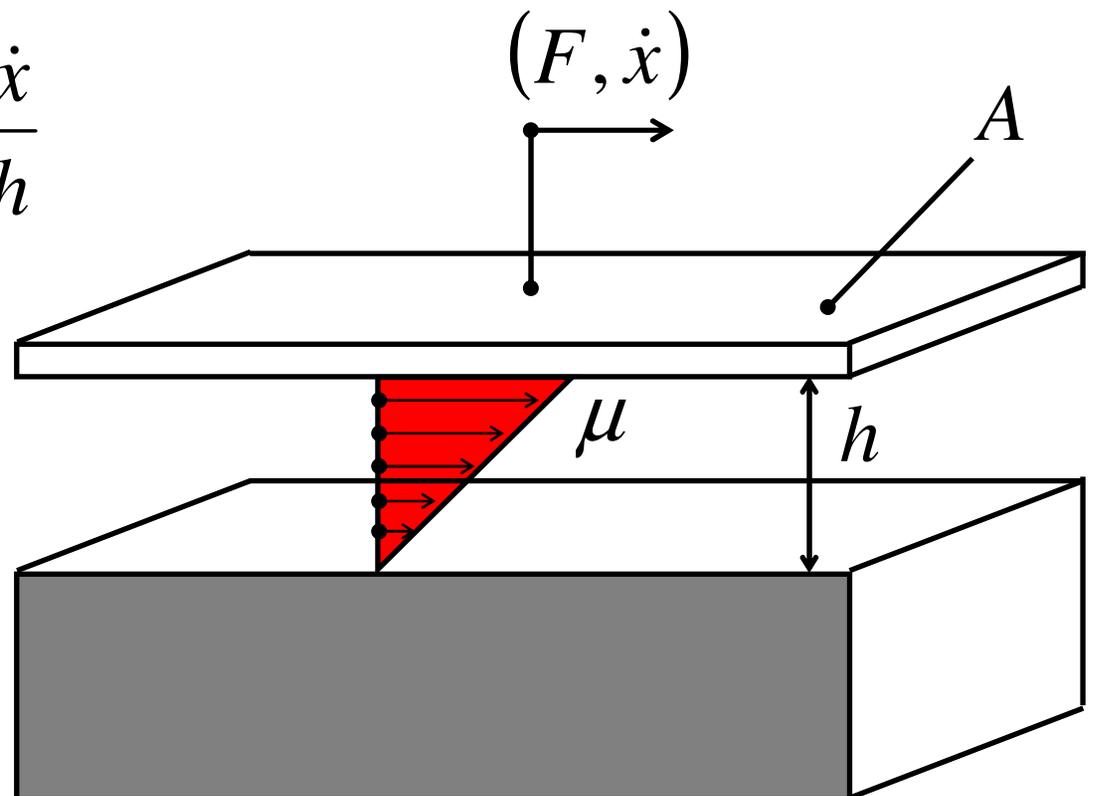
Relevant equations

$$\tau = \mu \frac{d\dot{x}}{dy}$$

$$F = \tau A = A\mu \frac{d\dot{x}}{dy} = A\mu \frac{\dot{x}}{h}$$

$$F = c\dot{x}$$

$$c = \frac{A\mu}{h}$$



Exercise (see next page too)

Perform a frequency analysis of the part

- ❑ Develop & prove (FEA) how to increase nat. freq. via geometry change
- ❑ Any constraints you might have? Geometry changes can't be unbounded
- ❑ Explain effect of your change on vibration amplitude (relative to outer base) at given ω , via sketches & plots

Xtra credit, assume:

- ❑ Flexure is contained between two parallel plates (on top and bottom)
- ❑ Viscous air damping in the gaps on both sides
- ❑ 1 micron gap between the flexure sides and plates
- ❑ Elaborate on how well flexure is damped (don't just use intuition)

Useful equations (c = damping coefficient, k = stiffness, m = mass)

Damping ratio

$$\zeta = \frac{c}{2\sqrt{km}}$$

Frequency at peak with max gain

$$\omega_p = \omega_n \sqrt{1 - 2\zeta^2}$$

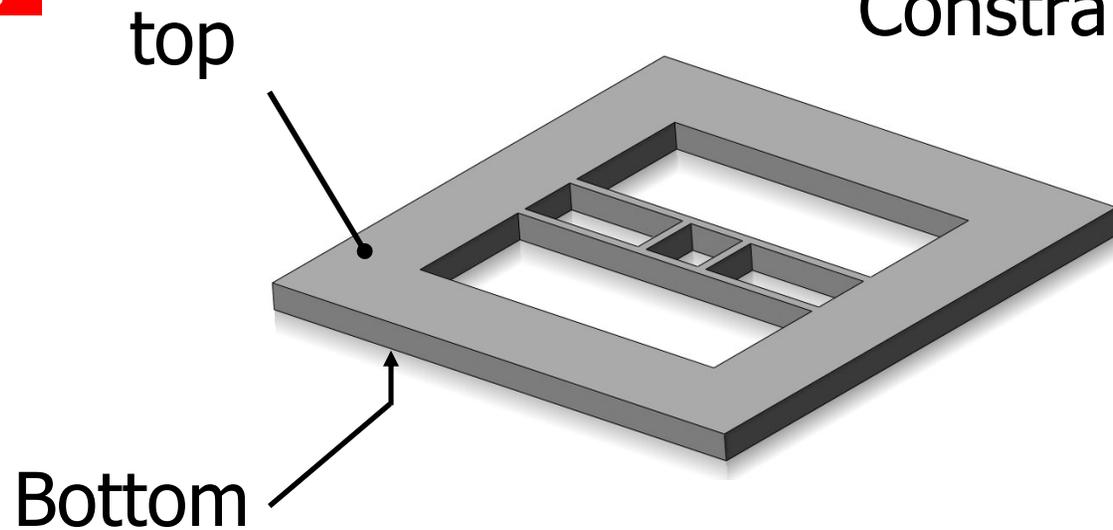
Gain at peak amplitude

$$G|_p = \frac{1}{\sqrt{4\zeta^2 - 4\zeta^4}}$$

Flexure

Flexure design

Constrained on 4 sides



See this diagram for extra credit:

Top plate

Flexure

Bottom plate

Multiple Resonances

